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AN INVESTIGATION OF WIND POWER POTENTIAL AT KALAM - NWFP

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Pakistan Meteorological Department (Project is financed by Ministry of Science & Technology)

Executive Summary

Pakistan Meteorological Department (PMD) conducted a wind power potential survey of the northern areas of Pakistan. Funding for this project was provided by the Ministry of Science & Technology. Under this wind data was collected at 42 sites along the Northern parts of the Country.

In this report the analysis based on one year wind data has been presented along with the wind generated electric power at Kalam (Swat), NWFP. Wind data with one minute average speed and direction were collected at 10 meters and 30 meters height and 50 meters values were computed from models.

At 50 meters we have the annual average wind speed of 1.71 m/s during twelve months August-2006 to July-2007 the highest of 3.63 is observed in July. Seasonal Diurnal Wind variation indicates that maximum wind speed is available in the morning thought-out the year. Wind frequency distribution shows that during 29% of the time wind speed is 5 m/s or above.

Sometimes simply wind speed averages do not give the true picture of the wind power optional of an area. For the purpose it is common to assign areas to one of the seven wind classes based on "wind power density" of the area. Monthly and annual wind power density has been computed and added in the report. The annual power density of Kalam is 155.66 w/m² according to international wind classification, this power density categorize Kalam as a below marginal site for wind power generation. Though monthly power density values indicates that the power density is blow marginal category but this is compensated by very high values during summer months especially in June and July.

Wind generated electric power has as also been computed on hypothetical 600Kw wind turbine and its hourly, monthly and annual values has been added in this report. The annual power production form a single 600kw wind turbine come out to 240,300 kWh which shows the capacity factor of 5% for Kalam. Internationally it is accepted that if any site has a capacity factor of 25% and above than that site is suitable for installation of economically viable wind power farms. As such Kalam and surrounding areas can be classified as no suitable site for installing big economically viable wind farms.

1. **Introduction:**

Wind energy is the fastest growing renewable energy source today. A continued interest in wind energy development worldwide has produced steady improvements in technology and performance of wind power plants. New wind power projects have proven that wind energy not only is cost competitive but also offers additional benefits to the economy and the environment.

A steady supply of reasonably strong wind is necessary requirement for utilizing the power in the wind. Development of wind energy depends upon a clear understanding of wind resources. Site location, turbine performance and physical effects of turbulence and energy extraction represent a few of the issues that must be addressed by anyone interested in developing wind energy.

As such any plan to develop wind energy must begin by understanding the wind resource. Where are the best potential wind sites located? How much energy could be extracted from the wind at those sites?

1.1 Characteristic of wind:

The global winds are caused by pressure differential across the earth's surface. The amount of solar radiation absorbed at the earth's surface is greater at the equator than at the poles. This variation in incoming heat sets up convective cells in the lowest layer of the atmosphere. In the simplest form air rises at the equator and sinks at the poles. However the rotation of the earth complicates this simple heat transfer. A series of circulations are set up in both northern and southern hemispheres.

The areas of the globe where air is descending are zones of high pressure and where the air is ascending, low-pressure zones are formed. The pressure gradient drives the flow of air from high to low pressure, thus causing the wind. The wind is then acted on the corriolis force due to the earth's rotation. The resultant wind is turned easterly or westerly. On a smaller scale, wind is created because of temperature difference between land and sea and mountains and valleys. The local topographical features and roughness of the terrain also cause air movements.

2.0 <u>Wind Mapping Project of Pakistan Meteorological Department:</u>

As any plan to develop wind energy must begin by understanding the wind resources. Where are the best potential wind sites located? How much energy could be extracted from the wind at those sites? Will the wind turbine performance be affected by the turbulence or other wind resource characteristics?

To answer these questions and to provide wind resource database for the different potential parts of the country, Pakistan Meteorological Department prepared a phased programme. Government of Pakistan, Ministry of Science and Technology provided the necessary funding for undertaking the Phase II. Second phase covers the Northern areas of Pakistan.

2.1 Study Area:

The project area for the wind mapping Phase-II covers the Northern areas of Pakistan including Districts are Swat, Dir, Chitral, Gilgit, Skardu, Haripur, Shangla, Buneer, Nowshara, Peshawar, Mohmad Agency, Khyber Agency and Azad Kashmir.

Forty-Two stations for collecting wind data have been installed to study the wind regime as shown in Map-1. The list of stations is given below:

Fatehpur, Bahrain, Kalam, Khawazakhaila, Malamjabba, Tahash, Khungipayan, Dir, Tarbella, Nizampur, Warsak, Chitral City, Drosh, Mirkhani, Shagore, Garam Chasma, Khagozi, Reshan, Mastuj, Kalash, Ayune, Astore, Bunji, Chillas, Gilgit, Gupis, Sost, Passu, Aliabad, Shigar, Barapayan, Sermik, Lowaramaina, Ramatkore, ShahidaSir, Danakool, Besham, Moorti Pahari, Rangla, Pedar, Lempiapatian, Dargaye.

Kalam is situated in district Swat, NWFP. Latitude & Longitude of Kalam is: Latitude = 35.20°, Longitude = 72.55°

2.2 **Data source:**

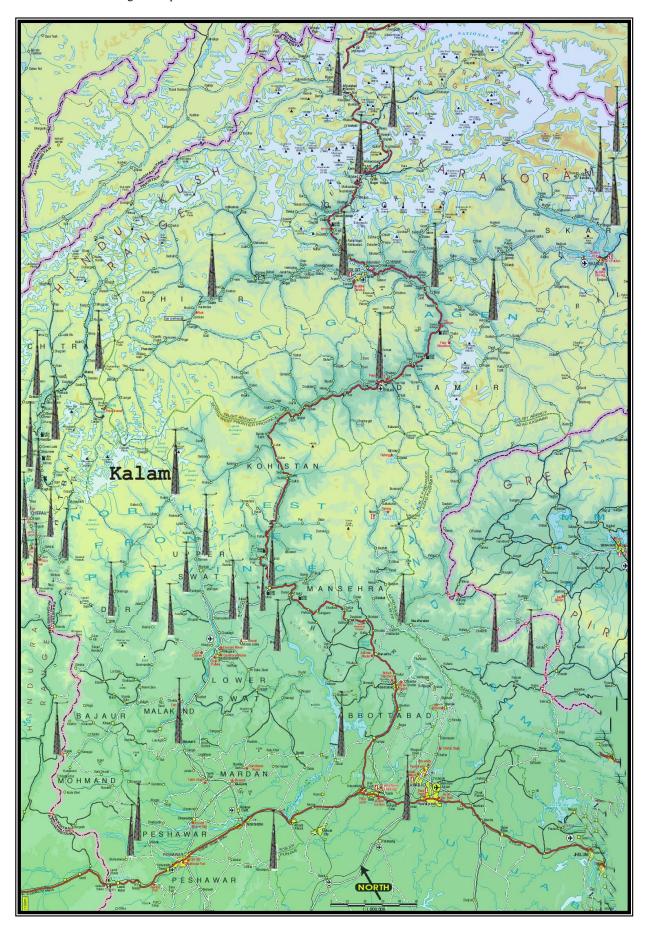
To undertake this study 30-meter high towers are erected at the locations mentioned above. On each of these high towers two wind speed anemometers are installed at the height of 10 meters and 30 meters, respectively; wind vane for recording wind direction is installed at 30 meters height. Temperature sensors are also installed at 10 meters height. Automatic data loggers developed locally have been installed to record data at each site. These data loggers are recording, one-minute average wind speed at both level, five-minute average wind direction, five-minute average temperature and 10-minute average minimum and maximum wind speed. While selecting the above-mentioned locations for wind monitoring; the main objective was to identify potentially windy areas that also possess other desirable qualities of wind energy developed site. Further following guidelines as far as possible were also kept in mind while choosing an exact location for monitoring towers.

- Towers are placed as for as possible away from the local obstruction to the wind
- Selected location should be representative of the majority of the site.

Since sating a tower near obstructions such as trees or building can adversely affect the analysis of the site's wind characteristics such as magnitude of wind resource, wind shear and turbulence levels the tower in most cases are placed as for as possible away from local obstructions to the wind. But where this rule could not be followed, the tower was placed at horizontal distance of 10 times the height of the obstruction in the prevailing wind direction as required internationally. The following parameters have been recorded during the study.

- i. Wind speed one minute average at 10 & 30 meters
- ii. Maximum wind speeds during 10 minutes
- iii. Minimum wind speeds during 10 minutes
- iv. Wind direction five minutes average at 30 meters
- v. Temperature 5 minutes average in °C

Every month a team of observers and Maintenance Engineers visit site to inspect the instruments and to download the data on a laptop. Finally, the data is compiled and analyzed at Renewable Energy Research Cell established at Meteorological Department Islamabad.



Map-1: Shows 42-Towers Installed in Wind Mapping Project in Northern Areas

3.0 Methodology; Analysis & Discussion:

3.1 Wind speed variation with height:

Wind speed tends to increase with height in most locations, a phenomenon known as wind shear. The degree of wind shear depends mainly upon on two factors, atmospheric mixing and the roughness of the terrain.

Atmospheric mixing typically follows a daily cycle driven by solar heating. At the hub height of a wind turbine, this cycle often causes wind speeds to increase in the daytime and decrease at night. However, the range of variation between night and day typically diminishes as hub height increases. At a height of approximately 50 meters, it weakens or may even disappear in some cases.

Terrain roughness also affects wind shear by determining how much the wind is slowed near the ground. In areas with a high degree of roughness, such as forests or cities, near- surface wind speeds tend to be low and wind shear high, whereas the converse is true in areas of low roughness such as flat, open fields. Wind shear may be greatly reduced or eliminated where there is an abrupt change in terrain height such as a sea cliff or mountain ridge.

To save money wind measurements sometimes are taken at a lower height than the wind turbine tower. In that case, it is essential to measure wind shear at different times of day in different seasons to accurately predict the performance of a wind power plant. The shear can be measured by monitoring wind speeds at two or three heights on a tower. Since wind turbines produce much more power in stronger winds, wind turbine designers try to put turbines on the tallest possible towers. At some point, however, the increased cost of towers outweighs the benefits. With current wind turbine technology, the optimum tower height for large wind machines appears to be approximately 40 to 50 meters.

For saving money in this survey also the wind has been recorded at 10 & 30 meters and for calculating the wind speed at 50 meters the following two methods has been used in this study.

3.1.1 *Log Law:*

The turbulent mixing in the atmosphere may be considered in a similar way to molecular mixing (this is called k theory). Assuming the mixing is dominated by mechanical mixing due to shear forces a relationship of wind speed with height is derived.

$$u = \frac{u_*}{k} \ln \left(\frac{z - D}{z_o} \right)$$

Where

 U_* is the friction notify

k is the von Karman constant

 $\mathbf{Z_0}$ is the roughness length

D is the displacement height

The von Karman constant is generally taken as 0.4. The roughness length Z_0 is related to the vegetation cover of the area. The values of roughness length are given in Table-1. The displacement height D is the height above the roughness elements where the flow is free. For most vegetation it is small and is generally treated as zero. For large roughness elements like trees and building in towns it is not negligible and is the order of the average height of the elements. The <u>log law</u> may only be used for heights above D. Turbines are rarely sited in forests or towns, so D is usually taken as zero.

The wind speed at any height z can then be computed provided that the wind speed at a height Z_R is known. Thus:

$$\frac{u}{u_R} = \frac{\ln \left(\frac{z}{z_o} \right)}{\ln \left(\frac{z}{z_o} \right)}$$

Where

 U_R is the wind speed at reference height Z_R

The reference height is usually 10m or 30m as this is the height at which mean wind data is generally collected.

3.1.2 *Power Law:*

Engineers often prefer to use a <u>Power Law</u> to describe the increase in wind speed with height, as it is easier to evaluate.

$$\frac{u}{u_R} = \left(\frac{z - D}{z_R}\right)^{\alpha}$$

Where:

 α is the power law exponent

 U_R is the wind speed at reference height Z_R

The power law exponent typically varies between 0.1 and 0.32 depending upon the landscape type. A value of 1/7 is often quoted as a reasonable value for the power law exponent in countryside. The exponent can be calculated from the roughness length.

$$\alpha = \frac{\ln \left(\ln \left(\frac{z}{z_{o}} \right) \right)}{\ln \left(\frac{z}{z_{R}} \right)} \approx \frac{1}{\ln \sqrt{\frac{z \cdot z_{R}}{z_{o}}}}$$

Where: Z is the measurement height

Z_R is the reference height

Z₀ is the roughness length

The power law exponent therefore varies with the interval between the two measurement heights. The power law should be carefully employed since it is not a physical representation of the surface layer and does not describe the flow nearest to the ground very well. Both the log law and the power law are simplified expressions of the <u>wind profile</u>. They are valid in flat homogeneous terrain. So they do not include the effects of topography, obstacles or changes in roughness or stability.

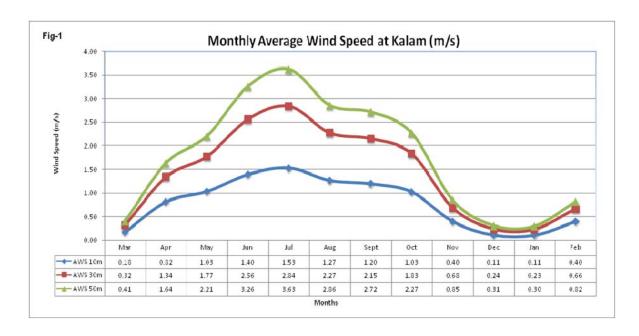
Table 1: Typical values of surface roughness length Z_0 and power law exponent α for various types of terrain

Type of terrain	\mathbf{Z}_0	α
Mud Flats, Ice	10 ⁻⁵ to 3x 10 ⁻⁵	
Calm Sea	2x10 ⁻⁴ to 3x10 ⁻⁴	
Sand	$2x10^{-4}$ to 10^{-3}	0.01
Mown Grass	0.001 to 0.01	
Low Grass	0.01 to 0.04	0.13
Fallow Field	0.02 to 0.03	
High Grass	0.04 to 0.1	0.19
Forest and Woodland	0.1 to 1	
Built up area, Suburb	1 to 2	0.32
City	1 to 4	

3.2 Average Wind Speed:

By using above mentioned methods the wind speed at 50 meters has been computed and monthly average of these wind speed at 50 meters height have been given in Fig 2 in graphical as well as tabular form.

Fig-1 shows monthly average wind speed at height of 10 meters, 30 meters and 50 meters from August 2006 to July 2007. At 30 meters height, we have the maximum average wind speed of 2.84 m/s during July, 2007. At 50 meters we have the annual average wind speed of 1.77 m/s from August-2006 to July 2007 and the highest average wind speed of 3.63 m/s is observed during July 2007.



3.3 **Diurnal Wind speed Variation:**

Fig-2 shows the annual diurnal wind speed variations at Kalam. The wind speed is generally lower during night and after sunrise it starts picking up and reaches maximum around 1400 which is around 4.42 m/s and 5.54 m/s at 30 meters and 50 meters height respectively.

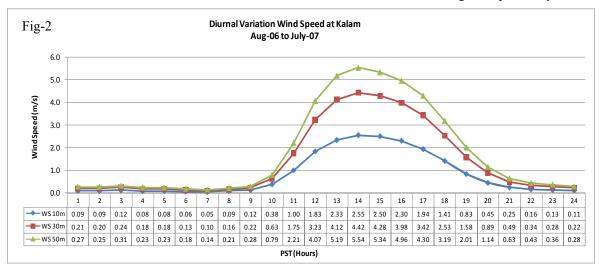
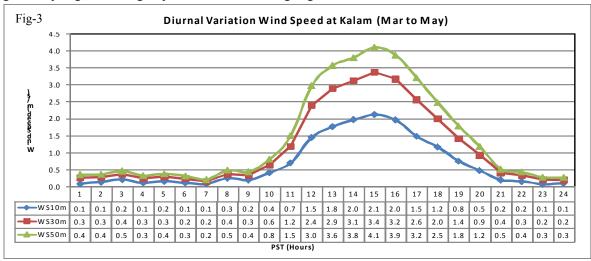
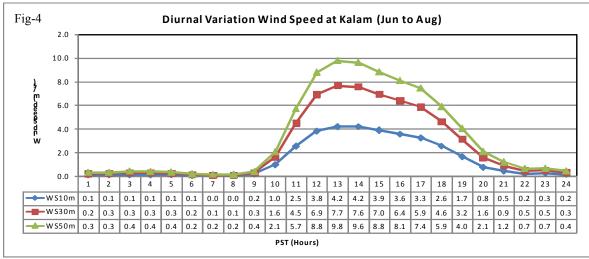
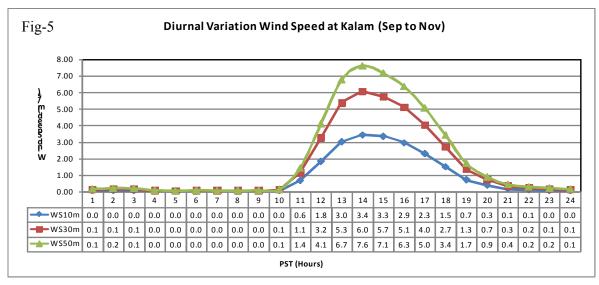
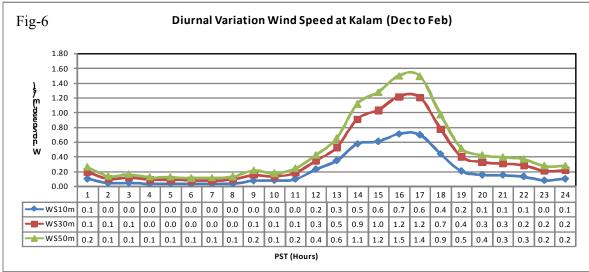


Fig-3, Fig-4, Fig-5 and Fig-6 shows the seasonal diurnal wind speed variations at Kalam for (Mar-May), (June-Aug), (Sep-Nov) and (Dec-Feb) respectively. Seasonal wind speed is generally higher during daytime and low during night in Kalam.









3.4 Wind speed Frequency Distribution:

Wind speed frequency distribution can simply be obtained by plotting the different wind speeds against their frequencies / relative frequencies. For obtaining frequency distribution the following two procedures are necessary.

3.4.1 **Binning of Data:**

The sorting of the data into narrow wind speed bands is called binning of the data. In our case a bin width of 1m/sec has been used e.g. a measured wind speed of 3.5 m/sec would be placed in 3<X<=4 m/sec bin. The central value of each bin i.e. 0.5 m/sec, 1.5 m/sec etc has been used in calculations and frequency distribution group.

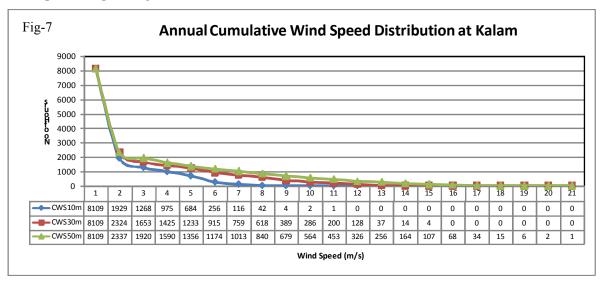
3.4.2 *Relative Frequency:*

It is proportional wind speed in each bin. It can be viewed as the estimate of probability of given wind speed in the bin. Relative frequency is defined as

R.F = probability P(Vi) = Frequency of given wind speed / Total period

3.4.3 Annual Cumulative Wind Frequency:

Fig-7 shows the Annual Cumulative Wind Frequency distribution at three heights 10, 30 and 50 meters. The analysis indicate that in a year at a height of 30 meters during 1233 hours the wind speed is greater than equal to 5 m/s whereas at 50 meters, during one year 1356 hours the wind speed is equal or greater than 5m/s.



3.4.4 Wind Frequency Distribution:

Fig-8 shows the Annual wind frequency distribution at Kalam. We can see that at 50 meters during 182 hours wind speed is 5 m/s, 160 hours speed is 6 m/s, 173 hours speed is 7 m/s, 115 hours speed is 8 m/s and during 110 hours the wind speed is 9m/s and so on. This indicates wind potential in this area.

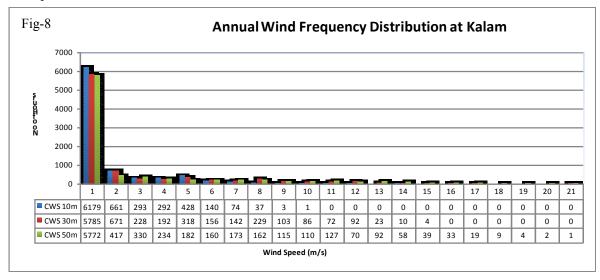
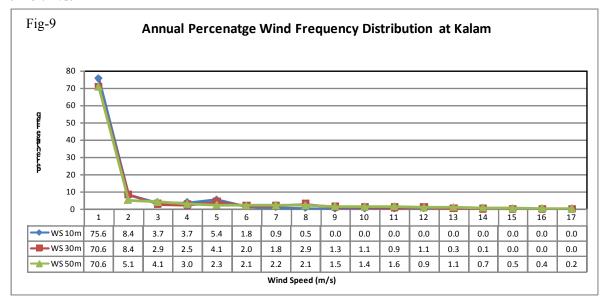


Fig-9 gives the frequency distribution in percentage. At 50 meters we find that during 2.3% of time wind is 5m/s, 2.1% of the time 6m/s and 2.2% of the time it is 7m/s. whereas at 30 meters height we get 4.1% of the time wind speed 5m/s, 2.0% of the times 6m/s and 1.8% of the time 7m/s.



3.4.5 Seasonal Wind Frequency Distribution:

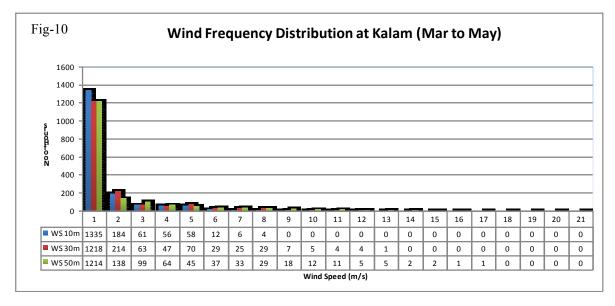
Figures 10–17 gives seasonal wind frequency distribution and percentage wind frequency distribution.

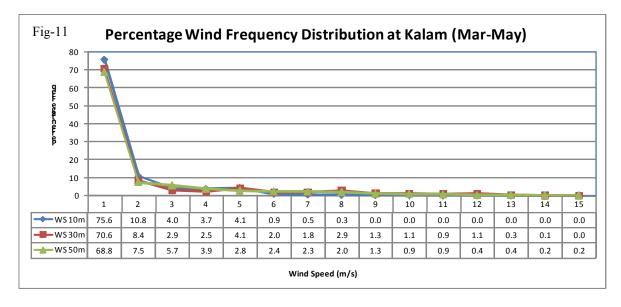
March- May

Fig-10 shows frequency distribution during the months of March to May. We can see that in this period at 30 meters height during 70 hours we get 5m/s, 29 hours 6m/s, 25 hours 7m/s.

Similarly at 50 meters we get 45 hours 5m/s, 37 hours 6m/s, 33 hours 7m/s, 29 hours 8m/s, 18 hours 9m/s, 12 hours 10m/s.

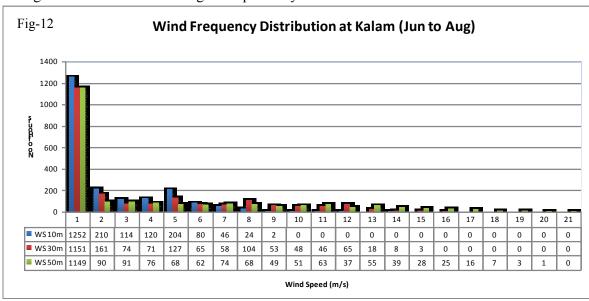
Similarly the above mentioned seasonal frequency distribution percentage terms have been presented in figure 11.

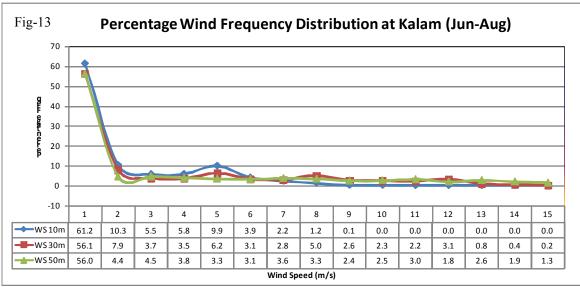




June - August

Fig-12 and 13 shows wind frequency distribution and percentage frequency distribution during the months of June to August respectively.



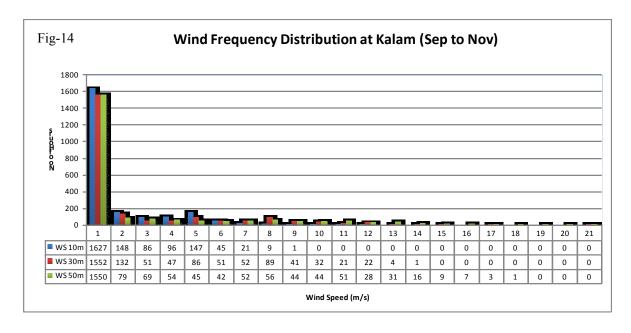


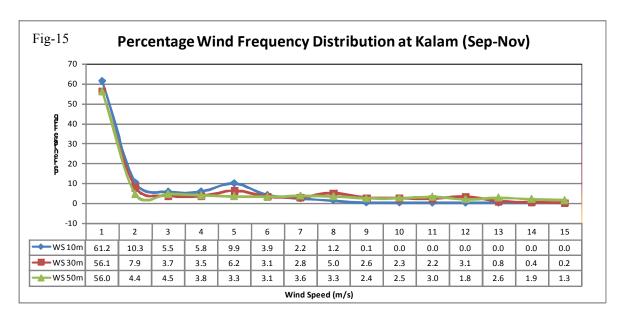
Sep - Nov

Fig-14 shows frequency distribution during the months of September to November. We can see that in this period at 30 meters height during 86 hours we get 5m/s, 51 hours 6m/s, 52 hours 7m/s.

Similarly at 50 meters we get 45 hours 5m/s, 42 hours 6m/s, 52 hours 7m/s, 56 hours 8m/s, 44 hours 9m/s, 44 hours 10m/s.

Similarly the above mentioned seasonal frequency distribution percentage terms have been presented in figure 15.



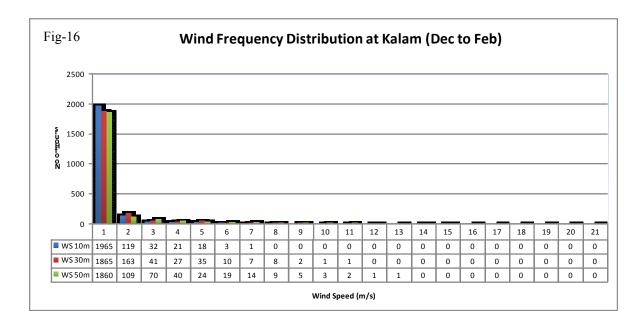


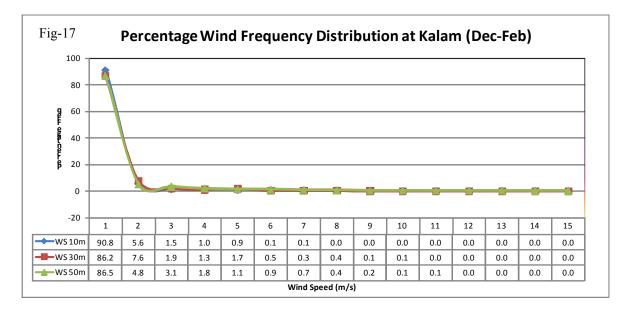
Dec-Feb

Fig-16 shows frequency distribution during the months of December to February. We can see that in this period at 30 meters height during 35 hours we get 5m/s, 10 hours 6m/s, 7 hours 7m/s.

Similarly at 50 meters we get 24 hours 5m/s, 19 hours 6m/s, 14 hours 7m/s, 9 hours 8m/s, 5 hours 9m/s, 3 hours 10m/s.

Similarly Fig-16 shows seasonal frequency distribution percentage for the months of Dec to Feb.

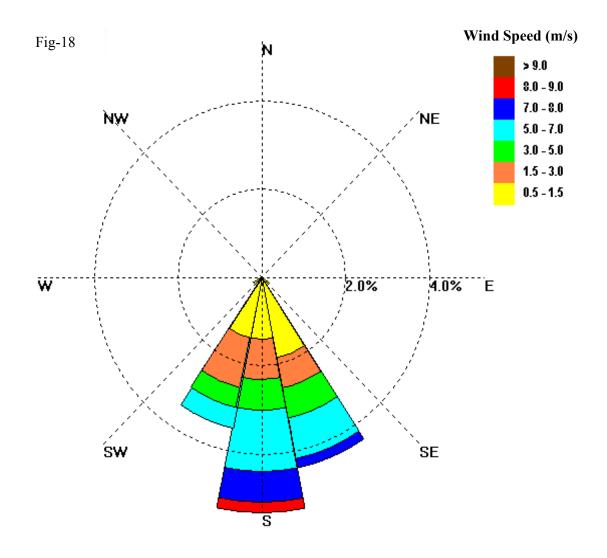




3.5 Wind Rose:

Fig-18 shows the Wind Rose Graph based on 12 months data from August 2006 – July 2007 collected at 30 meters height. Wind Rose indicates that most of the time the wind direction was South, South west and south east. The average wind speed is 1.41 m/s and the percentage of wind speed greater than 5m/s is 29%.

Wind Rose at Kalam (30m height during 12 months)



Average Wind Speed	Wind greater than 5 m/s	Comments
1.41 m/s	29%	

3.6 Wind speed statistic:

3.6.1 The statistical Mean:

It is the average of a set of n numbers. Mathematically, we can write

$$M e a n = \frac{\left[\sum_{i=1}^{n} x_{i}\right]}{N}$$

The Mean Wind Speed V can be calculated by the formula.

$$V = \sum_{i=1}^{n} V_{i} P(V_{i})$$

Where Vi is the central wind speed of bin 1 and P(Vi) is the probability/relative frequency that the wind speed has in bin i.

3.6.2 Variance:

It is one of the several indices of variability that statistician, use to characterize the dispersion among the measures in a given set of data. Mathematically, variance is written as

Variance =
$$\sigma^2 = \sum (X_i - V)^2$$

Where V is mean of data set

In case of wind speed data, we can write it, as

$$\sigma^2 = \sum V_i^2 P(Vi) - (V)^2$$

3.6.3 Standard Deviation

It is the square root of the variance, denoted by σ

$$\sigma^2 = (\sigma)^{1/2} = \sum (V_i^2 P(V_i) - (V)^2)^{1/2}$$

3.7 Wind power density:

While investigating a wind power potential of an area, the average values of wind speed does not truly represent this potential because lot of information regarding frequency distribution of wind speed is suppressed in the process of averaging wind speed. As such the most important values for estimating the wind power potential of a given site is the value of the wind power density or the available theoretical instantaneous power from the wind. This available wind power in the wind is the flux of Kinetic Energy crossing the wind energy conversion system and its cross – sectional area.

Like water flowing in the river, wind contains energy that can be converted to electricity using wind turbines. The amount of electricity that wind turbines produce depends upon the amount of energy in the wind passing through the area swept by the wind turbines blades in a unit of time. This energy flow is referred to as the wind power density.

A key aspect of wind power density is its dependence on wind speed cubed. This means that the power contained in the wind increases very rapidly with wind speed; if the speed doubles, the power increases by a factor of eight. In practice, the relationship between the power output of a wind turbine and wind speed does not follow a cubic relationship. Below a certain minimum speed, the turbine does not have enough wind to operate, whereas above a certain speed its output levels off or begins to decline. In very high winds the turbine may even be shut down to prevent damage to it.

Wind power density also depends on air density. At higher attitudes, air density decreases and, as a result, so does the available power. This effect can reduce the power output of wind turbines on high mountains by as much as 40 percent compared to the power that could be produced at the same wind speeds at sea level. Air density depends inversely on temperature: colder temperatures are favorable for higher air densities and greater wind power production.

3.7.1 Wind power classes:

To simplify the characterization of the wind power potential, it is common to assign areas to one of seven wind classes, each representing arrange of wind power density at the special height above the ground. The standard International wind power classifications are shown in Table 2.

	Resource	30m I	Height	50m I	Height
Class	Potential	Wind Speed m/s	Wind Power W/m²	Wind Speed m/s	Wind Power W/m²
1		0 - 5.1	0 - 160	0 - 5.6	0 - 200
2	Marginal	5.1 - 5.9	160 - 240	5.6 - 6.4	200 - 300
3	Moderate	5.9 - 6.5	240 - 320	6.4 - 7.0	300 - 400
4	Good	6.5 - 7.0	320 - 400	7.0 - 7.5	400 - 500
5	Excellent	7.0 - 7.4	400 - 480	7.5 - 8.0	500 - 600
6		7.4 - 8.2	480 - 640	8.0 - 8.8	600 - 800
7		8.2 - 11.0	640 - 1600	8.8 - 11.9	800 - 2000

Table-2: International Wind Power Classification

By and large, the areas being developed today using large wind turbine are ranked as class 5 and above. Class 4 areas are also being considered for further development as wind turbines are adopted to run more efficiently a lower wind speeds. Class1 and class2 areas are not being deemed suitable for large machines, although a smaller wind turbine may be economical in areas where the value of the energy produced is higher

3.7.2 *Power of wind Energy:*

A parcel of Wind possesses kinetic energy

$$E = \frac{1}{2}mV^2$$

From this, power density is calculated as

$$P = \frac{e}{t} = \frac{1}{2} \frac{dm}{dt} V^2$$

Where $\frac{dm}{dt}$ is the mass of air following time.

From fluid dynamics, it can be proved that

$$dm/_{dt} = \varphi AV$$

Volume of cylindrical cross section can be written as

$$V = \pi r^2 L \qquad ---- \qquad (1)$$

Where r is radius of cylinder and L is length of it.

The wind moving with velocity V travels this distance L in time t so

$$S = L = Vt$$

So equation L takes the form

$$V = \pi r^2 V t$$

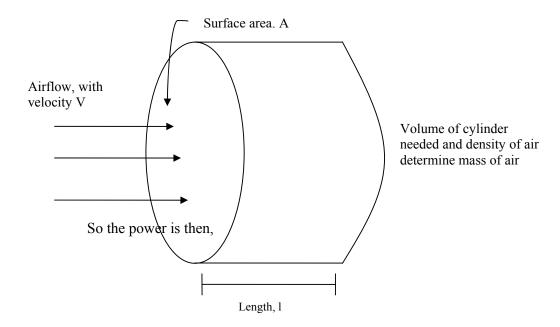
Now mass of wind can be written as

$$M = \varphi A v t$$

Differentiating

$$dm/_{dt} = \varphi AV d/_{dt(t)} = \varphi AV$$

Where φ is density of wind and others parameters have been defined in diagram.



$$P = \frac{1}{2} \frac{dm}{dt} V^2 = \frac{1}{2} \varphi AVT / t V^2$$
$$= \frac{1}{2} \varphi AV^3$$

And power density

$$P_A = \frac{1}{2} \varphi V^3$$

Density of wind at mean sea level is 1.225 kg/m³

At 15° C, The area depends upon the size of the rotor. Therefore, it is clear that power density chiefly depends on wind velocity and goes up as a cube of it.

3.7.3 Wind power calculation using Mean wind Speed:

Wind power calculated from Mean wind speed is not true representative of wind power. In real world, the wind varies constantly. Actual wind power density at most sites can rang from 1.0 to 3 times greater then that calculated. For example, we take wind speed of 5, 7 and 8 m/sec respectively the respective power densities are 76 wat/m², 210 watt/m² and 313 watt/m². The average of which is 200 watt/m². On the other hand, the average wind speed is 6.7 m/sec and power density of average wind is 181 watt/m². So the power of wind calculated by mean wind speed is less than the actual power present in wind i.e. Mean wind speed is not true representative for the wind power calculations.

To overcome this drawback we find some alternative arrangement, which reduces the deficit. The Weibull distribution is the best fit of wind data to calculate wind power based on mean wind speed and variance/standard deviation.

3.7.4 Weibull distribution:

The Weibull distribution (named after the Swedish physicist W. Weibull, who applied it when studying material strength in tension and fatigue in the 1930s) provides a close approximation to the probability laws of many natural phenomenons. It has been used to represent wind speed distribution for application in wind loads studies for sometime. In recent years most attention has been forced on this method for wind frequency applications not only due to its greater flexible and simplicity but also because it can give a good fit to experimental data.

The Weibull distribution function, which is a two-parameter function, has been found to fit much wind data with acceptable accuracy is expressed mathematically as

$$\phi(u) = \frac{k}{c} \left(\frac{u}{c}\right)^{k-1} \exp\left(-\left(\frac{u}{c}\right)^{k}\right)$$

Where:

u is the wind speed

c is the scale parameter with units of speed

k is the shape parameter and is dimensionless

When k = 2 the distribution reduces to Rayleigh distribution and if k=1 an exponential distribution is found. These are special cased of Weibull distribution.

Solving the equation, we find that the scale factor c is closely related to the mean wind speed for the site.

$$\overline{u} = c\tau \left(1 + \frac{1}{K}\right)$$

Where au is the complete gamma function

Similarly

$$\overline{u^n} = c^n \tau \left(1 + \frac{n}{k}\right)$$

And so

$$\overline{u^3} = c^3 \tau \left(1 + \frac{3}{k} \right)$$

The available power density is obtained:

$$E = \frac{1}{2}\varphi c^3 \tau \left(1 + \frac{3}{k}\right)$$

Where

E is the power density in watts / m^2

The shape factor k is related to the variance of the wind

$$\sigma^2 = c2 \left[\left(1 + \frac{2}{k} \right) - \left(\tau \left(1 + \frac{1}{k} \right) \right)^2 \right]$$

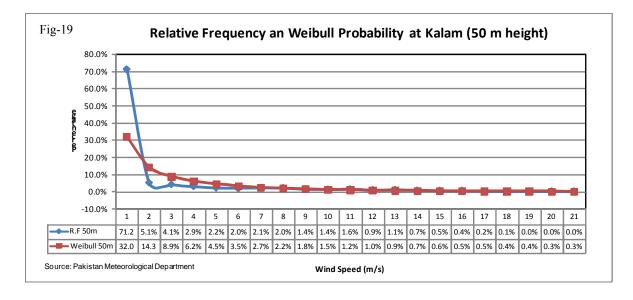
The two Weibull parameters k and c may be derived from site data.

A measure of the confidence of the fit of the Weibull curve to the real data is also returned. Often the Weibull curve is a good fit to the most of the data, but a poor fit to some. If the poor fit is in the low wind speed range, i.e. below cut in it may be possible to ignore the poor fit as this portion of wind does not contribute greatly to the overall power production.

The mathematical description of the wind frequency allows us to match with the turbine power curve. Thus a measure of the average total power capture in a year is achieved. Additionally the choice of turbine cut in and furling speed may be chosen to maximum the total energy capture.

3.7.5 Weibull Parameters:

Fig-19 shows the Weibull fit to the relative frequency of wind speed.



The Weibull parameters for three different heights 10 meters, 30 meters and 50 meters are given in Table-3 along with other key results of analysis. If we look at the shape parameters K and scale parameter C for 50 meters height we can find that the shape parameter K varies over a wind range from the lowest of 0.55 during November to the highest of 0.87 during the month of January with a annual value of K being 0.75.

The lowest values of the scale parameter C 0.66 is observed in December while the highest value of 3.44 is obtained in July and with an annual value of 1.76.

3.7.6 Average Wind Speed & Standard Deviation:

In Table-3 monthly average wind speed and standard deviation at three different heights are also given. The average wind speed values for 10 meters and 30 meters height have been obtained from the recorded data, whereas the values for the 50 meters height have been computed by using the power law as explained in the earlier section.

At 10 meters height the annual average wind speed is 1.17 m/s with Standard deviation of 1.24, at 30 meters this average speed is 1.76 m/s with Standard deviation of 2.19.

At 50 meters the monthly average wind speed varies from the lowest of 0.73 m/s in January to highest of 3.89 m/s during July. Whereas the average wind speed is 2.13 m/s with Standard deviation of 2.81.

3.7.7 **Power Density:**

The monthly power densities for three different heights 10meters, 30meters and 50meters have also been given in Table-3. At 10 meters this power density varies between 0.32 W/m² January to 0.35 W/m² in December with Average of 10.94 W/m².

At 30 meters height the power density varies from 1.01 W/m^2 in January to 1.18 W/m^2 in December and the average values is about 69.84 W/m^2 .

At 50 meters height the power density of Kalam varies from 2.13 W/m^2 in January to 2.68 W/m^2 in July. The average power density of the area is 155.66 W/m^2 .

Table-3: Monthly Average Wind, St. Deviation and Wind Power Density at Kalam

			10 m		
	Avg V (m/s)	St Dev	C (m/s)	K	P/A (w/m ²)
January	0.58	0.40	0.65	1.52	0.32
February	0.82	0.88	0.79	0.92	2.51
March	0.63	0.47	0.69	1.37	0.48
April	1.21	1.30	1.17	0.93	8.02
May	1.36	1.56	1.25	0.86	14.04
June	1.70	1.85	1.62	0.91	23.15
July	1.81	1.92	1.76	0.94	25.70
August	1.59	1.74	1.51	0.90	19.27
September	1.52	1.73	1.42	0.87	19.04
October	1.38	1.59	1.27	0.86	14.72
November	0.83	0.99	0.75	0.83	3.63
December	0.59	0.42	0.65	1.45	0.35
Average	1.17	1.24	1.13	1.03	10.94
			30 m		
	Avg V (m/s)	St Dev	C (m/s)	K	P/A (w/m²)
January	0.68	0.65	0.69	1.05	1.01
February	1.06	1.43	0.86	0.72	11.84
March	0.74	0.75	0.74	0.99	1.54
April	1.71	1.98	1.57	0.85	28.56
May	2.06	2.68	1.72	0.75	76.17
June	2.84	3.52	2.49	0.79	165.31
July	3.09	3.66	2.81	0.83	180.90
August	2.57	3.19	2.25	0.79	123.36
September	2.45	3.18	2.07	0.75	125.54
October	2.14	2.88	1.74	0.72	97.38
November	1.09	1.71	0.75	0.61	25.32
December	0.68	0.68	0.68	1.00	1.18
Average	1.76	2.19	1.53	0.82	69.84
			50 m		
	AvgV (m/s)	St Dev	C (m/s)	K	P/A (w/m²)
January	0.73	0.83	0.68	0.87	2.13
February	1.20	1.79	0.88	0.65	26.32
March	0.82	0.97	0.74	0.83	3.37
April	2.01	2.45	1.79	0.81	55.43
May	2.49	3.41	2.00	0.71	164.13
June	3.54	4.58	3.00	0.76	374.32
July	3.89	4.75	3.44	0.80	404.34
August	3.18	4.10	2.69	0.76	269.37
September	3.03	4.10	2.45	0.72	282.47
October	2.62	3.70	2.02	0.69	218.28
November	1.26	2.18	0.74	0.55	65.10
December	0.74	0.90	0.66	0.82	2.68
Average	2.13	2.81	1.76	0.75	155.66

ESTIMATING WIND GENERATED ELECTRIC POWER OUTPUT

Appendix-I

Monthly Average Diurnal Variation of Wind Generated Electric Power Output.

Appendix-II

Hourly Wind Generated Electric Power Output

4.0 Estimating Wind Generated Electric Power Output

The average power output of wind energy conversion technologies (WECT) is a very important parameter since it determines the energy output over time thereby influencing the economic feasibility of a wind project. It is by far more useful than the rated power, which does not account for the variability of wind velocity thereby easily overestimating energy revenues. The average power of wind turbine, $\overline{P_{WT}}$, is the power produced at each wind speed multiplied by the fraction that wind speed is experienced, integrated over all possible wind speeds. In integral form this can be expressed as (Manwell et al., 2002; Borowy and Salameh, 1996):

$$\overline{P_{WT}} = \int_{0}^{\infty} P_{WT}(v) df(v)$$

This integral can be replaced with a summation over bins, N_{B_s} to calculate the average wind turbine power (Manwell et al., 2002).

$$\overline{P_{WT}} = \sum_{j=1}^{N_B} \left\{ \exp \left[-\left(\frac{v_{j-1}}{c}\right)^k \right] - \exp \left[-\left(\frac{v_j}{c}\right)^k \right] \right\} P_{WT} \left(\frac{v_{j-1} + v_j}{2}\right)$$

Please note that the relative frequency, f_j/N , corresponds to the term in brackets and the power output is calculated at the midpoint between v_{j-1} and v_j .

The available power at any given wind speed v that is convertible by a turbine is defined by (Manwell et al., 2002 Johnson, 1985)

$$P_{WT}(v) = \frac{1}{2} \rho A C_p \eta v^3$$

Where η is the drive train efficiency (i.e. generator power/rotor power), C_p , is the machine power coefficient. In an idealized wind turbine no losses are experienced and the power coefficient, C_p , is equal to Betz' limit (i.e. $C_{p,Betz}=16/27$) and $\eta=1$. Of course, in reality both the drive train efficiency and the power coefficient cannot be maximized. The extent to which the power output is limited by physical laws as well as engineering inefficiency is dependent on the specific characteristics of individual wind turbine types. This aspect will be discussed further in the analysis of the case study.

WECTs have a range of different power output performance curves, which need to be recognized when estimating the potential power output. The power output performance curves are not only defined by parameters such as the power coefficient and the drive train efficiency but also constrained by cut-in speed, furl-out speed and rated wind speed. Where the cut-in wind seed, ν_c , is the minimum wind velocity to generate power from a turbine, the rated wind speed, ν_R , is the wind speed at which the 'rated power' of a WETC is achieved and generally corresponds to the point at which the conversion efficiency is near its maximum and furl-out wind speed, ν_F , is the wind speed at which the turbine shuts down to prevent structural damage.

To account for the above-mentioned constraints we can formulate a novel formula for the average electrical power output of a turbine, $\overline{P_{WTA}}$:

$$\overline{P_{WTA}} = \begin{cases}
\sum_{j=1}^{N_B} \left\{ \exp\left[-\left(\frac{v_{j-1}}{c}\right)^k\right] - \exp\left[-\left(\frac{v_j}{c}\right)^k\right] \right\} P_{WT}\left(\frac{v_{j-1} + v_j}{2}\right) & (v_c \le v \le v_R) \\
\overline{P_{WTA}} = \left\{ \sum_{j=1}^{N_B} \left\{ \exp\left[-\left(\frac{v_{j-1}}{c}\right)^k\right] - \exp\left[-\left(\frac{v_j}{c}\right)^k\right] \right\} P_{WT}(v_r) & (v_R \le v \le v_F) \\
0 & (v < v_c \text{ and } v > v_F)
\end{cases}$$

The energy production of the wind turbine WE(t) over time t can thus be calculated as

$$WE(t) = \overline{P_{WTA}}t$$

Another way of stating the energy output from a wind turbine is to look at the capacity factor for the turbine in its particular location. The capacity factor CF, is the actual energy output over a given period of time, WE(t), divided by the theoretical maximum energy output (i.e. this means that the machine is constantly running at its rated output) during the selected time-span, RO(t). This can be formulated as

$$CF = \frac{WE(t)}{RO(t)}$$

Theoretically capacity factor vary from 0 to 100%. In practice they usually range from 20 to 70% and mostly be around 20-30 percent. However, the economic feasibility of a wind turbine does not of course depend on the capacity factor of a wind turbine alone but also depends on the costs of alternative power systems. Therefore, a low capacity factor does not automatically render a wind turbine project unfeasible.

In order to maximize the energy output of a given wind regime the optimum wind speed, v_{opt} , needs to be determined. The optimum wind speed indicates at what wind velocity most energy is available in a given wind regime. It is at this particular wind speed that engineers should ensure that the power coefficient is most efficient to allow for the highest energy conversion of a turbine. The optimum wind speed can be calculated as follows (Lu et al., 2002):

$$v_{opt} = c \left(\frac{k+2}{k}\right)^{\frac{1}{2}}$$

In this regard, the power density of a turbine is a good comparative indicator to show the average power output per m^2 of wind swept area, A, at a given site. This can be defined as

Power Density =
$$\frac{\overline{P_{WTA}}}{A}$$

Another important aspect of that critically determines the energy output of a turbine is elevation. In many cases the available recorded wind speed data has been measured at a lower level than the planned hub height of the wind turbine. As wind velocity increases vertically the recorded wind speed data can be adjusted using the following standard formula (Borowy and Salameh, 1996.) where ν is the projected wind speed, ν_i the wind speed at reference height, H the hub height of a turbine, Hi the reference height and α the power-law exponent.

$$v = v_i \left(\frac{H}{H_i}\right)^{\alpha}$$

 α is often quoted to have a value of 1/7 and is seen as a reasonable power law exponent for even and unobstructed landscapes. However, where WECT development is planned either offshore or near woodlands or close to any other non flat terrains this value can differ subsequently and a more through analysis of α is necessary. Justus as well as Counnihan offer mathematical solution for 'fitting' α to these environments (Manwell et al., 2002).

4.1 Hypothetical Wind Generated Electric Power:

A **wind turbine** is a machine for converting the kinetic energy in wind into mechanical energy. If the mechanical energy is used directly by machinery, such as a pump or grinding stones, the machine is usually called a windmill. If the mechanical energy is then converted to electricity, the machine is called a wind generator.

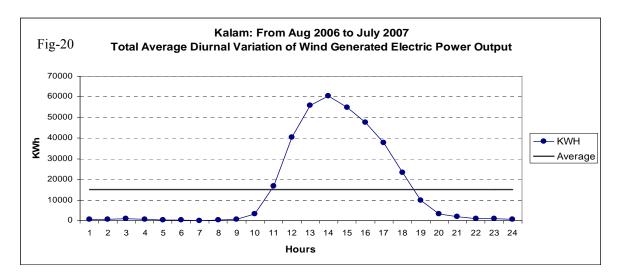
Hypothetical wind generated electric power output at Kalam has been estimated by using the 600KW wind turbine bonus 600/44 MK IV type. The cut in wind speed of this turbine is 3m/s and cutout wind speed is 25m/s. Rotor diameter of this turbine is 44 meters and hub height has been taken as 50 meters. The monthly and annual wind generated electric power outputs at Kalam are shown below in graphs and table-4.

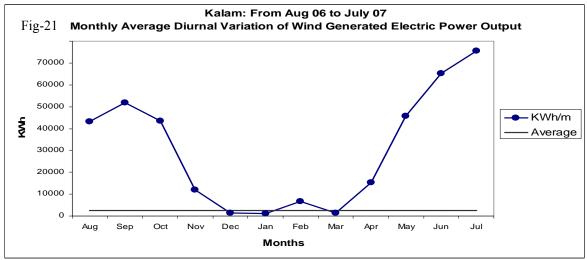
Table-4: Hypothetical wind generated electric energy output & capacity Factor for a Bonus 600/44MK IV Turbine at Kalam.

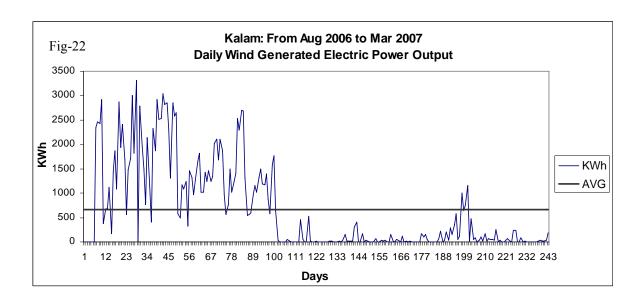
	PMD (Calculator (usin	g 50M)	
Month	Input W/m ²	Output W/m ²	C.F.	KWh / Month
January	2	1	0%	578
February	27	7	2%	7,266
March	3	1	0%	1,085
April	55	15	4%	16,115
May	150	25	6%	28,604
June	309	42	11%	45,571
July	345	48	12%	53,733
August	236	36	9%	40,438
September	238	34	9%	37,026
October	187	28	7%	31,377
November	57	10	2%	10,581
December	3	1	0%	829
Annual	81	18	5%	240,300

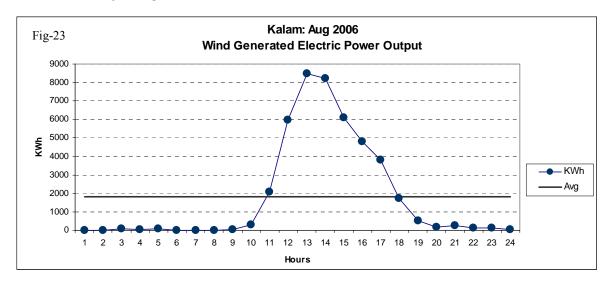
Wind Turbine spec	eification
Turbine	Bonus 600 / 44 MK IV
Power	600 KW
Cut in Wind	3 m/s
Cut out wind	25 m/s
Rotor Diameter	44 m
Hub height	50 m

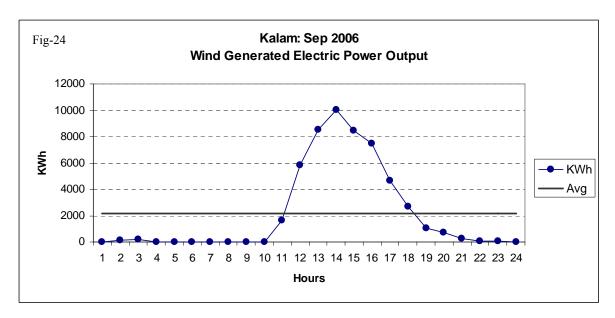
Figure 20 shows the average diurnal variation of wind generated electric energy output at Kalam (Aug-July). The graph shows that the maximum power is produced at about 1 PM; of course, this is the same time when we have the maximum wind speed in 24 hours. Figure 21 & 22 shows the monthly and daily wind generated electric power output. Figure 21 depicts that at Kalam the wind have more potential in the month of September as compared to other months. Figure 23 to 34 shows the monthly average diurnal variation of wind generated electric energy output.

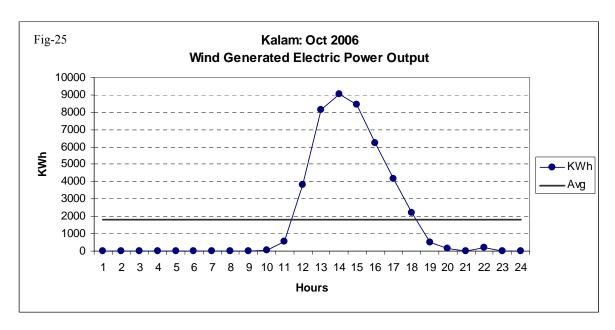


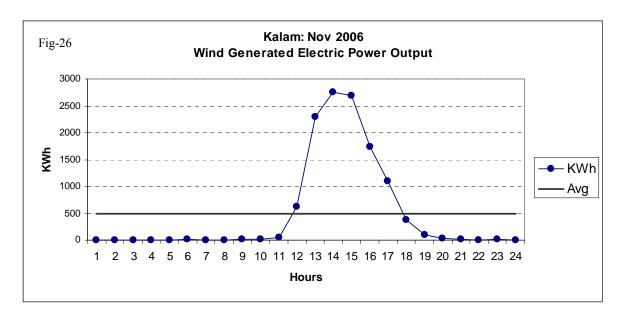


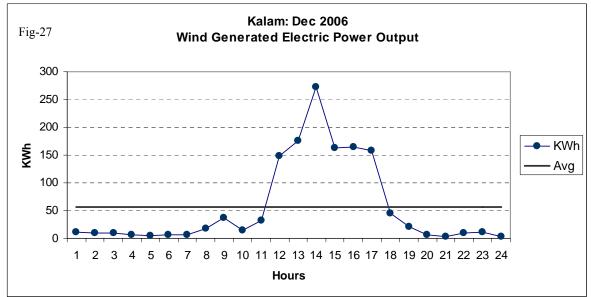


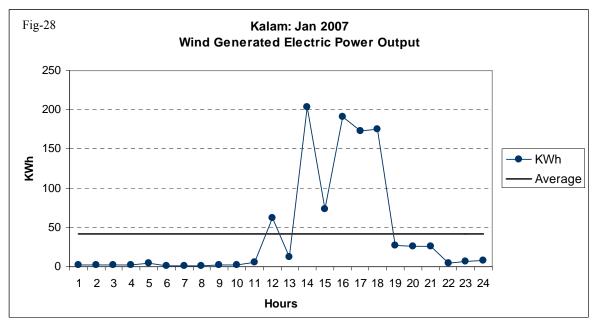


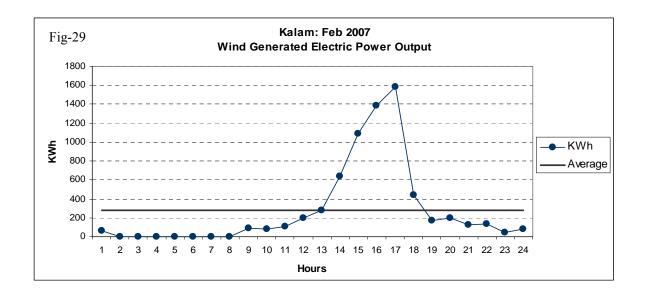


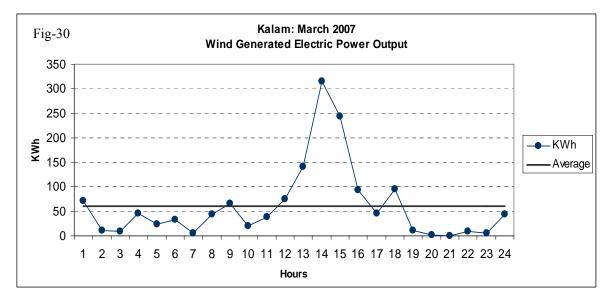


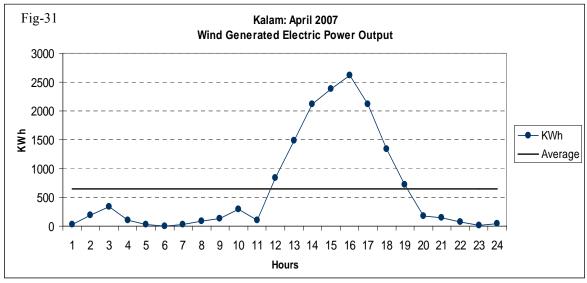


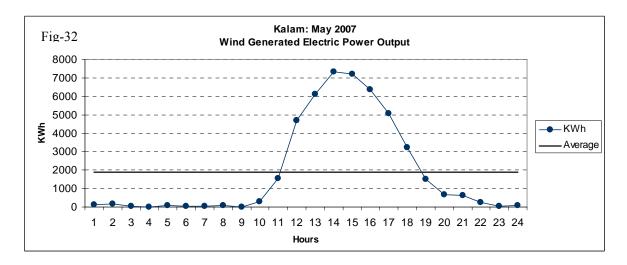


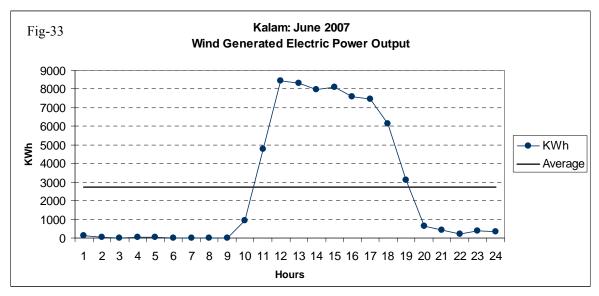


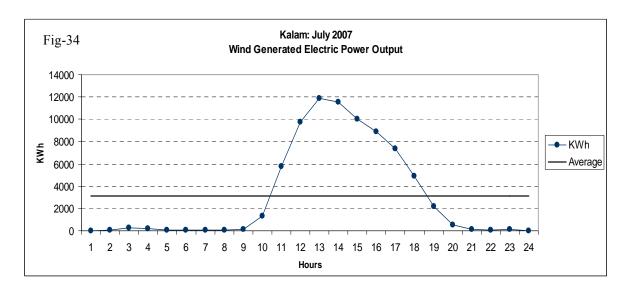








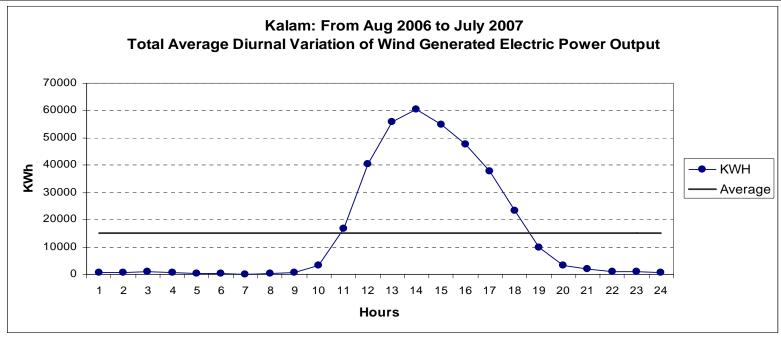




Appendix-I

Majajji Aug 2000 to July 2007 wind Power Output of Bonus 600/44 Turbine (12 Month & Summa	Kalam	Aug 2006 to July 2007	Wind Power Output of Bonus 600/44 Turbine (12 Month's Summary
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Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
Aug-06	20	11	92	57	79	18	3	6	43	318	2070	5981	8470	8241	6119	4822	3821	1747	498	173	264	119	112	56	43143
Sep-06	29	153	190	21	3	4	2	1	0	18	1671	5849	8517	10064	8454	7458	4649	2688	1078	708	254	40	86	28	51966
Oct-06	1	1	3	2	1	1	1	9	17	45	578	3831	8164	9047	8436	6223	4195	2215	497	134	23	188	4	2	43619
Nov-06	1	0	2	0	1	14	6	1	24	10	44	626	2295	2756	2692	1745	1101	376	104	33	23	5	18	7	11886
Dec-06	12	9	10	7	5	7	6	18	36	15	32	148	176	273	163	164	158	45	21	6	3	9	11	3	1336
Jan-07	2	2	3	2	4	2	1	1	2	2	5	62	12	204	74	192	173	176	27	26	26	5	7	8	1017
Feb-07	61	0	3	1	2	1	1	4	86	79	109	196	277	639	1088	1387	1581	442	169	195	123	135	47	78	6703
Mar-07	72	10	9	46	24	32	6	45	67	19	38	74	141	315	244	94	46	96	11	2	1	9	5	44	1452
Apr-07	37	195	340	96	26	5	35	92	127	297	100	833	1488	2121	2380	2612	2119	1344	715	176	142	78	21	41	15420
May-07	133	156	35	6	75	36	32	103	9	307	1544	4699	6116	7339	7194	6360	5050	3245	1519	666	611	246	57	100	45638
Jun-07	107	48	21	62	23	13	5	1	18	950	4793	8435	8329	7983	8125	7598	7469	6158	3127	646	409	200	400	352	65274
Jul-07	21	50	271	203	78	43	50	49	139	1359	5800	9768	11870	11562	10041	8869	7359	4923	2177	554	166	63	108	32	75556
KWH	496	636	977	503	322	175	147	331	568	3419	16784	40503	55857	60544	55012	47523	37722	23455	9943	3321	2044	1100	875	753	363010
Average	15125	15125	15125	15125	15125	15125	15125	15125	15125	15125	15125	15125	15125	15125	15125	15125	15125	15125	15125	15125	15125	15125	15125	15125	



Appendix-II

Kalan	1	Au	gust 2	2006			Wii	nd F	owe	er Out	put o	f Bon	us 60	0/44 T	urbin	e (Mo	nth's	Sumn	nary)					
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	12.2	126.0	270.9	506.2	501.4	360.7	187.2	127.5	38.9	29.2	90.7	39.9	6.6	47.9	2345
8	2.8	0.9	86.6	24.1	0.1	0.0	0.0	0.0	0.0	2.5	107.8	338.4	566.8	548.5	468.1	236.1	72.4	1.0	0.2	0.0	0.0	0.0	0.0	0.0	2456
9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.2	96.4	127.8	405.5	574.4	354.3	380.0	303.6	85.1	71.5	29.8	0.0	0.0	0.0	0.1	2431
10	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	64.8	252.7	370.5	464.1	570.5	551.9	350.4	165.6	92.2	29.8	10.4	0.0	0.0	0.0	0.0	2923
11	0.0	0.0	0.0	29.8	1.2	0.1	0.1	0.2	2.1	0.1	0.7	45.9	44.6	60.9	111.6	53.8	28.5	0.7	0.2	0.3	0.1	0.6	0.0	0.0	381
12	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.7	170.2	81.7	4.1	30.7	67.0	122.0	41.3	0.0	46.3	115.5	5.1	0.0	0.0	686
13	0.0	0.0	2.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	23.9	83.5	132.7	95.1	52.4	39.0	196.0	49.8	3.6	0.0	0.1	0.0	3.3	0.0	682
14	0.0	0.0	0.0	0.0	2.6	0.1	0.1	0.0	0.0	0.0	23.4	403.4	446.9	104.5	0.7	31.4	9.5	14.0	0.0	0.0	0.4	15.4	66.3	2.4	1121
15	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	1.0	9.4	11.3	0.7	0.3	9.4	15.8	97.1	20.7	1.2	1.1	0.0	0.0	0.0	0.0	168
16	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.6	355.9	470.5	380.5	171.8	34.7	1.1	5.5	21.5	0.0	0.0	0.0	0.3	0.0	1445
17	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	231.5	532.7	503.5	314.0	104.8	142.6	32.9	3.4	0.0	0.0	0.0	0.0	0.0	1866
18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	11.4	60.6	118.5	103.9	187.1	365.1	168.2	66.0	10.6	1.2	0.0	0.0	0.0	0.0	0.0	1093
19	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.2	52.4	188.8	423.8	540.1	520.3	515.6	317.1	232.9	69.1	6.6	0.0	0.0	1.4	3.6	2874
20	0.0	0.0	0.5	0.0	0.0	0.0	0.0	0.0	39.8	153.8	322.0	481.5	436.3	324.5	129.0	43.9	2.4	0.0	0.4	3.0	0.5	0.0	0.0	0.0	1938
21	0.0	0.5	0.9	0.0	0.0	0.0	0.0	0.0	0.0	22.3	207.9	385.0	440.9	384.6	251.9	336.8	211.0	139.3	36.9	2.1	0.2	0.0	0.0	0.0	2421
22	0.0	0.0	0.0	1.9	69.7	17.4	1.3	0.0	0.0	0.0	60.0	106.7	177.2	420.5	358.8	288.4	165.6	8.2	0.1	0.0	0.0	0.0	0.0	0.0	1676
23	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	7.3	69.7	183.1	231.5	13.2	2.3	16.5	24.2	1.6	0.9	0.4	2.1	0.5	0.0	553
24	9.2	9.7	1.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5.2	207.4	396.5	400.0	281.7	117.3	47.7	3.3	0.0	0.4	0.0	0.0	0.0	0.0	1480
25	0.0	0.0	0.0	0.1	1.1	0.3	0.1	0.0	0.0	0.1	170.8	426.5	492.0	320.9	120.4	75.2	68.4	33.1	5.1	0.1	0.0	0.0	0.0	0.0	1714
26	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	10.1	60.7	321.0	525.6	545.4	434.5	395.2	418.5	231.9	61.3	4.8	0.1	0.0	0.0	0.0	3009
27	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.3	52.3	289.2	321.0	240.0	17.1	269.1	450.6	156.4	14.7	2.9	0.4	0.0	0.0	0.0	1814
28	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	46.8	423.4	530.7	493.1	344.0	367.5	305.9	361.8	184.2	71.4	31.5	55.7	56.4	33.3	0.9	3307
29	0.1	0.0	0.0	0.7	4.6	0.0	1.6	6.2	8.0	0.0	0.0	0.0	0.0	1.3	0.0	0.3	0.6	0.1	2.0	0.1	0.0	0.0	0.0	1.3	20
30	7.5	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	3.6	169.2	524.5	487.0	470.8	458.4	366.0	251.2	40.9	0.6	0.0	0.0	0.0	0.0	2780
31	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	111.3	422.2	535.5	466.1	222.6	172.1	2.9	1.3	23.5	3.4	0.0	0.0	0.0	0.0	1961
KWh	20	11	92	57	79	18	3	6	43	318	2070	5981	8470	8241	6119	4822	3821	1747	498	173	264	119	112	56	43143

Kalan	n	Se	ptembe	er 200	6		Wir	nd F	ow	er C	utput	of Bo	nus 60	00/44 T	urbin	e (Mor	nth's S	umma	ary)						
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	10.4	54.5	185.9	19.3	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	17.2	126.8	312.4	311.8	207.0	184.9	57.7	11.2	0.5	0.7	0.4	0.8	1502
2	0.4	0.0	0.5	0.8	0.5	3.9	1.7	0.6	0.0	0.0	0.2	13.4	191.5	283.1	177.8	20.5	37.7	1.6	0.0	0.0	3.5	7.3	16.8	0.0	762
3	0.0	10.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	25.9	336.2	527.4	395.1	293.9	205.2	72.5	4.2	43.0	203.5	15.6	1.5	0.1	4.8	2139
4	0.7	0.3	0.1	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	11.7	194.2	228.8	403.9	296.3	9.6	3.2	0.0	0.0	0.0	0.1	0.0	1149
5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6	44.7	81.9	27.9	32.5	95.7	91.6	31.5	0.0	0.0	0.0	0.0	0.0	0.0	406
6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	19.7	384.8	535.5	558.3	437.6	236.0	128.8	27.5	0.3	0.0	0.0	0.0	0.0	2328
7	0.0	0.0	0.1	0.0	0.1	0.0	0.0	0.0	0.0	0.0	76.7	278.6	371.4	344.6	304.1	204.2	179.9	75.2	33.5	8.0	0.0	0.0	0.0	0.0	1876
8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	102.1	271.4	383.6	553.1	565.9	539.4	344.1	102.5	42.0	15.3	0.0	0.0	0.0	0.0	2919
9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	213.5	365.1	564.7	553.5	339.9	197.0	159.6	101.5	22.0	1.3	0.4	0.0	0.0	0.0	2519
10	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6	64.8	432.7	456.4	412.0	271.9	407.1	260.0	174.4	47.6	8.0	0.0	0.0	0.0	0.0	2535
11	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	20.1	313.0	528.4	547.2	515.5	539.8	373.4	145.5	9.9	19.8	0.1	0.0	0.0	21.3	3034
12	13.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	7.5	256.4	501.0	559.4	405.8	364.3	299.6	121.5	263.3	31.5	5.3	0.0	0.0	0.0	0.0	2829
13	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.0	226.9	470.6	476.3	500.3	473.7	295.8	198.4	86.4	92.9	35.7	0.0	0.0	1.8	0.0	2861
14	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	132.0	531.6	511.9	510.0	373.9	191.6	62.3	0.4	0.0	0.0	0.0	0.0	0.0	0.0	2314
15	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	215.2	363.3	247.8	386.4	101.8	0.0	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.0	1315
16	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	9.2	370.7	499.3	503.2	445.1	492.7	340.1	174.7	15.1	0.1	0.0	0.0	0.0	0.5	2851
17	0.1	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	7.5	206.0	326.4	468.3	476.9	451.1	275.0	212.6	87.0	79.2	0.4	0.0	0.0	0.0	0.0	2591
18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	48.4	335.7	433.0	522.5	424.3	393.8	279.9	156.2	44.4	4.2	8.7	0.1	0.1	0.0	2651
19	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	29.9	73.0	75.4	373.6	18.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	570
20	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	33.8	117.2	65.6	130.3	97.3	19.1	30.8	0.1	1.4	0.2	0.3	0.1	0.0	0.0	496
21	0.0	0.0	0.0	0.1	1.4	0.0	0.0	0.0	0.0	0.0	0.2	0.0	0.3	40.3	7.9	111.8	240.7	425.7	157.8	115.4	66.6	5.0	0.0	0.5	1174
22	0.0	83.1	1.9	0.0	0.1	0.2	0.0	0.1	0.0	0.0	0.0	0.1	183.4	377.6	259.3	157.6	11.5	1.3	16.2	0.0	0.0	0.2	0.0	0.0	1093
23	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	7.0	238.5	274.0	101.1	69.7	161.9	57.0	214.6	58.1	20.9	44.7	0.4	0.1	0.0	1248
24	0.1	1.2	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	2.3	26.5	3.1	18.3	71.0	183.9	10.4	11.8	0.1	0.0	0.4	0.0	0.1	0.0	329
25	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	10.9	89.6	356.4	289.3	209.1	48.6	21.5	194.7	115.3	32.5	18.8	66.6	0.0	1453
26	4.3	3.5	0.0	0.5	0.3	0.0	0.0	0.0	0.0	0.0	0.0	17.2	43.0	303.4	529.7	331.2	90.5	0.0	1.7	0.3	0.9	1.0	0.0	0.0	1327
27	0.0	0.4	1.2	0.6	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	147.6	202.2	227.5	175.7	135.9	73.1	9.5	0.0	0.0	0.0	0.0	0.1	974
28	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	146.6	462.1	300.8	54.1	144.9	141.0	2.1	0.0	0.0	0.0	0.0	0.0	0.0	1252
29	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	222.6	291.3	279.0	296.1	321.3	151.9	78.6	8.9	0.7	0.0	0.0	0.0	0.0	1651
30	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	22.6	166.4	302.6	298.9	331.1	257.0	131.1	80.2	142.2	79.6	5.4	0.0	0.1	1817
KWh	29	153	190	21	3	4	2	1	0	18	1671	5849	8517	10064	8454	7458	4649	2688	1078	708	254	40	86	28	51966

Kalam)	Oct	ober 2	2006			Wir	nd P	owe	Out	put of	Bonu	s 600/	44 Tur	bine (I	Month'	's Sun	nmary)							
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	0.4	0.6	8.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.0	99.4	184.2	281.5	201.2	61.6	7.1	0.4	0.4	0.0	0.0	172.9	3.9	1.1	1016
2	0.3	0.0	1.3	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	244.0	262.8	202.2	107.1	120.2	68.5	3.9	4.4	0.0	0.1	0.1	0.4	1016
3	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.9	272.8	402.9	319.2	203.8	177.8	40.9	1.4	0.0	0.0	0.0	0.0	0.0	1421
4	0.0	0.0	0.1	0.6	0.2	0.2	0.1	0.0	0.0	0.0	0.0	0.2	0.3	245.0	350.0	304.6	233.0	109.9	1.1	0.4	0.0	0.0	0.0	0.0	1246
5	0.0	0.0	0.0	8.0	0.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	20.8	286.7	369.9	434.3	223.4	110.2	10.1	0.0	0.0	0.0	0.0	0.0	1456
6	0.0	0.0	0.0	0.0	0.1	0.1	0.4	1.2	0.0	0.0	0.5	14.5	37.3	223.7	356.5	247.0	175.7	167.8	10.7	0.0	0.0	0.0	0.0	0.0	1235
7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	175.4	418.3	210.9	175.4	107.5	231.9	18.6	0.1	0.0	0.0	0.0	0.0	0.0	1338
8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	31.7	277.4	421.7	236.5	230.6	279.8	224.3	200.5	101.4	18.0	0.0	0.0	0.0	0.0	2022
9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.3	340.2	531.3	350.4	267.6	327.6	228.1	52.3	2.4	0.1	0.0	0.0	0.0	0.0	2103
10	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	20.4	327.9	409.7	340.4	376.5	122.8	31.4	51.6	0.0	0.0	0.0	0.0	0.0	0.0	1681
11	0.0	0.0	0.1	0.1	0.0	0.0	0.2	0.0	0.0	0.0	0.0	120.7	417.9	392.9	388.0	349.5	241.9	165.0	31.7	0.0	0.0	0.0	0.0	0.0	2108
12	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	11.4	372.2	318.2	317.5	264.9	248.5	227.5	109.9	0.9	1.6	0.0	0.0	0.0	0.0	1873
13	0.1	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	30.6	108.2	84.0	173.9	233.2	67.8	31.0	205.6	27.7	1.2	1.7	0.0	0.0	0.0	965
14	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	10.9	277.5	235.9	31.2	0.0	0.1	0.0	0.2	0.0	0.0	0.0	0.0	0.0	556
15	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.5	148.6	197.7	155.9	117.3	75.0	57.0	1.8	0.0	0.0	0.0	0.0	0.0	0.0	758
16	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	205.9	327.2	400.8	267.5	198.8	96.2	0.0	0.0	0.0	0.0	0.0	0.0	1497
17	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	58.1	230.7	139.5	210.8	144.7	33.6	168.8	30.0	0.0	0.0	0.3	0.0	0.0	1017
18	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	10.5	212.1	426.7	282.5	242.7	53.0	4.3	0.1	0.0	0.0	0.0	0.0	0.0	1232
19	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.0	0.0	28.7	433.6	281.1	162.2	155.7	141.6	201.3	2.2	0.0	0.0	0.0	0.0	0.0	0.0	1407
20	0.0	0.0	0.0	0.0	0.0	0.0	0.0	7.4	15.7	45.1	265.4	369.0	495.8	471.3	454.3	219.8	107.6	54.4	24.5	2.5	0.5	0.0	0.0	0.0	2533
21	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	8.0	165.9	468.9	548.6	519.5	357.6	192.0	26.0	8.7	0.0	0.0	0.0	0.0	0.0	2295
22	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	139.6	407.6	415.4	464.0	406.9	365.7	367.5	114.4	20.0	0.5	0.0	0.0	0.0	0.0	2702
23	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	31.9	224.1	438.1	537.5	408.1	410.9	334.9	226.9	33.7	32.0	0.0	0.0	0.0	0.0	2678
24	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.9	5.3	177.9	169.8	365.4	263.3	117.4	31.2	73.7	73.7	21.0	14.8	0.3	0.0	1316
25	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	18.5	13.9	53.1	162.3	72.3	114.7	111.5	0.0	0.0	0.0	0.0	0.0	546
26	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	105.5	279.7	58.0	38.1	69.4	5.0	0.8	0.0	0.0	0.0	0.0	0.1	0.0	557
27	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	48.4	228.8	126.1	121.2	62.3	9.9	0.4	0.0	0.0	0.0	0.0	0.0	0.0	597
28	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5.9	297.4	243.7	129.4	140.2	116.9	28.0	2.6	0.0	0.0	0.0	0.0	0.0	964
29	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	108.7	391.0	355.2	182.6	91.6	18.0	0.1	0.0	0.0	0.0	0.0	0.0	1147
30	0.0	0.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	162.9	393.9	291.3	121.7	42.6	7.7	0.4	0.0	0.0	0.0	0.0	0.0	1021
31	0.0	0.0	0.1	0.0	0.1	0.1	0.4	0.1	8.0	0.0	0.0	0.0	306.3	456.8	360.5	133.8	40.3	18.3	0.3	0.0	0.0	0.0	0.0	0.0	1318
KWh	1	1	3	2	1	1	1	9	17	45	578	3831	8164	9047	8436	6223	4195	2215	497	134	23	188	4	2	43619

Kalam	1	Nove	mber	2006			Win	d Po	ower	Out	put o	f Bonu	s 600/4	4 Turb	ine (M	onth's	Summ	ary)							
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4	1.9	115.6	299.3	466.0	366.4	158.9	36.0	38.2	8.7	0.0	0.0	0.0	0.0	0.0	1491
2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	44.4	199.0	174.3	197.1	205.8	314.8	55.5	0.1	0.0	0.0	0.0	0.0	0.0	1191
3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	240.2	408.0	294.7	177.3	41.4	3.2	0.0	0.0	0.0	0.0	0.0	0.1	1165
4	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	35.9	391.9	468.5	348.9	97.9	36.0	22.0	0.0	0.0	0.0	0.0	0.0	0.0	1401
5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	101.9	345.7	143.2	219.5	49.2	5.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	865
6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	22.2	0.0	0.0	234.6	160.6	55.2	53.3	25.9	19.4	0.0	0.0	0.1	0.1	0.0	0.0	0.0	571
7	0.0	0.0	0.0	0.0	0.0	0.2	0.0	0.0	0.0	0.0	0.0	51.6	366.8	442.3	398.1	252.9	54.7	13.7	0.0	0.0	0.0	0.0	0.0	0.0	1580
8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	41.0	188.5	341.0	394.0	372.0	291.6	111.2	32.5	0.0	0.0	0.0	0.0	0.0	1772
9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	44.0	124.4	110.5	185.4	114.3	62.7	12.0	0.0	0.0	0.0	0.0	0.0	653
10	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.2	0.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	18.2	0.1	0.1	0.5	5.9	2.9	0.0	0.0	29
11	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.8	3.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.5	5
12	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	2.2	0.0	0.9	0.5	0.3	2.6	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	7
13	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.9	1.2	2.4	0.4	0.9	0.2	1.1	0.1	0.0	0.0	0.0	7
14	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.3	0.1	0.0	0.0	0.1	0.3	0.0	0.0	1
15	0.2	0.1	0.0	0.1	0.5	12.4	5.7	0.1	0.0	0.0	0.0	0.0	0.3	0.3	16.4	10.5	6.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	53
16	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.1	0.0	3.4	0.1	1.0	6.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	11
17	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.7	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2
19	0.0	0.0	0.0	0.0	0.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	1
20	0.0	0.0	0.0	0.0	0.1	1.2	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.0	0.0	0.3	0.0	0.0	0.0	1.8	4
21	0.0	0.1	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.1	2.6	0.0	0.0	2.5	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	6
22	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	48.5	127.0	128.8	19.1	36.5	0.1	46.3	30.7	16.4	1.6	1.9	0.0	457
23	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	1.5	5.4	19.7	0.1	0.0	0.2	0.1	7.2	0.7	0.0	0.0	0.0	0.0	0.0	15.8	4.9	56
24	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.4	0.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1
25	0.0	0.0	0.1	0.2	0.1	0.0	0.1	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1
26	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	15.2	0.0	0.1	4.1	160.6	156.6	110.7	68.0	4.0	0.0	0.0	0.0	0.1	0.1	519
27	8.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.3	7.2	1.5	0.1	0.0	0.0	0.0	0.0	0.0	0.1	10
28	0.3	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3
29	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.1	0.0	0.2	0.0	0.3	0.2	0.0	1
30	0.0	0.0	0.7	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	10.4	9.3	0.0	0.0	0.3	0.0	0.0	0.0	0.0	21
KWh	1	0	2	0	1	14	6	1	24	10	44	626	2295	2756	2692	1745	1101	376	104	33	23	5	18	7	11886

Kalam	1	Dece	mber	2006			Win	d Po	wer C	utpu	ut of E	onus 6	00/44 T	urbine	(Mont	h's Sเ	ımma	ry)							
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.2	0.0	0.0	0
2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.1	0.0	2.4	1.7	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5
3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	1.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1
6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
7	0.1	4.7	7.8	3.0	0.2	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.0	0.4	0.1	0.0	0.0	0.0	0.0	0.9	3.0	0.4	25
8	0.6	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.3	0.0	0.9	0.4	3.0	6.1	0.3	12
9	0.0	0.1	0.1	0.4	0.1	0.0	0.0	0.5	0.1	0.0	0.0	0.1	0.2	0.0	0.0	0.9	0.4	0.1	0.0	0.1	0.0	1.9	0.0	0.0	5
10	8.0	0.0	0.1	0.0	0.0	0.0	0.1	0.5	0.2	0.0	0.0	0.0	0.0	0.0	0.9	0.2	0.0	0.6	0.1	0.0	0.0	0.0	0.0	0.0	4
11	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.1	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.0	0.1	1
12	0.1	0.1	0.0	0.0	0.0	0.4	0.1	0.4	0.0	0.0	0.0	0.0	0.0	0.0	9.7	1.7	0.0	0.0	0.0	0.1	0.1	0.0	0.3	0.5	13
13	0.0	0.2	0.1	0.0	0.4	0.0	0.1	0.0	0.0	0.0	0.3	0.1	0.0	0.1	0.0	0.2	2.2	0.0	0.0	0.0	0.1	0.1	0.0	0.0	4
14	0.0	0.0	0.0	0.0	1.0	0.1	0.7	2.3	26.8	0.1	0.0	0.0	0.0	0.0	0.1	0.3	0.0	0.0	0.0	0.1	0.0	0.1	0.3	0.3	32
15	0.1	0.2	0.1	0.1	3.4	1.3	4.0	1.3	1.5	9.0	3.6	14.3	0.7	79.3	4.1	21.2	7.3	0.0	0.1	2.3	0.0	0.0	0.0	0.0	154
16	0.3	0.1	0.1	0.0	0.0	0.0	0.0	0.0	1.7	4.0	0.0	0.1	0.0	0.0	0.0	0.4	0.0	0.4	0.1	0.6	8.0	0.0	0.0	0.1	9
17	0.0	0.0	0.5	0.1	0.0	0.0	0.4	5.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	2.1	0.0	0.1	1.9	0.1	0.1	11
18	0.1	0.1	0.0	0.0	0.0	0.5	0.0	5.1	1.6	0.4	0.1	0.0	0.1	0.2	0.2	1.4	0.3	0.3	7.3	1.6	0.0	0.0	0.1	0.0	19
19	1.0	0.1	0.1	0.0	0.2	0.0	0.1	0.2	0.0	0.0	0.0	0.0	0.0	0.3	7.9	3.7	1.8	0.2	0.1	0.1	0.2	1.0	0.5	0.5	18
20	8.0	0.0	0.2	0.0	0.0	3.7	1.0	0.4	3.6	0.1	2.5	0.3	4.7	132.8	90.2	54.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	302
21	0.3	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	18.0	127.7	161.3	3.0	0.0	0.0	99.6	0.2	0.0	0.0	0.0	0.0	0.0	0.0	410
22	0.1	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.3	0.0	0.0	0.0	0.0	0.0	0.0	0.2	1
23	0.1	1.1	0.0	0.4	0.0	0.5	0.0	0.0	0.0	1.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3
24	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	6.1	0.1	0.0	0.0	7.6	64.4	45.8	42.2	11.1	0.7	0.3	0.0	0.0	0.0	178
25	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
26	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.5	5.2	19.8	5.6	3.9	0.1	0.1	0.0	0.0	0.0	0.0	0.4	0.1	36
27	0.3	0.7	8.0	1.6	0.0	0.1	0.1	0.1	0.4	0.0	0.0	0.0	0.0	0.0	0.0	10.6	0.4	0.1	0.1	0.1	0.7	0.1	0.1	0.1	16
28	0.0	1.7	0.1	0.0	0.0	0.0	0.0	0.9	0.1	0.1	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3
29	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.5	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5
30	0.0	0.0	0.5	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	1
31	0.0	0.1	0.0	1.1	0.0	0.0	0.0	0.0	0.5	0.1	0.0	0.1	1.3	35.1	30.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	68
KWh	12	9	10	7	5	7	6	18	36	15	32	148	176	273	163	164	158	45	21	6	3	9	11	3	1336

Kalam	1	Janu	uary 2	007			Wind	d Po	wer (Outp	ut of	Bonu	s 60	0/44 Tu	rbine ((Month	n's Sur	nmary	')						
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	0.0	0.0	0.0	0.5	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	2.4	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3
2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.1	0.5	0.0	0.0	2
3	0.0	0.0	0.0	0.0	0.5	0.0	0.1	0.2	0.4	0.0	1.2	25.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6	0.1	0.7	0.1	29
4	0.1	0.1	0.4	0.1	0.0	0.0	0.1	0.0	0.4	0.4	8.0	3.0	0.0	0.0	0.0	15.4	3.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	24
5	0.0	0.0	0.0	0.0	1.3	0.4	0.0	0.0	0.1	0.0	8.0	0.8	0.0	22.8	4.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.8	0.5	32
6	0.4	0.1	0.5	0.1	0.0	0.0	0.0	0.0	0.0	0.0	1.0	0.0	0.0	0.4	1.7	2.2	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.5	7
7	0.1	0.1	0.0	0.0	0.5	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.0	0.0	0.0	0.0	0.3	0.5	2
8	0.0	0.1	0.1	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.0	0.1	0.0	0.2	3.6	51.1	81.5	11.7	0.5	0.0	0.1	0.5	0.8	150
9	0.1	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.3	21.4	3.3	0.1	0.0	0.0	0.0	0.0	0.0	25
10	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.1	1.4	1.2	3
11	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.3	0.1	0.0	19.7	20.8	2.3	0.0	0.1	44
12	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	26.3	0.5	0.3	1.6	0.3	0.0	0.0	0.0	0.0	0.0	29
13	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.1	0
14	0.0	0.0	0.1	0.1	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.2	44.1	17.2	41.2	12.6	0.0	0.1	0.0	0.0	0.0	117
15	0.0	0.0	1.4	0.0	0.1	0.4	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.3	0.1	0.0	0.1	0.0	0.0	0.0	0.0	0.0	2
16	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	3.5	0.0	19.8	0.0	0.0	0.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	24
17	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
18	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.2	0.4	0.0	0.0	0.4	6.1	15.4	1.7	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	24
19	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.0	0.0	0.0	0.0	0.0	0.1	1.0	0.9	2
20	0.1	0.4	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.1	0.2	1.7	3
21	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.3	0.1	0.1	1.0	0.7	0.5	0.1	1.0	0.6	5
22	0.6	0.0	0.0	0.0	0.0	0.1	0.0	0.7	0.3	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.1	0.1	0.0	0.2	0.9	0.6	0.0	4
23	0.1	0.1	0.1	0.0	0.1	0.0	0.1	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.3	0.0	1
24	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.4	1.4	29.2	7.1	22.6	11.0	66.6		0.1	0.0	0.3	0.0	0.0	0.0	0.0	165
25	0.1	0.0	0.1	0.1	0.0	0.1	0.2	0.0		0.1	0.0	0.0	0.0	0.0	0.1	26.7	28.5	40.9	1.0	3.0	0.2		0.1		101
26	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0			0.0	0.0	4.9	131.9		3.7	0.8	0.0	0.0	0.1	0.0		0.0		153
27	0.1	0.6	0.0	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0		25.0	20.7	4.4	0.0	0.0	0.1		0.0		51
28	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.0	0.1	0
29	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0		0.8	2.9	2.3	0.2	0.0	0.9		0.0		7
30	0.0	0.1	0.0	0.0	0.0	0.1	0.1	0.0	0.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.3	0.1	0.0	0.1	1
31	0.0	0.1	0.1	0.7	1.6	0.1	0.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	1.4	1.4	0.2	0.1	0.4	7
KWh	2	2	3	2	4	2	1	1	2	2	5	62	12	204	74	192	173	176	27	26	26	5	7	8	1017

Kalar	n	Febr	uary 2	2007			Win	ıd P	ower	Outp	out of	Bonu	s 600/	44 Tur	bine (N	/lonth's	s Sum	mary)							
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	0.1	0.3	0.5	0.0	0.1	0.0	0.0	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.3	0.0	0.1	0.0	1
2	0.1	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.3	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.3	71.4	0.1	0.0	73
3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	19.3	156.3	30.5	7.9	0.0	0.0	215
4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
5	0.0	0.0	0.4	0.0	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.1	0.3	1.7	0.3	17.7	11.2	0.0	0.0	33
6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	75.2	68.2	47.1	9.7	0.8	0.0	0.0	0.0	0.0	0.0	0.0	201
7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	12.1	25.3	1.2	0.0	0.0	0.0	0.0	0.0	0.0	0.2	39
8	0.0	0.0	0.2	0.0	0.0	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	67.9	99.1	49.4	17.8	0.2	0.0	0.0	0.0	0.0	53.2	288
9	18.4	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	4.1	0.8	0.0	64.4	67.9	0.5	0.9	0.0	0.0	0.0	0.0	0.0	157
10	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.7	117.5	82.0	0.0	155.1	1.4	0.0	0.0	1.5	0.3	0.0	0.0	359
11	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.0	82.4	73.5	59.6	149.3	107.9	15.8	0.1	0.0	0.0	9.7	40.0	7.9	0.3	9.6	10.1	4.0	574
12	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	6.1	31.4	9.0	1.3	0.0	5.2	2.6	0.0	0.0	0.0	0.0	0.0	0.0	56
13	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.5	0.1	3.5	74.3	31.9	2.8	0.1	0.0	0.0	0.0	0.0	0.0	113
14	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.3	45.6	170.9	299.3	140.6	151.5	51.1	36.9	0.7	11.1	33.9	36.0	19.8	999
15	2.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	70.9	109.4	280.9	122.8	45.4	17.0	0.0	0.0	0.0	0.0	649
16	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.0	0.0	0.0	9.6	25.6	96.5	195.0	331.2	54.3	20.6	9.2	0.6	0.0	0.0	0.0	743
17	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	34.4	68.8	194.7	318.9	306.8	195.7	35.4	0.7	0.0	0.0	0.0	0.0	0.0	1155
18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.2	1.4	3.0	15.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	21
19	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.0	1.0	2.6	4.3	50.3	265.5	136.5	21.6	0.0	0.0	0.0	0.0	0.0	0.0	482
20	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.1	3.4	0.3	0.4	0.0	0.0	0.5	5.0	11.3	13.4	17.3	0.7	2.3	0.0	0.0	0.0	0.1	55
21	39.2	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.2	28.0	3.1	9.3	1.6	0.1	0.0	0.4	0.0	0.0	82
22	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.4	0.2	0.0	0.0	0.0	0.0	0.0	1.8	0.0	0.0	0.0	0.1	0.0	0.0	0.7	3
23	0.7	0.0	1.4	0.2	0.1	0.4	0.1		0.0	1.5	12.4	1.9	0.0	0.1	0.9	1.2	5.5	8.9	0.1	0.0	0.0	0.0	0.1	0.0	36
24	0.0	0.0	0.2	1.0	0.0	0.0	0.4		0.1	0.0	35.0	0.0	0.0	0.0	0.0	0.2	0.1	1.6	0.5	0.2	60.8	0.6	0.4	0.0	101
25	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0	4.2	8.8	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	14
26	0.0	0.0	0.0	0.0	8.0	0.0	0.0		0.0	0.0	0.0	0.1	0.2	0.0	0.0	2.2	114.9	46.7	0.0	1.2	0.0	0.0	0.0	0.0	166
27	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	3.3	0.5	1.0	1.4	9.3	7.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	23
28	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	0.0	5.0	0.0	0.0	24.8	36.2	0.0	0.0	0.0	0.0	0.0	0.1	67
KWh	61	0	3	1	2	1	1	4	86	79	109	196	277	639	1088	1387	1581	442	169	195	123	135	47	78	6703

Kalan	n	Ma	arch 2	2007			Wine	d Pow	er Ou	tput	of Bo	nus 6	00/44	Turbin	e (Mont	h's Տւ	ımma	ry)							
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.3	1.8	41.6	0.0	0.0	0.0	0.0	0.0	0.0	44
2	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.1	0.0	9.5	34.7	0.0	0.0	0.0	0.0	0.0	0.0	45
3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.5	1.8	0.2	23.0	0.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	26
4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	10.1	0.0	0.0	46.9	185.0	14.0	0.2	1.1	1.7	0.0	0.0	0.0	0.0	0.0	259
5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.3	0.0	0.7	0.0	0.0	0.1	0.0	0.0	0.0	1
6	0.0	0.1	0.1	0.0	0.1	0.1	0.1	1.2	19.8	0.0	6.9	0.1	0.0	0.0	0.0	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	29
7	0.0	0.0	0.0	1.2	0.1	0.6	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.5	1.2	0.1	0.0	0.0	0.0	0.0	0.0	0.0	4
8	0.0	0.0	0.0	0.0	0.0	0.5	0.0	0.1	0.1	3.1	0.0	0.0	0.0	0.0	0.1	1.9	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	6
9	0.0	3.0	0.2	1.2	0.1	19.4	0.3	0.0	0.1	5.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	30
10	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	34.9	8.1	16.7	3.1	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	63
11	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5.4	15.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	21
12	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.3	0.0	0.0	3.4	0.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5
13	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	10.8	64.2	58.3	41.0	39.2	21.5	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	235
14	0.1	0.2	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.7	22.4	211.4	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	235
15	0.0	0.0	0.0	0.2	0.2	0.5	0.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6	0.2	0.0	0.0	0.0	0.0	0.0	1.9	4
16	0.1	0.1	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6	1.0	0.1	0.0	0.0	0.0	0.4	0.1	0.0	3
17	0.2	0.0	0.0	0.0	0.0	0.1	0.1	30.9	42.5	8.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	83
18	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.1	0.0	0.0	0.3	0.0	0.5	0.0	0.0	0.7	1.3	3.5	7
19	0.0	0.0	1.0	1.0	0.0	0.1	0.0	7.6	2.6	1.0	8.7	0.0	0.0	0.0	0.1	0.3	0.0	0.2	1.5	0.1	0.1	0.0	0.0	0.0	24
20	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0
21	0.6	0.0	0.0	0.7	0.3	0.2	0.0	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2
22	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.1	0.1	0.6	0.0	1.0	0.0	0.0	2
23	0.1	0.9	1.0	0.0	0.0	0.0	0.1	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.1	0.1	3.2	0.1	0.0	0.0	0.0	0.0	0.0	0.0	6
24	0.0	0.0	0.2	0.5	0.1	0.1	0.0	0.0	0.2	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1
25	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	1.1	0.0	0.0	0.0	0.0	0.0	0.0	1
26	0.1	0.4	0.4	0.1	0.3	0.0	0.1	1.2	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.1	7.5	3.0	0.3	0.0	0.3	0.1	0.2	0.0	14
27	0.0	0.1	0.4	1.7	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.9	2.6	2.5	4.1	11.9	6.8	5.6	1.1	0.0	0.0	0.0	0.5	38
28	0.1	0.0	0.5	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	13.0	2.2	5.1	0.3	0.0	0.2	0.0	0.0	0.1	22
29	0.9	0.0	0.0	0.0	10.7	2.1	0.4	0.0	0.0	0.0	0.0	0.2	0.0	0.0	0.0	6.4	1.7	0.5	0.3	0.1	0.0	0.1	0.0	0.0	23
30	0.4	1.3	0.9	0.5	0.0	0.2	1.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	1.0	2.9	0.0	0.1	0.1	0.0	0.1	0.1	23.0	32
31	69.7	4.4	4.3	38.9	12.5	8.4	3.0	3.4	0.7	8.0	0.5	3.5	8.0	3.3	0.0	0.1	0.1	0.4	0.0	0.2	0.3	7.1	3.4	15.5	188
KWh	72	10	9	46	24	32	6	45	67	19	38	74	141	315	244	94	46	96	11	2	1	9	5	44	1452

Kalan	n	Ap	ril 200	7			Winc	Pov	ver O	utput	of Bo	onus 6	00/44	Turbir	ne (Mo	nth's	Summ	ary)							
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	13.0	27.7	3.4	2.9	0.0	0.0	0.0	0.0	0.0	0.0	0.5	45.7	19.0	12.8	5.4	8.0	0.4	0.0	0.1	0.0	0.1	0.0	0.0	0.0	132
2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	1.7	26.4	32.6	2.7	1.5	0.0	22.1	28.7	17.4	2.7	0.0	136
3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	2.2	9.9	0.0	0.0	0.1	0.0	0.0	0.2	0.1	0.3	0.1	0.1	0.0	0.9	0.0	0.0	14
4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	29.9	22.1	32.2	59.6	134.6	110.8	103.9	15.7	0.7	0.5	0.0	0.0	0.0	510
5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.6	10.1	25.3	38.2	38.2	29.0	0.0	0.0	0.3	0.0	0.0	0.0	0.0	142
6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.5	107.0	202.8	185.4	133.6	85.6	39.8	9.7	0.9	8.0	1.1	17.1	0.0	0.0	833
7	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.1	1.9	1.3	11.2	2.4	1.9	0.0	0.1	0.1	0.0	0.0	0.0	0.0	0.3	20
8	1.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.3	0.1	6.8	21.2	2.7	2.8	4.9	3.4	0.3	0.1	0.4	1.1	0.3	0.0	0.0	46
9	1.4	1.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	1.3	4.5	3.6	20.2	23.7	1.0	0.9	0.7	1.9	0.1	0.0	0.5	0.0	61
10	0.1	0.1	0.1	0.0	0.3	1.3	0.0	0.0	18.0	16.7	1.7	20.8	9.2	55.6	54.9	45.8	1.0	0.8	6.1	4.9	4.8	0.1	0.0	0.0	242
11	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.2	4.4	4.4	37.3	43.9	8.6	0.1	2.8	2.9	2.1	3.1	0.0	0.0	0.0	110
12	0.0	1.0	0.5	0.0	0.1	0.6	0.0	8.0	0.0	7.1	1.1	70.5	175.7	74.2	63.7	81.4	1.0	0.3	0.7	0.5	0.6	0.1	0.0	0.0	480
13	0.0	0.1	0.1	0.1	0.0	0.1	0.0	0.0	0.0	0.0	1.0	3.4	1.6	31.1	19.7	27.0	1.0	0.0	0.0	0.1	0.0	0.7	0.0	0.0	86
14	0.0	0.7	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.3	2.2	0.6	3.6	1.0	0.3	1.1	0.3	0.4	0.0	1.2	0.1	0.4	13
15	0.0	0.5	0.3	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.1	1.8	3.7	30.7	15.0	4.4	0.1	0.0	0.1	0.1	0.0	0.8	0.1	0.1	58
16	0.1	0.1	0.1	0.0	0.3	0.1	0.0	0.0	0.0	0.0	1.1	7.0	1.8	13.9	85.4	91.5	12.9	0.1	0.0	0.0	3.2	0.4	0.2	0.0	218
17	0.3	0.0	0.4	0.0	0.2	0.1	0.0	1.0	52.5	203.5	0.0	0.0	102.1	99.5	68.1	18.4	28.9	44.2	63.1	23.0	1.6	11.1	0.6	0.5	719
18	0.0	0.0	0.0	0.0	6.9	1.2	29.3	82.1	43.4	20.1	1.4	140.4	124.0	93.0	157.5	384.7	271.3	77.1	39.6	1.3	0.0	0.0	0.0	0.0	1473
19	3.3	140.2	215.8	87.2	12.7	0.1	0.1	0.9	0.1	0.1	0.1	0.0	1.0	106.4	347.3	356.2	243.7	25.0	6.3	0.0	0.0	0.0	0.0	0.0	1547
20	0.1	0.0	0.1	0.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	99.7	164.5	157.5	247.5	326.1	244.8	67.4	49.1	0.5	0.0	0.0	0.0	0.0	1358
21	0.1	0.0	0.1	1.3	4.0	0.6	3.4	1.9	8.4	8.0	20.0	0.2	3.4	0.9	43.2	205.5	146.1	66.1	6.0	0.1	0.0	0.0	0.0	0.0	519
22	0.0	0.1	0.0 1.6	0.0	0.0	0.2	0.4	0.0	0.0	0.0	6.1 0.0	109.0	162.4 183.8	205.6 221.8	207.2 118.8	46.0 46.2	85.9 26.7	164.9 274.5	38.2	63.8 37.9	45.0 9.6	9.4	0.1	14.6 4.8	1159 1291
23	14.2	21.6	115.2	0.1	0.1	0.0	0.0	5.3	2.0	0.0	0.0	0.4	0.8	53.9	46.8	106.3	315.1	103.1	25.8	0.0	0.0	0.3	0.2	0.0	799
25	0.4	0.7	0.2	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4	4.9	15.4	43.7	28.7	73.5	153.7	66.1	4.1	0.0	0.1	0.0	0.0	392
26	0.4	0.7	1.0	0.1	0.0	0.0	1.1	0.0	0.0	31.0	16.3	5.4	14.2	14.4	136.0	215.1	143.5	97.4	47.4	0.0	0.0	0.0	0.0	0.1	724
27	0.0	0.4	0.1	0.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.3	0.3	2.0	28.1	33.8	8.7	13.5	0.0	0.0	0.0	0.0	0.0	88
28	0.0	0.0	0.1	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.0	12.0	119.5	165.1	133.8	159.0	170.8	133.1	129.6	10.2	0.0	0.0	0.0	0.0	1034
29	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	16.9	108.0	307.9	84.7	5.9	57.1	0.2	0.0	0.8	0.0	0.0	4.0	0.3	586
30	0.5	0.1	0.0	2.0	0.1	0.5	0.1	0.0	0.0	0.0	0.0	0.0	19.7	160.8	168.7	103.7	74.0	6.7	0.0	0.3	42.6	18.1	12.2	20.4	631
KWh	37	195	340	96	26	5	35	92	127	297	100	833	1488	2121	2380	2612	2119	1344	715	176	142	78	21	41	15420
LZAAII	31	195	340	90	20	J	33	32	121	231	100	000	1400	2121	2300	2012	2113	1344	713	170	142	10	41	41	13720

Kalan	n	Ma	y 2007	7			Wind	l Pov	wer	Outpu	ıt of B	onus	600/44	Turbi	ine (M	onth's	Sum	mary)							
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	16.4	1.4	0.1	0.0	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	10.9	149.2	16.9	0.0	0.0	0.0	0.0	0.1	0.1	195
2	1.8	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	53.2	209.1	320.6	445.4	485.7	336.6	69.4	1.0	0.0	0.0	0.0	0.0	1923
3	0.1	1.1	0.0	0.1	0.1	0.0	0.0	0.0	0.0	0.0	128.5	497.2	289.2	413.5	351.7	286.0	115.3	196.4	69.6	31.1	301.1	10.5	2.9	1.4	2696
4	19.9	0.0	7.4	2.7	0.0	0.1	10.9	0.3	0.0	0.0	0.0	30.4	160.0	241.9	101.5	57.3	110.9	36.0	45.6	4.4	4.7	5.7	0.1	0.0	840
5	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	48.3	256.5	112.5	106.2	46.7	9.0	4.0	0.0	88.7	85.7	0.0	0.0	758
6	0.0	0.5	0.1	0.0	0.0	0.1	0.0	0.0	0.0	0.0	2.7	154.6	335.4	434.7	442.1	412.5	320.6	106.0	18.3	1.8	0.0	0.0	0.0	0.1	2229
7	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	24.2	243.0	165.1	271.6	337.9	201.3	2.8	0.0	0.2	0.0	57.5	10.3	2.6	56.8	1373
8	64.2	38.3	23.3	1.7	3.9	0.0	0.0	0.0	0.0	0.0	0.0	149.4	422.4	232.6	226.7	84.2	20.5	5.3	1.5	0.1	0.0	0.1	0.1	0.0	1274
9	0.3	0.7	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	218.5	373.1	269.1	257.8	302.1	72.3	37.7	1.0	0.0	0.0	0.0	0.0	1533
10	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	84.7	45.6	121.2	256.0	68.1	14.4	35.6	71.0	0.0	0.8	0.0	0.0	0.0	698
11	0.0	0.4	0.0	0.2	0.4	0.5	2.8	0.0	0.1	0.0	0.5	2.2	5.2	58.5	208.1	372.6	374.5	143.2	90.6	11.6	0.0	0.0	0.0	0.0	1271
12	0.4	0.0	0.0	0.5	0.3	2.7	8.0	0.2	0.1	11.7	241.1	497.5	515.6	588.7	593.1	576.5	544.2	442.0	255.5	42.4	9.5	0.0	0.0	0.0	4323
13	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	1.7	45.1	273.3	451.2	490.4	555.3	587.5	560.8	510.4	391.6	142.6	20.0	1.2	0.0	0.0	0.0	4031
14	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	38.1	203.6	514.6	559.6	546.2	305.2	324.5	261.7	40.7	4.3	0.0	0.0	0.0	0.0	2799
15	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5.6	183.7	467.8	552.0	477.1	312.0	33.4	7.0	9.4	47.1	51.1	92.6	43.4	35.4	2318
16	18.4	112.5	2.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	25.7	159.3	212.6	91.4	246.2	277.7	55.0	9.4	14.6	7.6	18.3	0.8	2.9	1255
17	0.3	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	31.5	163.6	232.0	179.6	115.1	77.2	106.7	0.4	0.0	0.0	0.0	0.0	907
18	0.0	0.1	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6	13.3	56.1	12.8	3.9	12.0	3.2	129.0	19.4	0.7	0.2	0.1	0.0	0.3	252
19	10.2	1.0	1.1	0.0	0.0	0.0	0.0	0.0	0.3	10.0	12.1	9.0	0.1	0.1	1.5	4.9	189.9	22.2	3.9	81.2	15.0	2.8	3.7	0.1	369
20	0.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.8	197.0	223.6	274.0	177.6	417.2	162.2	135.1	5.0	137.3	45.7	18.9	0.3	0.0	1795
21	0.0	0.0	0.0	0.1	70.3	32.1	17.4	89.5	6.4	0.0	7.0	40.6	49.6	12.5	201.6	201.5	2.3	0.2	60.1	1.7	0.0	0.0	0.7	0.0	794
22	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	6.6	162.0	89.7	54.0	335.8	358.7	259.0	169.5	11.4	0.0	0.0	0.0	0.0	0.0	1447
23	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	27.8	9.8	190.4	369.3	43.6	91.9	208.6	59.2	131.1	77.8	0.0	0.0	0.1	0.0	1209
24	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	39.9	62.4	95.6	44.4	254.2	34.6	18.2	6.7	0.2	1.6	0.0	0.9	1.6	0.0	560
25	0.1	0.0	0.0	0.1	0.3	0.5	0.0	0.0	0.0	0.0	18.8	0.1	0.1	0.4	54.8	31.6	21.8	2.0	0.0	0.0	0.0	0.4	0.0	0.1	131
26	0.1	0.0	0.0	0.0	0.0	0.0	0.0	13.2	_	0.0	0.0	0.0	141.1	308.7	318.7	249.8	215.2	441.0	174.5	42.5	0.5	0.0	0.0	0.0	1905
27	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.3	115.7	442.4	568.3	529.4	288.6	307.5	395.3	128.3	27.2	1.4	0.0	0.0	0.0	0.0	0.0	2804
28	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	124.2	219.3	530.9	412.9	394.2	187.1	5.3	0.4	0.1	0.0	0.0	0.0	0.0	0.0	0.0	1874
29	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.9	404.4	105.6	110.0	112.4	62.2	35.2	57.4	101.5	31.6	0.0	0.1	0.1	0.5	1026
30	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	49.2	79.0	124.6	162.2	0.3	0.1	0.0	0.0	32.5	112.3	27.4	0.0	0.0	0.0	588
31	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	99.5	175.1	63.5	41.8	12.0	57.4	4.0	5.7	0.0	0.0	0.0	0.0	2.7	462
KWh	133	156	35	6	75	36	32	103	9	307	1544	4699	6116	7339	7194	6360	5050	3245	1519	666	611	246	57	100	45638

Kalan	n	Ju	ne 20	07			Wir	nd P	owe	r Outp	out of	Bonu	s 600/	44 Tur	bine (Month	า's Suเ	mmary	/)						
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	0.1	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	34.2	132.2	291.2	349.3	350.1	283.8	336.2	74.7	30.6	9.2	9.7	0.0	0.0	0.0	1901
2	0.1	1.0	0.1	0.0	0.4	0.1	0.0	0.0	0.0	0.0	0.0	108.1	53.2	14.5	0.0	0.0	0.0	0.0	1.2	78.0	100.5	14.0	0.0	0.1	371
3	0.0	0.2	0.0	0.0	0.9	0.0	0.1	0.2	0.0	0.0	0.0	0.1	5.7	26.2	27.7	9.3	0.5	0.0	0.5	0.0	0.0	0.0	0.0	0.0	71
4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	9.7	7.2	2.1	0.7	18.8	17.9	0.0	0.7	0.2	0.0	0.0	0.0	0.0	0.0	57
5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	8.0	21.3	8.0	0.3	0.7	2.8	13.3	0.3	0.0	9.4	0.0	0.1	0.0	0.0	50
6	5.6	0.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	139.8	66.1	47.5	14.6	1.3	54.2	356.1	184.2	0.4	0.0	0.0	0.0	0.0	870
7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	32.7	92.3	124.6	111.6	252.3	154.1	44.9	0.0	0.0	0.0	0.0	0.0	813
8	0.1	0.5	0.4	0.8	0.1	0.0	0.4	0.0	0.0	0.0	0.0	137.0	206.9	48.2	130.1	139.6	115.5	65.5	32.6	0.0	0.0	0.0	0.0	0.0	878
9	0.0	0.2	0.7	0.4	0.0	0.0	3.6	0.6	0.0	0.0	0.0	0.0	0.1	0.0	0.3	19.7	71.3	40.5	8.5	0.0	0.0	0.0	0.0	0.1	146
10	0.1	0.9	1.5	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	76.4	94.8	125.7	62.9	86.5	0.0	0.0	0.0	0.0	0.0	449
11	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	1.0	66.6	130.0	151.6	122.9	148.4	162.1	72.1	8.2	0.0	0.0	0.0	0.0	863
12	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	267.4	194.2	236.1	220.8	158.5	122.0	78.3	79.1	8.8	0.1	0.0	0.0	0.0	1365
13	0.0	0.0	0.0	0.0	0.0	0.2	0.0	0.0	0.0	0.0	113.6	344.2	196.0	135.3	132.5	164.6	249.3	395.5	147.6	17.5	0.5	0.0	0.0	0.0	1897
14	0.0	0.0	0.0	0.0	8.5	12.2	0.5	0.0	0.0	0.0	48.8	362.1	294.3	416.9	576.1	517.9	439.8	348.7	182.5	36.0	43.6	120.7	103.8	48.4	3561
15	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	105.4	452.2	537.4	361.6	452.8	315.3	410.4	452.4	539.9	318.4	60.2	18.3	0.2	0.0	0.0	4025
16	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	127.4	539.7	519.1	553.2	565.1	550.5	410.4	363.0	342.6	159.6	16.8	0.0	0.0	0.0	0.0	4147
17	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	16.8	147.5	477.5	548.0	506.7	479.3	389.0	286.7	349.1	205.4	20.8	8.0	0.0	0.0	0.0	0.0	3428
18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.4	304.0	531.7	418.7	403.8	354.5	312.0	281.5	268.0	202.2	49.1	0.1	0.1	0.0	0.0	3129
19	0.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.3	164.0	398.3	321.8	289.4	480.0	374.4	306.9	391.2	116.6	4.4	0.1	0.0	0.0	0.0	2849
20	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	132.4	431.2	577.4	584.1	482.2	393.4	285.4	318.0	211.2	122.5	32.0	0.5	0.0	0.0	0.0	3570
21	0.0	0.0	0.0	0.1	0.0	0.0	0.0	0.0	0.0	1.1	145.2	382.3	543.4	566.6	554.4	548.4	518.2	268.3	82.8	36.2	28.3	0.0	0.0	0.0	3675
22	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6	86.9	390.6	547.0	563.3	501.4	491.2	386.2	463.7	56.5	100.3	16.9	2.2	0.8	1.7	0.0	3609
23	0.1	0.2	1.7	0.0	0.0	0.1	0.0	0.0	0.0	30.5	338.2	500.1	594.0	509.2	577.3	584.4	565.9	525.9	251.9	43.5	61.5	1.3	0.0	0.1	4586
24	0.0	0.3	0.2	0.0	0.0	0.0	0.0	0.3	0.4	27.8	231.7	536.3	526.4	485.9	509.2	514.4	425.1	361.3	192.2	61.8	18.2	1.9	0.2	0.4	3894
25	12.9	35.6	13.7	14.1	0.3	0.0	0.0	0.0	0.1	5.2	18.1	52.6	18.8	0.9	17.3	121.4	241.5	405.0	258.2	15.4	19.6	11.4	112.8	75.9	1451
26	49.4	0.0	0.0	0.0	0.0	0.0	0.0	0.3	0.0	21.8	342.2	542.4	595.6	395.2	319.6	464.9	436.9	457.4	229.1	35.9	13.1	8.3	0.0	0.0	3912
27	0.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	195.6	230.8	374.5	552.6	537.5	531.3	391.1	261.3	48.0	59.4	32.7	70.9	38.8	179.5	225.5	3730
28	37.6	9.1	2.6	45.8	13.2	0.0	-	0.0	0.0	0.0	121.7	185.6	5.5	21.6	0.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	443
29	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.3	7.4	105.2	179.0	204.0	235.8	261.8	343.9	132.6	54.2	85.5	56.5	22.2	2.3	1.9	1.9	1695
30	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	56.3	293.9	502.9	569.5	559.3	556.4	519.6	424.1	284.1	56.7	16.3	0.0	0.0	0.0	0.0	3839
KWh	107	48	21	62	23	13	5	1	18	950	4793	8435	8329	7983	8125	7598	7469	6158	3127	646	409	200	400	352	65274

Kalar	n	J	uly 20	07			Wind	d Pov	wer Oı	utput	of Bor	nus 60	0/44 T	urbine	(Mont	h's Su	ımmaı	ry)							
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.7	62.7	223.5	519.1	576.6	510.6	399.1	332.7	320.6	162.1	20.4	15.2	11.5	21.4	26.5	3207
2	16.5	6.9	158.6	173.6	0.3	0.0	0.0	0.0	0.1	97.7	522.0	477.2	211.7	81.9	74.5	45.8	67.2	122.6	19.8	0.0	0.0	0.0	0.0	0.0	2076
3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	2.2	89.3	380.7	558.4	526.4	512.7	580.8	545.1	433.0	186.3	22.4	29.6	1.9	0.0	0.0	3869
4	0.0	0.0	0.0	0.9	0.7	10.3	0.0	0.0	6.0	47.9	133.1	393.4	533.2	584.6	578.2	556.5	479.2	370.3	114.5	21.6	1.0	0.0	0.0	0.0	3831
5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	14.7	126.6	257.7	484.3	243.2	259.2	314.6	62.6	0.6	3.7	0.3	0.2	0.0	0.0	0.0	1768
6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	7.6	120.1	394.0	553.9	548.9	483.9	441.4	420.4	157.2	47.5	23.9	0.0	0.0	0.0	0.0	3199
7	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.0	123.6	499.7	392.5	233.4	52.1	66.8	0.1	5.4	0.6	0.3	0.2	0.1	2.3	35.6	4.9	1418
8	0.1	2.8	9.8	6.4	0.1	0.0	0.0	0.0	0.0	0.0	146.6	449.9	553.6	522.7	319.9	240.6	386.1	441.6	171.9	46.1	16.2	6.2	0.0	0.0	3321
9	0.0	0.0	0.2	0.0	0.4	2.2	0.5	0.0	0.0	26.3	236.4	322.0	461.1	567.3	502.3	473.8	494.7	252.7	139.2	14.3	0.0	0.0	0.0	0.0	3493
10	0.0	0.0	0.0	0.0	0.7	0.0	0.0	0.0	0.0	0.1	66.4	179.0	445.0	504.7	537.8	555.0	462.8	210.9	119.6	25.7	8.0	0.0	0.0	0.0	3116
11	0.0	0.0	0.0	0.4	3.1	0.1	1.3	8.0	18.4	171.9	458.3	551.7	581.0	569.8	396.1	382.5	229.8	249.2	128.2	25.7	23.2	0.0	0.0	0.0	3791
12	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.3	4.6	49.7	330.8	455.3	433.6	211.1	112.4	459.9	181.6	5.2	8.0	0.3	0.6	0.0	0.0	0.1	2246
13	0.1	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	55.0	251.2	89.5	110.7	52.4	5.5	0.7	0.0	0.1	0.0	0.0	0.0	0.0	0.0	0.0	565
14	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.5	4.9	4.7	195.8	130.8	237.6	0.1	0.0	7.2	0.3	0.0	0.5	0.2	0.0	583
15	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.3	81.7	172.1	408.5	472.4	411.5	438.4	312.7	208.2	202.8	91.8	3.9	1.3	0.0	0.0	0.1	2806
16	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.9	142.1	430.2	518.2	311.7	371.1	235.3	186.3	192.7	48.1	13.6	0.0	0.0	0.0	0.0	2450
17	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	46.2	404.9	557.6	462.8	367.9	273.8	214.9	292.9	147.5	54.1	16.3	0.4	0.0	0.0	0.0	2839
18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	10.5	38.0	220.8	441.3	521.2	305.9	297.8	370.1	244.6	94.5	30.0	12.7	0.3	0.0	0.0	2588
19	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.7	246.9	530.8	572.8	594.5	552.5	423.9	288.4	109.8	26.7	3.8	3.1	0.0	0.1	0.3	3403
20	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	81.5	455.3	519.1	540.0	552.7	529.3	510.9	384.0	424.5	267.9	93.5	25.8	32.5	3.9	0.0	4421
21	4.4	6.2	99.2	21.6	72.7	30.8	48.3	47.5	100.4	57.3	97.4	3.0	0.0	0.0	0.2	0.7	0.2	0.0	0.0	0.0	0.0	0.1	0.0	0.1	590
22	0.0	0.0	2.0	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	64.5	47.6	51.1	55.9	33.5	3.2	0.0	0.1	0.0	0.1	259
23	0.0	1.4	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.5	131.4	168.7	227.8	326.9	89.8	53.8	29.2	19.2	5.4	0.3	0.0	0.0	0.0	1055
24	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.9	135.2	388.5	551.6	529.5	467.0	396.0	87.9	85.6	61.0	3.6	0.1	0.0	0.0	2707
25	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.3	19.8	142.4	319.0	408.2	237.9	193.6	89.1	64.8	15.1	4.6	0.1	0.1	0.0	0.0	1495
26	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	24.4	49.8	44.3	20.4	81.8	25.8	56.3	45.9	0.1	0.0	0.0	0.0	0.0	0.0	0.0	349
27	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.6	174.6	562.4	520.5	514.5	517.3	296.3	316.6	157.3	33.0	23.7	0.0	0.0	0.0	0.0	3118
28	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	29.4	216.8	416.0	522.0	548.6	548.7	523.4	517.9	217.8	82.5	37.4	2.9	0.0	0.0	0.0	3663
29	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.6	179.7	282.8	489.1	521.5	562.9	549.9	491.9	447.9	374.7	191.1	40.2	20.3	7.3	46.5	0.0	4209
30	0.0	32.7	0.7	0.0	0.0	0.0	0.0	0.0	5.7	193.9	397.1	452.3	416.1	430.2	45.5	8.0	10.8	1.6	0.1	0.1	0.1	0.0	0.0	0.0	1988
31	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.8	57.9	154.1	301.9	239.0	233.3	17.7	32.2	47.6	32.9	16.6	0.9	0.0	0.0	0.0	1135
KWh	21	50	271	203	78	43	50	49	139	1359	5800	9768	11870	11562	10041	8869	7359	4923	2177	554	166	63	108	32	75556