Pakistan Meteorological Department



A STUDY OF WIND POWER POTENTIAL AT AYUN-CHITRAL

By:

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Executive Summary

Pakistan Meteorological Department (PMD) conducted a wind power potential survey of the northern areas of Pakistan. Funding for this project was provided by the Ministry of Science & Technology. Under this wind data was collected at 42 sites along the Northern parts of the Country.

In this report the analysis based on one year wind data has been presented along with the wind generated electric power at Ayun-Chitral. Wind data with ten minute average speed and direction were collected at 10 meters and 30 meters height and 50 meters values were computed from models.

At 50 meters we have the annual average wind speed of 3.93 m/s during twelve months May-2007 to April-2008 the highest of 6.88 is observed in August 2007. Seasonal Diurnal Wind variation indicates that maximum wind speed is available in the evening through-out the year. Wind frequency distribution shows that during 6.0% of the time wind speed is 5 m/s or above.

Sometimes simply wind speed averages do not give the true picture of the wind power optional of an area. For the purpose it is common to assign areas to one of the seven wind classes based on "wind power density" of the area. Monthly and annual wind power density has been computed and added in the report. The annual power density of Ayun-Chitral is **169** W/m² according to international wind classification, this power density categorize Ayun-Chitral as a Marginal site for wind power generation.

Wind generated electric power has as also been computed on hypothetical 600Kw wind turbine and its hourly, monthly and annual values has been added in this report. The annual power production form a single 600kw wind turbine come out to 491,091 kWh which shows the capacity factor of 9% for Ayun-Chitral. Internationally it is accepted that if any site has a capacity factor of 25% and above than that site is suitable for installation of economically viable wind power farms. As such Ayun-Chitral and surrounding areas can be classified as not suitable site for installing big economically viable wind farms.

1. **Introduction:**

Wind energy is the fastest growing renewable energy source today. A continued interest in wind energy development worldwide has produced steady improvements in technology and performance of wind power plants. New wind power projects have proven that wind energy not only is cost competitive but also offers additional benefits to the economy and the environment.

A steady supply of reasonably strong wind is necessary requirement for utilizing the power in the wind. Development of wind energy depends upon a clear understanding of wind resources. Site location, turbine performance and physical effects of turbulence and energy extraction represent a few of the issues that must be addressed by anyone interested in developing wind energy.

As such any plan to develop wind energy must begin by understanding the wind resource. Where are the best potential wind sites located? How much energy could be extracted from the wind at those sites?

1.1 Characteristic of wind:

The global winds are caused by pressure differential across the earth's surface. The amount of solar radiation absorbed at the earth's surface is greater at the equator than at the poles. This variation in incoming heat sets up convective cells in the lowest layer of the atmosphere. In the simplest form air rises at the equator and sinks at the poles. However the rotation of the earth complicates this simple heat transfer. A series of circulations are set up in both northern and southern hemispheres.

The areas of the globe where air is descending are zones of high pressure and where the air is ascending, low-pressure zones are formed. The pressure gradient drives the flow of air from high to low pressure, thus causing the wind. The wind is then acted on the corriolis force due to the earth's rotation. The resultant wind is turned easterly or westerly. On a smaller scale, wind is created because of temperature difference between land and sea and mountains and valleys. The local topographical features and roughness of the terrain also cause air movements.

2.0 Wind Mapping Project of Pakistan Meteorological Department:

As any plan to develop wind energy must begin by understanding the wind resources. Where are the best potential wind sites located? How much energy could be extracted from the wind at those sites? Will the wind turbine performance be affected by the turbulence or other wind resource characteristics?

To answer these questions and to provide wind resource database for the different potential parts of the country, Pakistan Meteorological Department prepared a phased programme. Government of Pakistan, Ministry of Science and Technology provided the necessary funding for undertaking the Phase II. Second phase covers the Northern areas of Pakistan.

2.1 Study Area:

The project area for the wind mapping Phase-II covers the Northern areas of Pakistan including Districts are Swat, Dir, Chitral, Gilgit, Skardu, Haripur, Shangla, Buneer, Nowshara, Peshawar, Mohmad Agency, Khyber Agency and Azad Kashmir.

Forty-Two stations for collecting wind data have been installed to study the wind regime as shown in Map-1. The list of stations is given below:

Fatehpur, Bahrain, Kalam, Khawazakhaila, Malamjabba, Tahash, Khungipayan, Dir, Tarbella, Nizampur, Warsak, Chitral City, Drosh, Mirkhani, Shagore, Garam Chasma, Khagozi, Reshan, Mastuj, Kalash, Ayun, Astore, Bunji, Chillas, Gilgit, Gupis, Sost, Passu, Aliabad, Shigar, Barapayan, Sermik, Lowaramaina, Ramatkore, ShahidaSir, Danakool, Shaheed Gali, Moorti Pahari, Rangla, Pedar, Shaheedgali, Dargai.

Ayun is situated in Chitral. Latitude & Longitude of Ayun is: Latitude = 35.81°, Longitude = 71.84°, Elevation = 4765 ft.

2.2 Data source:

To undertake this study 30-meter high towers are erected at the locations mentioned above. On each of these high towers two wind speed anemometers are installed at the height of 10 meters and 30 meters, respectively; wind vane for recording wind direction is installed at 30 meters height. NRG automatic data loggers have been installed to record data at each site. These data loggers are recording, ten-minute average wind speed at both level, ten-minute average wind direction, and 10-minute average minimum and maximum wind speed. While selecting the above-mentioned locations for wind monitoring; the main objective was to identify potentially windy areas that also possess other desirable qualities of wind energy developed site. Further following guidelines as far as possible were also kept in mind while choosing an exact location for monitoring towers.

- Towers are placed as for as possible away from the local obstruction to the wind
- Selected location should be representative of the majority of the site.

Since sating a tower near obstructions such as trees or building can adversely affect the analysis of the site's wind characteristics such as magnitude of wind resource, wind shear and turbulence levels the tower in most cases are placed as for as possible away from local obstructions to the wind. But where this rule could not be followed, the tower was placed at horizontal distance of 10 times the height of the obstruction in the prevailing wind direction as required internationally. The following parameters have been recorded during the study.

- i. Wind speed ten minute average at 10 & 30 meters
- ii. Maximum wind speeds during 10 minutes
- iii. Minimum wind speeds during 10 minutes
- iv. Wind direction ten minutes average at 30 meters

Every month a team of observers and Maintenance Engineers visit site to inspect the instruments and to download the data on a laptop. Finally, the data is compiled and analyzed at Renewable Energy Research Cell established at Meteorological Department Islamabad.

3.0 Methodology; Analysis & Discussion:

3.1 Wind speed variation with height:

Wind speed tends to increase with height in most locations, a phenomenon known as wind shear. The degree of wind shear depends mainly upon on two factors, atmospheric mixing and the roughness of the terrain.

Atmospheric mixing typically follows a daily cycle driven by solar heating. At the hub height of a wind turbine, this cycle often causes wind speeds to increase in the daytime and decrease at night. However, the range of variation between night and day typically diminishes as hub height increases. At a height of approximately 50 meters, it weakens or may even disappear in some cases.

Terrain roughness also affects wind shear by determining how much the wind is slowed near the ground. In areas with a high degree of roughness, such as forests or cities, near-surface wind speeds tend to be low and wind shear high, whereas the converse is true in areas of low roughness such as flat, open fields. Wind shear may be greatly reduced or eliminated where there is an abrupt change in terrain height such as a sea cliff or mountain ridge.

To save money wind measurements sometimes are taken at a lower height than the wind turbine tower. In that case, it is essential to measure wind shear at different times of day in different seasons to accurately predict the performance of a wind power plant. The shear can be measured by monitoring wind speeds at two or three heights on a tower. Since wind turbines produce much more power in stronger winds, wind turbine designers try to put turbines on the tallest possible towers. At some point, however, the increased cost of towers outweighs the benefits. With current wind turbine technology, the optimum tower height for large wind machines appears to be approximately 40 to 50 meters.

For saving money in this survey also the wind has been recorded at 10 & 30 meters and for calculating the wind speed at 50 meters the following two methods has been used in this study.

3.1.1 *Log Law:*

The turbulent mixing in the atmosphere may be considered in a similar way to molecular mixing (this is called k theory). Assuming the mixing is dominated by mechanical mixing due to shear forces a relationship of wind speed with height is derived.

$$u = \frac{u_*}{k} \ln \left(\frac{z - D}{z_o} \right)$$

Where

 U_* is the friction notify

k is the von Karman constant

 $\mathbf{Z_0}$ is the roughness length

D is the displacement height

The von Karman constant is generally taken as 0.4. The roughness length Z_o is related to the vegetation cover of the area. The values of roughness length are given in Table-1. The displacement height D is the height above the roughness elements where the flow is free. For most vegetation it is small and is generally treated as zero. For large roughness elements like trees and building in towns it is not negligible and is the order of the average height of the elements. The <u>log law</u> may only be used for heights above D. Turbines are rarely sited in forests or towns, so D is usually taken as zero.

The wind speed at any height z can then be computed provided that the wind speed at a height Z_R is known. Thus:

$$\frac{u}{u_R} = \frac{\ln \left(\frac{z}{z_o} \right)}{\ln \left(\frac{z}{z_o} \right)}$$

Where

 U_R is the wind speed at reference height Z_R

The reference height is usually 10m or 30m as this is the height at which mean wind data is generally collected.

3.1.2 *Power Law:*

Engineers often prefer to use a <u>Power Law</u> to describe the increase in wind speed with height, as it is easier to evaluate.

$$\frac{u}{u_R} = \left(\frac{z - D}{z_R}\right)^{\alpha}$$

Where:

 α is the power law exponent

 U_R is the wind speed at reference height Z_R

The power law exponent typically varies between 0.1 and 0.32 depending upon the landscape type. A value of 1/7 is often quoted as a reasonable value for the power law exponent in countryside. The exponent can be calculated from the roughness length.

$$\alpha = \frac{\ln \left(\ln \left(\frac{z}{z_{o}} \right) \right)}{\ln \left(\frac{z}{z_{R}} \right)} \approx \frac{1}{\ln \sqrt{\frac{z \cdot z_{R}}{z_{o}}}}$$

Where: Z is the measurement height

Z_R is the reference height

 Z_0 is the roughness length

The power law exponent therefore varies with the interval between the two measurement heights. The power law should be carefully employed since it is not a physical representation of the surface layer and does not describe the flow nearest to the ground very well. Both the log law and the power law are simplified expressions of the <u>wind profile</u>. They are valid in flat homogeneous terrain. So they do not include the effects of topography, obstacles or changes in roughness or stability.

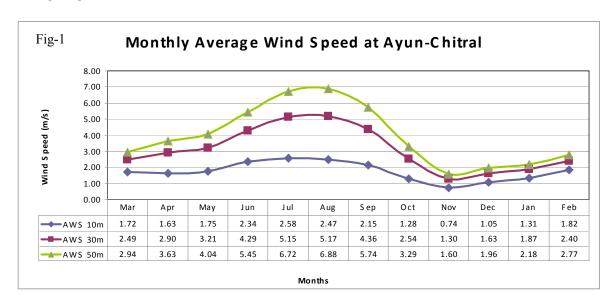
Table 1: Typical values of surface roughness length Z_0 and power law exponent α for various types of terrain

Type of terrain	\mathbf{Z}_0	α
Mud Flats, Ice	10 ⁻⁵ to 3x 10 ⁻⁵	
Calm Sea	2x10 ⁻⁴ to 3x10 ⁻⁴	
Sand	$2x10^{-4}$ to 10^{-3}	0.01
Mown Grass	0.001 to 0.01	
Low Grass	0.01 to 0.04	0.13
Fallow Field	0.02 to 0.03	
High Grass	0.04 to 0.1	0.19
Forest and Woodland	0.1 to 1	
Built up area, Suburb	1 to 2	0.32
City	1 to 4	

3.2 Average Wind Speed:

By using above mentioned methods the wind speed at 50 meters has been computed and monthly average of these wind speed at 50 meters height have been given in Fig 2 in graphical as well as tabular form.

Fig-1 shows monthly average wind speed at height of 10 meters, 30 meters and 50 meters from March 2007 to Feb 2008. At 30 meters height, we have the maximum average wind speed of 5.17 m/s during August, 2007. At 50 meters we have the annual average wind speed of 3.93 m/s from March-2007 to Feb 2008 and the highest average wind speed of 6.88 m/s is observed during August 2007.



3.3 **Diurnal Wind speed Variation:**

Fig-2 shows the annual diurnal wind speed variations at Ayun-Chitral. The wind speed is generally equal during day and night time, it reaches maximum in evening which is around 6.90 m/s and 5.5 m/s at 30 meters and 50 meters height respectively.

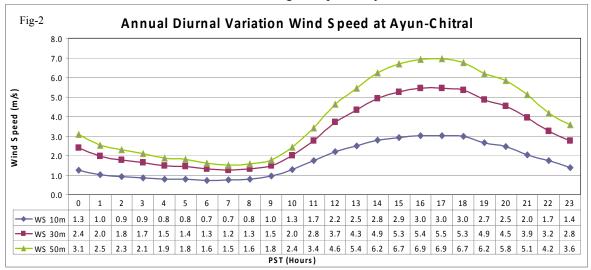
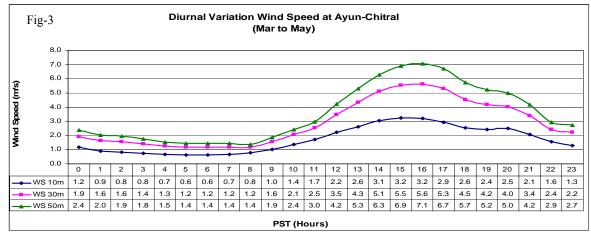
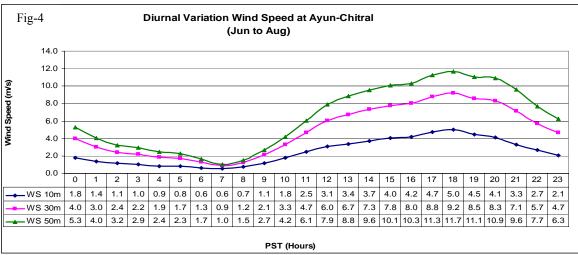
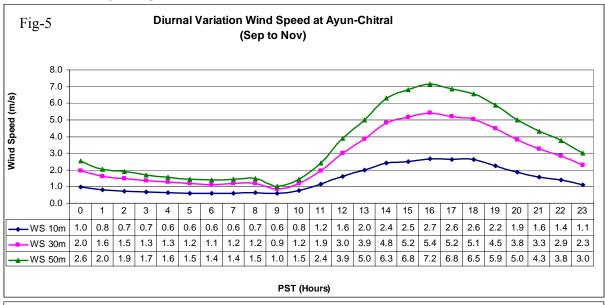
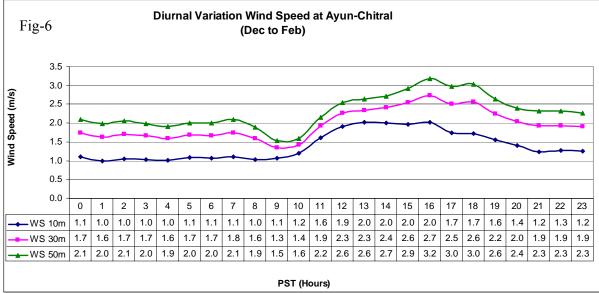


Fig-3, Fig-4, Fig-5 and Fig-6 shows the seasonal diurnal wind speed variations at Ayun-Chitral for (Mar-May), (Jun-Aug), (Sep-Nov) and (Dec-Feb) respectively. Seasonal wind speed is generally higher during daytime and low during night in Ayun-Chitral.









3.4 Wind speed Frequency Distribution:

Wind speed frequency distribution can simply be obtained by plotting the different wind speeds against their frequencies / relative frequencies. For obtaining frequency distribution the following two procedures are necessary.

3.4.1 **Binning of Data:**

The sorting of the data into narrow wind speed bands is called binning of the data. In our case a bin width of 1m/sec has been used e.g. a measured wind speed of 3.5 m/sec would be placed in 3<X<=4 m/sec bin. The central value of each bin i.e. 0.5 m/sec, 1.5 m/sec etc has been used in calculations and frequency distribution group.

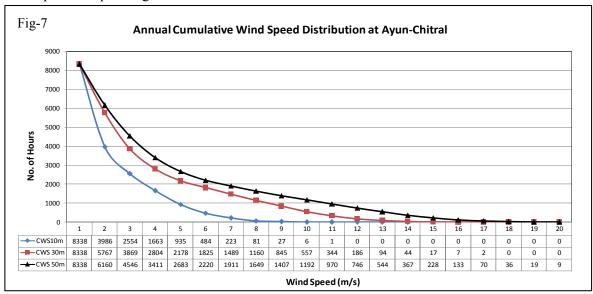
3.4.2 Relative Frequency:

It is proportional wind speed in each bin. It can be viewed as the estimate of probability of given wind speed in the bin. Relative frequency is defined as

R.F = probability P (Vi_1 = Frequency of given wind speed / Total period

3.4.3 Annual Cumulative Wind Frequency:

Fig-7 shows the Annual Cumulative Wind Frequency distribution at three heights 10, 30 and 50 meters. The analysis indicate that in a year at a height of 30 meters during 2178 hours the wind speed is greater than or equal to 5 m/s whereas at 50 meters, during one year 2683 hours the wind speed is equal or greater than 5m/s.



3.4.4 Wind Frequency Distribution:

Fig-8 shows the Annual wind frequency distribution at Ayun-Chitral. We can see that at 50 meters during 463 hours wind speed is 5 m/s, 310 hours speed is 6 m/s, 262 hours speed is 7 m/s, 242 hours speed is 8 m/s and during 215 hours the wind speed is 9m/s and so on. This indicates wind potential in this area.

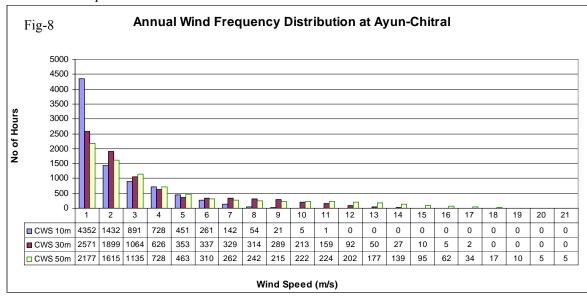
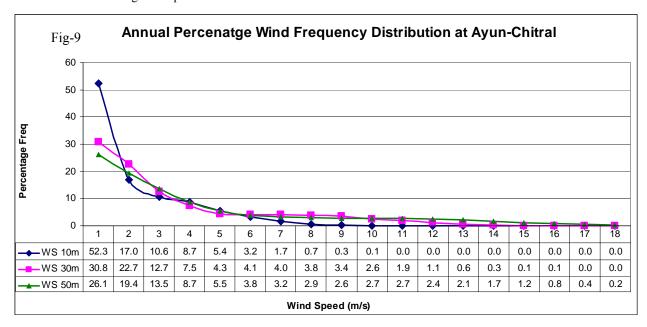


Fig-9 gives the frequency distribution in percentage. At 50 meters we find that during 5.5% of time wind is 5m/s, 3.8% of the time 6m/s and 3.2% of the time it is 7m/s. whereas at 30 meters height we get 4.3% of the time wind speed 5m/s, 3.2% of the times 6m/s and 1.7% of the time 7m/s.

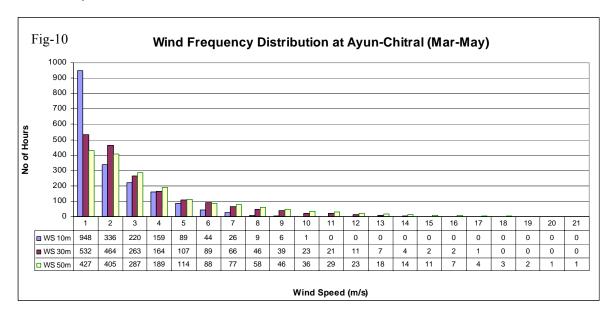


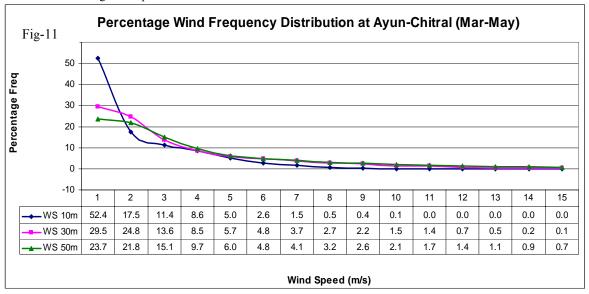
3.4.5 Seasonal Wind Frequency Distribution:

Figures 10–17 gives seasonal wind frequency distribution and percentage wind frequency distribution.

March-May

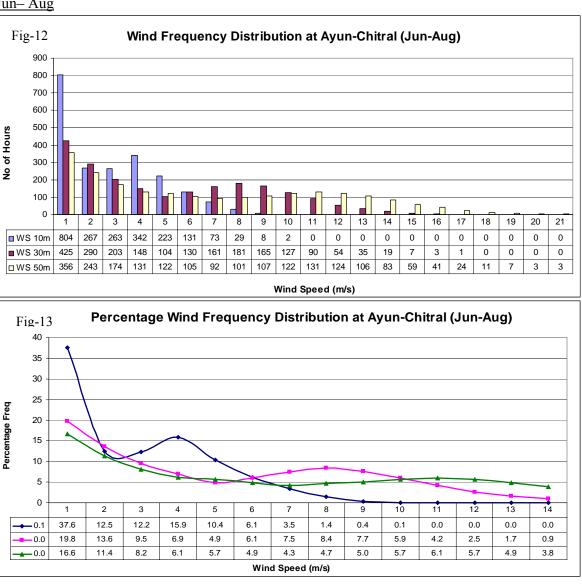
Fig-10 shows frequency distribution during the months of Mar to May. We can see that in this period at 30 meters height during 107 hours we get 5m/s, 89 hours 6m/s, 66 hours 7m/s. Similarly at 50 meters we get 114 hours 5m/s, 88 hours 6m/s, 77 hours 7m/s, 58 hours 8m/s, 46 hours 9m/s, 36 hours 10m/s.





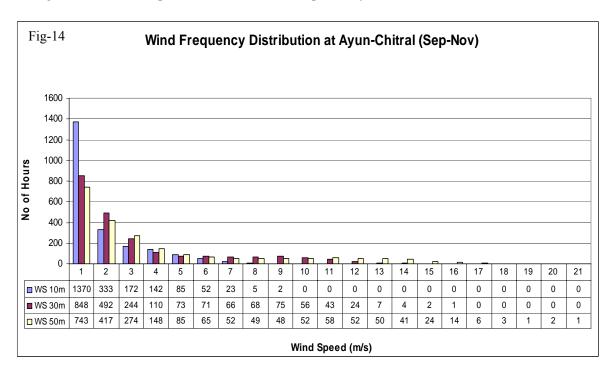
Similarly the above mentioned seasonal frequency distribution percentage terms have been presented in figure 11.

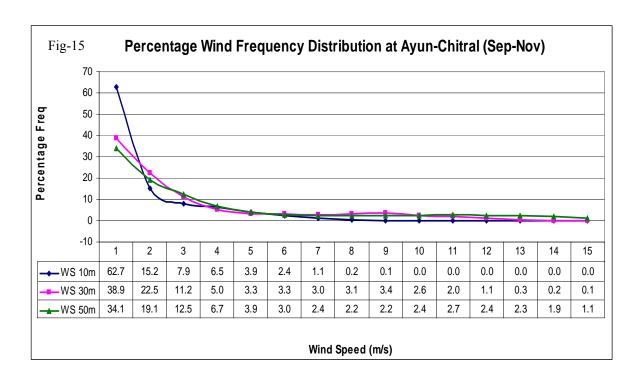
Jun-Aug



September – November

Fig-14 and 15 shows wind frequency distribution and percentage frequency distribution during the months of September to November respectively.



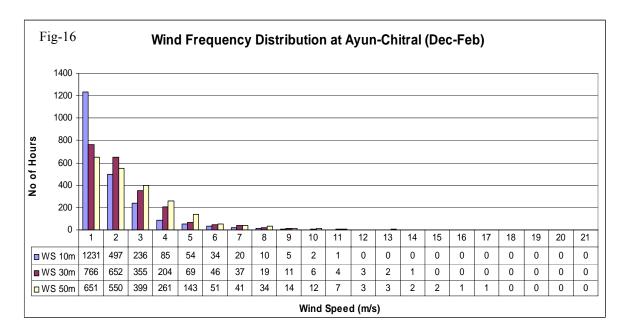


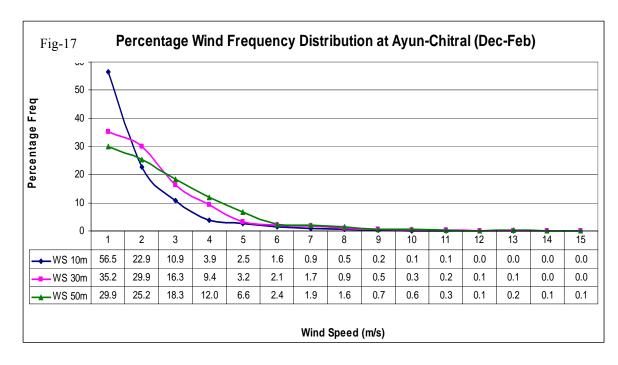
Dec – Feb

Fig-16 shows frequency distribution during the months of December to February. We can see that in this period at 30 meters height during 69 hours we get 5m/s, 46 hours 6m/s, 37 hours 7m/s.

Similarly at 50 meters we get 143 hours 5m/s, 51 hours 6m/s, 41 hours 7m/s, 34 hours 8m/s, 14 hours 9m/s, 12 hours 10m/s.

Similarly the above mentioned seasonal frequency distribution percentage terms have been presented in figure 17.

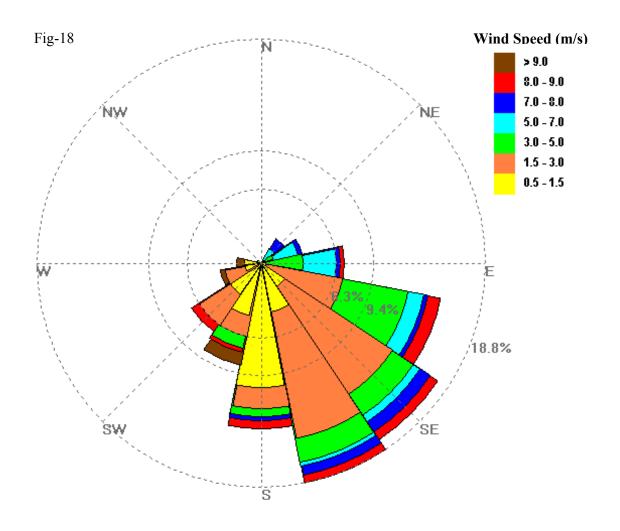




3.5 Wind Rose:

Fig-18 shows the Wind Rose Graph based on 12 months data from March 2007 – February 2008 collected at 30 meters height. Wind Rose indicates that most of the time the wind direction is South and South East. The average wind speed is 3.11 m/s and the percentage of wind speed greater than 5m/s is 22%.

Wind Rose at Ayun-Chitral (30m height during 12 months)



Average Wind Speed	Wind greater than 5 m/s	Comments
3.11 m/s	22%	

3.6 Wind speed statistic:

3.6.1 The statistical Mean:

It is the average of a set of n numbers. Mathematically, we can write

$$M e a n = \frac{\left[\sum_{i=1}^{n} x_{i}\right]}{N}$$

The Mean Wind Speed V can be calculated by the formula.

$$V = \sum_{i=1}^{n} V_{i} P(V_{i})$$

Where Vi is the central wind speed of bin 1 and P(Vi) is the probability/relative frequency that the wind speed has in bin i.

3.6.2 Variance:

It is one of the several indices of variability that statistician, use to characterize the dispersion among the measures in a given set of data. Mathematically, variance is written as

Variance =
$$\sigma^2 = \sum (X_i - V)^2$$

Where V is mean of data set

In case of wind speed data, we can write it, as

$$\sigma^2 = \sum V_i^2 P(Vi) - (V)^2$$

3.6.3 Standard Deviation

It is the square root of the variance, denoted by σ

$$\sigma^2 = (\sigma)^{1/2} = \sum (V_i^2 P(V_i) - (V)^2)^{1/2}$$

3.7 Wind power density:

While investigating a wind power potential of an area, the average values of wind speed does not truly represent this potential because lot of information regarding frequency distribution of wind speed is suppressed in the process of averaging wind speed. As such the most important values for estimating the wind power potential of a given site is the value of the wind power density or the available theoretical instantaneous power from the wind. This available wind power in the wind is the flux of Kinetic Energy crossing the wind energy conversion system and its cross – sectional area.

Like water flowing in the river, wind contains energy that can be converted to electricity using wind turbines. The amount of electricity that wind turbines produce depends upon the amount of energy in the wind passing through the area swept by the wind turbines blades in a unit of time. This energy flow is referred to as the wind power density.

A key aspect of wind power density is its dependence on wind speed cubed. This means that the power contained in the wind increases very rapidly with wind speed; if the speed doubles, the power increases by a factor of eight. In practice, the relationship between the power output of a wind turbine and wind speed does not follow a cubic relationship. Below a certain minimum speed, the turbine does not have enough wind to operate, whereas above a certain speed its output levels off or begins to decline. In very high winds the turbine may even be shut down to prevent damage to it.

Wind power density also depends on air density. At higher attitudes, air density decreases and, as a result, so does the available power. This effect can reduce the power output of wind turbines on high mountains by as much as 40 percent compared to the power that could be produced at the same wind speeds at sea level. Air density depends inversely on temperature: colder temperatures are favorable for higher air densities and greater wind power production.

3.7.1 Wind power classes:

To simplify the characterization of the wind power potential, it is common to assign areas to one of seven wind classes, each representing arrange of wind power density at the special height above the ground. The standard International wind power classifications are shown in Table 2.

	Разация	30m I	Height	50m I	Height
Class	Resource Potential	Wind Speed m/s	Wind Power W/m²	Wind Speed m/s	Wind Power W/m²
1		0 - 5.1	0 - 160	0 - 5.6	0 - 200
2	Marginal	5.1 - 5.9	160 - 240	5.6 - 6.4	200 - 300
3	Moderate	5.9 - 6.5	240 - 320	6.4 - 7.0	300 - 400
4	Good	6.5 - 7.0	320 - 400	7.0 - 7.5	400 - 500
5	Excellent	7.0 - 7.4	400 - 480	7.5 - 8.0	500 - 600
6		7.4 - 8.2	480 - 640	8.0 - 8.8	600 - 800
7		8.2 - 11.0	640 - 1600	8.8 – 11.9	800 - 2000

Table-2: International Wind Power Classification

By and large, the areas being developed today using large wind turbine are ranked as class 5 and above. Class 4 areas are also being considered for further development as wind turbines are adopted to run more efficiently a lower wind speeds. Class1 and class2 areas are not being deemed suitable for large machines, although a smaller wind turbine may be economical in areas where the value of the energy produced is higher

3.7.2 Power of wind Energy:

A parcel of Wind possesses kinetic energy

$$E = \frac{1}{2}mV^2$$

From this, power density is calculated as

$$P = \frac{e}{t} = \frac{1}{2} \frac{dm}{dt} V^2$$

Where $\frac{dm}{dt}$ is the mass of air following time.

From fluid dynamics, it can be proved that

$$dm/_{dt} = \varphi AV$$

Volume of cylindrical cross section can be written as

$$V = \pi r^2 L \qquad ---- \qquad (1)$$

Where r is radius of cylinder and L is length of it.

The wind moving with velocity V travels this distance L in time t so

$$S = L = Vt$$

So equation L takes the form

$$V = \pi r^2 V t$$

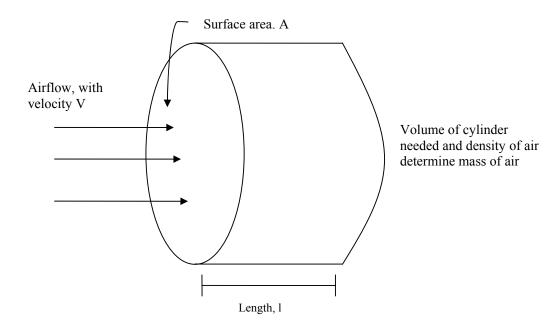
Now mass of wind can be written as

$$M = \varphi A v t$$

Differentiating

$$dm/_{dt} = \varphi AV d/_{dt(t)} = \varphi AV$$

Where φ is density of wind and others parameters have been defined in diagram.



So the power is then,

$$P = \frac{1}{2} \frac{dm}{dt} V^{2} = \frac{1}{2} \varphi AVT / t V^{2}$$
$$= \frac{1}{2} \varphi AV^{3}$$

And power density

$$P/_A = 1/_2 \varphi V^3$$

Density of wind at mean sea level is 1.225 kg/m³

At 15° C, The area depends upon the size of the rotor. Therefore, it is clear that power density chiefly depends on wind velocity and goes up as a cube of it.

3.7.3 Wind power calculation using Mean wind Speed:

Wind power calculated from Mean wind speed is not true representative of wind power. In real world, the wind varies constantly. Actual wind power density at most sites can rang from 1.0 to 3 times greater then that calculated. For example, we take wind speed of 5, 7 and 8 m/sec respectively the respective power densities are 76 wat/m², 210 watt/m² and 313 watt/m². The average of which is 200 watt/m². On the other hand, the average wind speed is 6.7 m/sec and power density of average wind is 181 watt/m². So the power of wind calculated by mean wind speed is less than the actual power present in wind i.e. Mean wind speed is not true representative for the wind power calculations.

To overcome this drawback we find some alternative arrangement, which reduces the deficit. The Weibull distribution is the best fit of wind data to calculate wind power based on mean wind speed and variance/standard deviation.

3.7.4 Weibull distribution:

The Weibull distribution (named after the Swedish physicist W. Weibull, who applied it when studying material strength in tension and fatigue in the 1930s) provides a close approximation to the probability laws of many natural phenomenon. It has been used to represent wind speed distribution for application in wind loads studies for sometime. In recent years most attention has been forced on this method for wind frequency applications not only due to its greater flexible and simplicity but also because it can give a good fit to experimental data.

The Weibull distribution function, which is a two-parameter function, has been found to fit much wind data with acceptable accuracy is expressed mathematically as

$$\phi(u) = \frac{k}{c} \left(\frac{u}{c}\right)^{k-1} \exp\left(-\left(\frac{u}{c}\right)^{k}\right)$$

Where:

u is the wind speed

c is the scale parameter with units of speed

k is the shape parameter and is dimensionless

When k = 2 the distribution reduces to Rayleigh distribution and if k=1 an exponential distribution is found. These are special cased of Weibull distribution.

Solving the equation, we find that the scale factor c is closely related to the mean wind speed for the site.

$$\overline{u} = c\tau \left(1 + \frac{1}{K}\right)$$

Where au is the complete gamma function

Similarly

$$\overline{u^n} = c^n \tau \left(1 + \frac{n}{k}\right)$$

And so

$$\overline{u^3} = c^3 \tau \left(1 + \frac{3}{k} \right)$$

The available power density is obtained:

$$E = \frac{1}{2}\varphi c^3 \tau \left(1 + \frac{3}{k}\right)$$

Where

E is the power density in watts / m^2

The shape factor k is related to the variance of the wind

$$\sigma^{2} = c2 \left[\left(1 + \frac{2}{k} \right) - \left(\tau \left(1 + \frac{1}{k} \right) \right)^{2} \right]$$

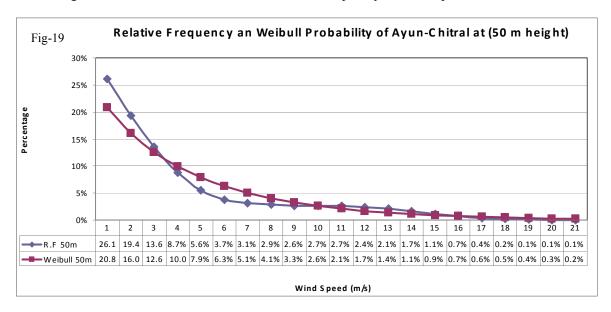
The two Weibull parameters k and c may be derived from site data.

A measure of the confidence of the fit of the Weibull curve to the real data is also returned. Often the Weibull curve is a good fit to the most of the data, but a poor fit to some. If the poor fit is in the low wind speed range, i.e. below cut in it may be possible to ignore the poor fit as this portion of wind does not contribute greatly to the overall power production.

The mathematical description of the wind frequency allows us to match with the turbine power curve. Thus a measure of the average total power capture in a year is achieved. Additionally the choice of turbine cut in and furling speed may be chosen to maximum the total energy capture.

3.7.5 Weibull Parameters:

Fig-19 shows the Weibull fit to the relative frequency of wind speed.



The Weibull parameters for three different heights 10 meters, 30 meters and 50 meters are given in Table-3 along with other key results of analysis. If we look at the shape parameters K and scale parameter C for 50 meters height we can find that the shape parameter K varies over a wind range from the lowest of 0.76 during July to the highest of 1.49 during the month of June with a annual value of K being 1.11.

The lowest values of the scale parameter C 1.15 is observed in July while the highest value of 7.56 is obtained in August and with an annual value of 3.60.

3.7.6 Average Wind Speed & Standard Deviation:

In Table-3 monthly average wind speed and standard deviation at three different heights are also given. The average wind speed values for 10 meters and 30 meters height have been obtained from the recorded data, whereas the values for the 50 meters height have been computed by using the power law as explained in the earlier section.

At 10 meters height the annual average wind speed is 1.89 m/s with Standard deviation of 1.63, at 30 meters this average speed is 2.78 m/s with Standard deviation of 2.48.

At 50 meters the monthly average wind speed varies from the lowest of 1.36 m/s in July to highest of 4.25 m/s during June. Whereas the average wind speed is 3.44 m/s with Standard deviation of 3.05.

3.7.7 **Power Density:**

The monthly power densities for three different heights 10meters, 30meters and 50meters have also been given in Table-3. At 10 meters this power density varies between 1.21 W/m² November to 31.52 W/m² in December with Average of 34.70 W/m².

At 30 meters height the power density varies from 8.85 W/m^2 in December to 234.02 W/m^2 in August and the average values is about 85.61 W/m^2 .

At 50 meters height the power density of Ayun-Chitral varies from 17.04 W/m² in December to 566.29 W/m² in August. The average power density of the area is 168.28 W/m².

Table-3: Monthly Average Wind, St. Deviation and Wind Power Density at Ayun-Chitral

		10 m			
	Avg V (m/s)	St Dev	C (m/s)	K	P/A (w/m²)
January	1.68	1.53	1.89	1.10	17.81
February	5.12	3.63	5.78	1.45	251.41
March	1.68	1.53	1.74	1.10	13.77
April	1.60	1.54	1.62	1.04	13.52
Мау	1.69	1.78	1.65	0.95	20.39
June	2.29	2.00	2.41	1.16	31.52
July	1.07	1.23	1.00	0.87	6.76
August	2.42	1.77	2.65	1.40	26.10
September	2.12	1.85	2.23	1.16	24.81
October	1.25	1.18	1.28	1.06	6.22
November	0.74	0.68	0.77	1.10	1.21
December	1.02	0.91	1.07	1.14	2.92
Average	1.89	1.63	2.01	1.13	34.70
	1	30 m	-		
	Avg V (m/s)	St Dev	C (m/s)	К	P/A (w/m²)
January	2.44	2.16	2.75	1.14	49.54
February	2.35	2.12	2.65	1.12	46.54
March	2.44	2.16	2.55	1.14	39.44
April	2.85	2.67	2.93	1.07	72.04
May	3.11	3.21	3.06	0.97	120.58
June	4.21	3.44	4.51	1.24	169.99
July	1.22	1.53	1.06	0.78	13.69
August	5.12	3.63	5.65	1.45	234.02
September	4.32	3.77	4.54	1.16	211.60
October	2.49	2.40	2.53	1.04	51.65
November	1.28	1.37	1.24	0.93	9.36
December	1.59	1.28	1.71	1.26	8.85
Average	2.78	2.48	2.93	1.11	85.61
		50 m			
	AvgV (m/s)	St Dev	C (m/s)	K	P/A (w/m²)
January	2.94	2.63	3.32	1.13	89.71
February	2.75	2.46	2.88	1.13	57.60
March	2.94	2.63	3.07	1.13	70.84
April	3.61	3.41	3.70	1.06	149.01
May	3.98	4.12	3.91	0.96	254.51
June	4.24	2.93	4.80	1.49	136.11
July	1.36	1.75	1.15	0.76	21.10
August	6.86	4.88	7.56	1.45	566.29
September	5.72	5.06	5.99	1.14	505.77
October	3.28	3.27	3.28	1.00	128.85
November	1.60	1.83	1.48	0.86	22.57
December	1.96	1.60	2.10	1.25	17.04
Average	3.44	3.05	3.60	1.11	168.28

ESTIMATING WIND GENERATED ELECTRIC POWER OUTPUT

Appendix-I

Monthly Average Diurnal Variation of Wind Generated Electric Power Output.

Appendix-II

Hourly Wind Generated Electric Power Output

4.0 Estimating Wind Generated Electric Power Output

The average power output of wind energy conversion technologies (WECT) is a very important parameter since it determines the energy output over time thereby influencing the economic feasibility of a wind project. It is by far more useful than the rated power, which does not account for the variability of wind velocity thereby easily overestimating energy revenues. The average power of wind turbine, $\overline{P_{WT}}$, is the power produced at each wind speed multiplied by the fraction that wind speed is experienced, integrated over all possible wind speeds. In integral form this can be expressed as (Manwell et al., 2002; Borowy and Salameh, 1996):

$$\overline{P_{WT}} = \int_{0}^{\infty} P_{WT}(v) df(v)$$

This integral can be replaced with a summation over bins, N_{B_s} to calculate the average wind turbine power (Manwell et al., 2002).

$$\overline{P_{WT}} = \sum_{j=1}^{N_B} \left\{ \exp \left[-\left(\frac{v_{j-1}}{c}\right)^k \right] - \exp \left[-\left(\frac{v_j}{c}\right)^k \right] \right\} P_{WT} \left(\frac{v_{j-1} + v_j}{2}\right)$$

Please note that the relative frequency, f_j/N , corresponds to the term in brackets and the power output is calculated at the midpoint between v_{j-1} and v_j .

The available power at any given wind speed v that is convertible by a turbine is defined by (Manwell et al., 2002 Johnson, 1985)

$$P_{WT}(v) = \frac{1}{2} \rho A C_p \eta v^3$$

Where η is the drive terrain efficiency (i.e. generator power/rotor power), C_p , is the machine power coefficient. In an idealized wind turbine no losses are experienced and the power coefficient, C_p , is equal to Betz' limit (i.e. $C_{p,Betz}=16/27$) and $\eta=1$. Of course, in reality both the drive terrain efficiency and the power coefficient cannot be maximized. The extent to which the power output is limited by physical laws as well as engineering inefficiency is dependent on the specific characteristics of individual wind turbine types. This aspect will be discussed further in the analysis of the case study.

WECTs have a range of different power output performance curves, which need to be recognized when estimating the potential power output. The power output performance curves are not only defined by parameters such as the power coefficient and the drive terrain efficiency but also constrained by cut-in speed, furl-out speed and rated wind speed. Where the cut-in wind seed, v_c , is the minimum wind velocity to generate power from a turbine, the rated wind speed, v_R , is the wind speed at which the 'rated power' of a WETC is achieved and generally corresponds to the point at which the conversion efficiency is near its maximum and furl-out wind speed, v_F , is the wind speed at which the turbine shuts down to prevent structural damage.

To account for the above-mentioned constraints we can formulate a novel formula for the average electrical power output of a turbine, $\overline{P_{WTA}}$:

$$\overline{P_{WTA}} = \begin{cases}
\sum_{j=1}^{N_B} \left\{ \exp\left[-\left(\frac{v_{j-1}}{c}\right)^k\right] - \exp\left[-\left(\frac{v_j}{c}\right)^k\right] \right\} P_{WT}\left(\frac{v_{j-1} + v_j}{2}\right) & (v_c \le v \le v_R) \\
\overline{P_{WTA}} = \left\{ \sum_{j=1}^{N_B} \left\{ \exp\left[-\left(\frac{v_{j-1}}{c}\right)^k\right] - \exp\left[-\left(\frac{v_j}{c}\right)^k\right] \right\} P_{WT}(v_r) & (v_R \le v \le v_F) \\
0 & (v < v_c \text{ and } v > v_F)
\end{cases}$$

The energy production of the wind turbine WE(t) over time t can thus be calculated as

$$WE(t) = \overline{P_{WTA}}t$$

Another way of stating the energy output from a wind turbine is to look at the capacity factor for the turbine in its particular location. The capacity factor CF, is the actual energy output over a given period of time, WE(t), divided by the theoretical maximum energy output (i.e. this means that the machine is constantly running at its rated output) during the selected time-span, RO(t). This can be formulated as

$$CF = \frac{WE(t)}{RO(t)}$$

Theoretically capacity factor vary from 0 to 100%. In practice they usually range from 20 to 70% and mostly be around 20-30 percent. However, the economic feasibility of a wind turbine does not of course depend on the capacity factor of a wind turbine alone but also depends on the costs of alternative power systems. Therefore, a low capacity factor does not automatically render a wind turbine project unfeasible.

In order to maximize the energy output of a given wind regime the optimum wind speed, v_{opt} , needs to be determined. The optimum wind speed indicates at what wind velocity most energy is available in a given wind regime. It is at this particular wind speed that engineers should ensure that the power coefficient is most efficient to allow for the highest energy conversion of a turbine. The optimum wind speed can be calculated as follows (Lu et al., 2002):

$$v_{opt} = c \left(\frac{k+2}{k}\right)^{\frac{1}{2}}$$

In this regard, the power density of a turbine is a good comparative indicator to show the average power output per m^2 of wind swept area, A, at a given site. This can be defined as

Power Density =
$$\frac{\overline{P_{WTA}}}{A}$$

Another important aspect of that critically determines the energy output of a turbine is elevation. In many cases the available recorded wind speed data has been measured at a lower level than the planned hub height of the wind turbine. As wind velocity increases vertically the recorded wind speed data can be adjusted using the following standard formula (Borowy and Salameh, 1996.) where ν is the projected wind speed, ν_i the wind speed at reference height, H the hub height of a turbine, Hi the reference height and α the power-law exponent.

$$v = v_i \left(\frac{H}{H_i}\right)^{\alpha}$$

 α is often quoted to have a value of 1/7 and is seen as a reasonable power law exponent for even and unobstructed landscapes. However, where WECT development is planned either offshore or near woodlands or close to any other non flat terrains this value can differ subsequently and a more through analysis of α is necessary. Justus as well as Counnihan offer mathematical solution for 'fitting' α to these environments (Manwell et al., 2002).

4.1 Hypothetical Wind Generated Electric Power:

A **wind turbine** is a machine for converting the kinetic energy in wind into mechanical energy. If the mechanical energy is used directly by machinery, such as a pump or grinding stones, the machine is usually called a windmill. If the mechanical energy is then converted to electricity, the machine is called a wind generator.

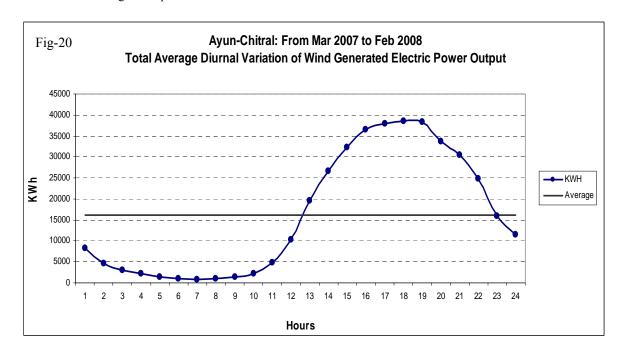
Hypothetical wind generated electric power output at Ayun-Chitral has been estimated by using the 600KW wind turbine bonus 600/44 MK IV type. The cut in wind speed of this turbine is 3m/s and cutout wind speed is 25m/s. Rotor diameter of this turbine is 44 meters and hub height has been taken as 50 meters. The monthly and annual wind generated electric power outputs at Ayun-Chitral are shown below in graphs and table-4.

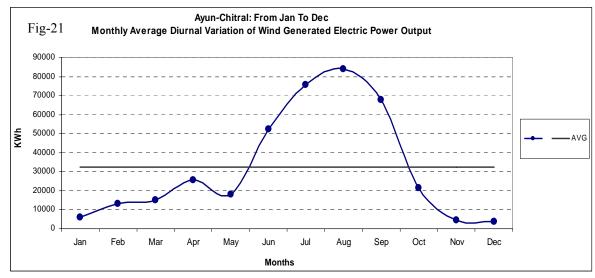
Table-4: Hypothetical wind generated electric energy output & capacity Factor for a Bonus 600/44MK IV Turbine at Ayun-Chitral.

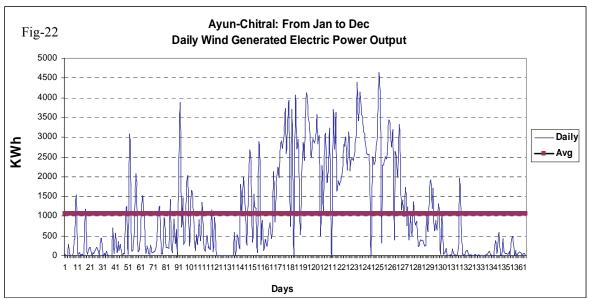
	PMD (Calculator (using	g 50M)	
Month	Input W/m ²	Output W/m ²	C.F.	KWh / Month
January	95	30	8%	33,866
February	61	21	5%	21,835
March	75	25	6%	27,876
April	157	42	11%	45,580
May	264	52	13%	58,947
June	144	49	12%	53,910
July	22	7	2%	7,561
August	597	122	31%	137,697
September	524	91	23%	99,295
October	136	36	9%	40,314
November	24	8	2%	8,421
December	18	6	2%	6,814
Annual	125	37	9%	491,091

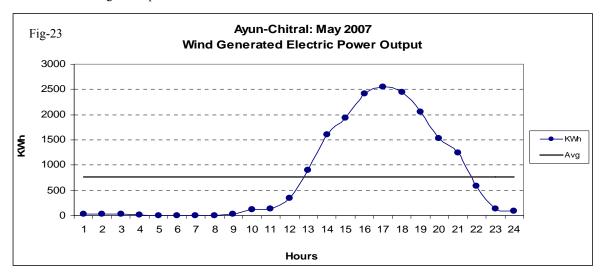
Wind Turbine spe	cification
Turbine	Bonus 600 / 44 MK IV
Power	600 KW
Cut in Wind	3 m/s
Cut out wind	25 m/s
Rotor Diameter	44 m
Hub height	50 m

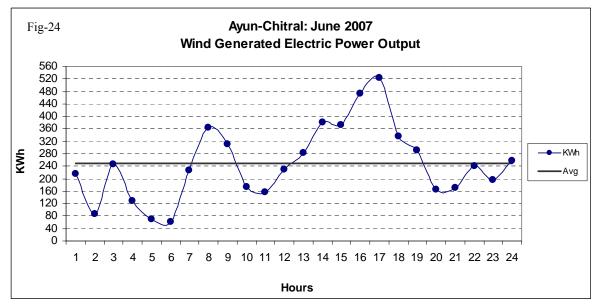
Figure 20 shows the average diurnal variation of wind generated electric energy output at Ayun-Chitral (March-Feb). The graph shows that the maximum power is produced at about 18 PM; of course, this is the same time when we have the maximum wind speed in 24 hours. Figure 21 & 22 shows the monthly and daily wind generated electric power output. Figure 21 depicts that at Ayun-Chitral the wind have more potential in the month of August as compared to other months. Figure 23 to 34 shows the monthly average diurnal variation of wind generated electric energy output.

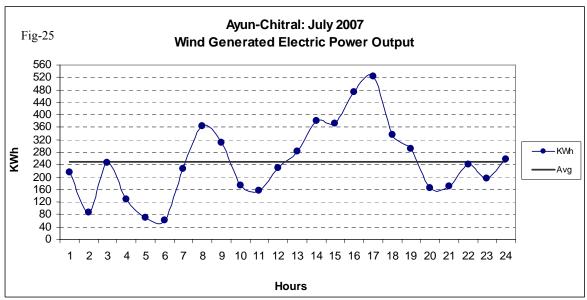


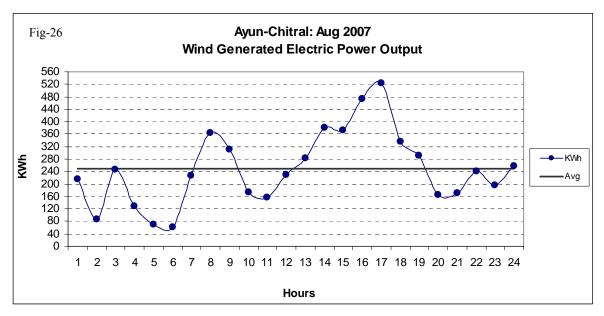


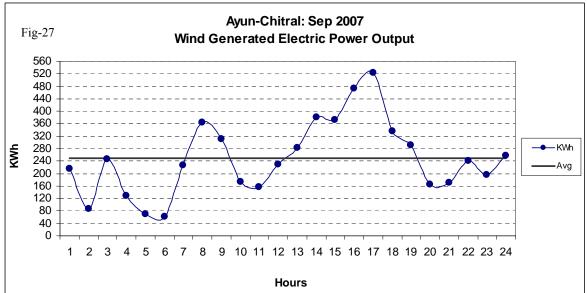


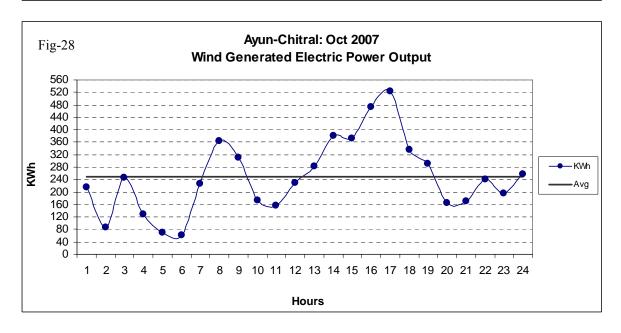


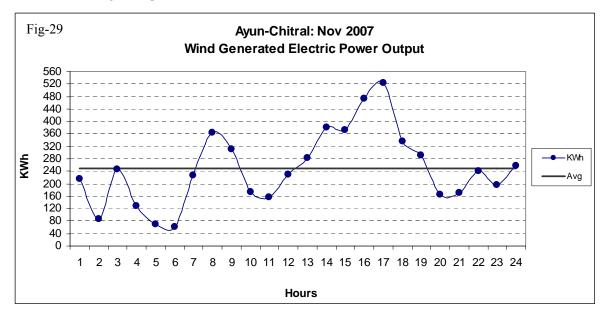


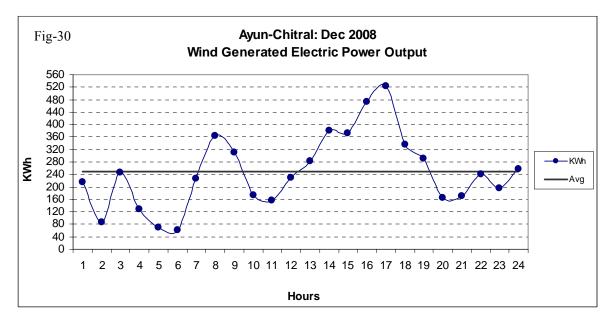


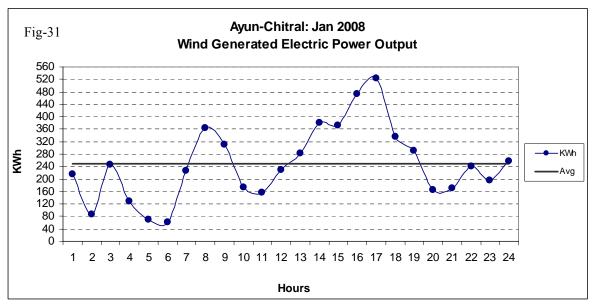


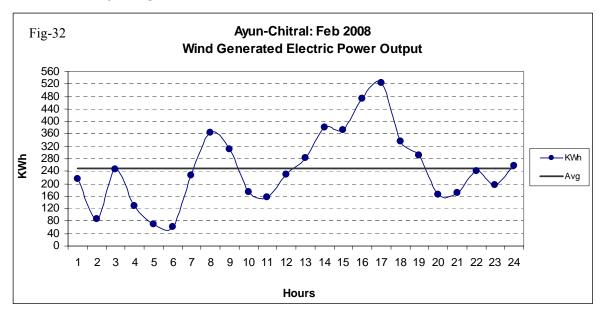


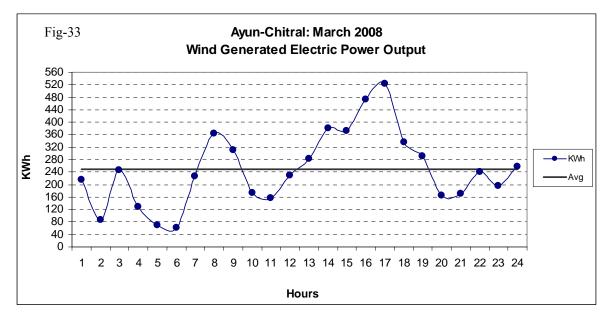


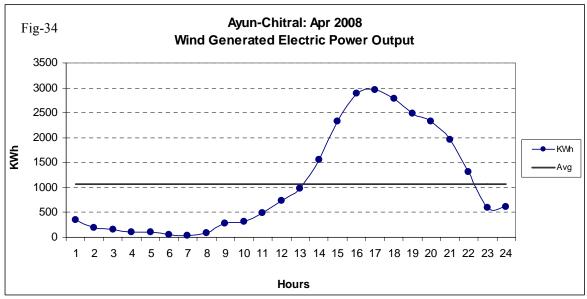










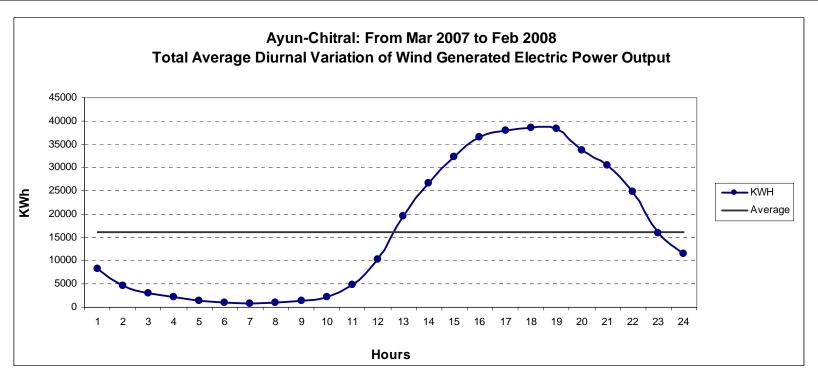


Appendix-I

Ayun-Chitral May 2007 to April 2008

Wind Power Output of Bonus 600/44 Turbine (12 Month's Summary)

Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
Jan	215.7	85.47	245.92	129.87	70.47	62.13	227.1	364.7	312.16	172.9	155.6	229.88	281.69	380.72	372.33	473.13	523.81	336.59	290.59	164.53	171.4	241.69	197.15	258.93	5964
Feb	190.7	107.8	132.96	115.39	112.36	160.28	140.3	113.5	101.51	151	321.3	884.77	1553.97	1614.32	1581.82	1497.47	1174.13	871.38	688.63	473.29	296.69	231.67	256.48	288.49	13060
Mar	517.5	290.4	135.16	111.56	71.36	26.23	11.87	13.43	6.41	12.29	79.23	333.21	801.88	1381.78	1811.12	1539.96	1730.26	1494.47	1131.41	865.23	1051.27	1188.77	381.38	263.86	15250
Apr	356.4	199.6	150.24	100.07	102.23	53.48	38.86	83.77	279.46	322.6	493.5	731.48	984.09	1558.85	2324.82	2887.97	2957.62	2775.74	2480.66	2328.8	1960.37	1317.46	599.22	610.28	25698
May	29.07	28.9	22.55	12.51	2.34	1.56	4.68	2.34	26.42	118.5	135.3	340.06	901.28	1601.75	1929.87	2419	2557.28	2440.38	2047.9	1536.29	1245.77	590.1	138.17	82.57	18215
June	1426	882.9	620.18	481.3	325.55	200.27	130.2	149.6	306.74	750.7	1118	1383.48	2309.77	2772.09	3111.53	3764.56	4109.36	4870.08	4995.34	4695.35	4776.45	4111.09	2820.87	2059.16	52171
July	1839	682.1	580.98	498.09	136.87	154.48	51.29	4.63	46.83	248.6	1224	2102.97	3675.21	4802.33	5692.73	6720.19	6516.43	7059.72	7890.22	7262.28	6881.46	5682.47	3549.17	2432.72	75735
Aug	2336	1605	730.5	450.97	316.34	226.88	63.41	4.46	0.39	150.7	645.2	2634.86	4621.84	5962.23	6411.61	6817.39	6973.03	7399.05	8025.27	7384.99	7177.84	6130.73	4535.76	3279.08	83884
Sep	1078	506.9	300.56	172.63	51.58	8.75	9.39	182	251.04	43.73	422.6	1511.84	3827.48	5077.52	6163.4	6530.66	6859.04	6525.96	7120.48	6646.87	5477.46	4404.99	2880.25	1833.35	67886
Oct	166.3	54.21	13.38	79.85	139.06	15.94	17.19	56.12	83.48	224	116	112.27	337.85	1157.33	2414.88	3171.09	3425.64	3100.97	2481.82	1754.19	1122.99	750.04	407.59	215.5	21418
Nov	19.79	19.06	17.45	10.92	25.89	26.99	21.69	15.94	18.79	6.8	0	2.34	53.57	116.78	348.24	446.31	743.79	785.04	694.32	427.87	207.96	183.37	127.28	28.65	4348.8
Dec	72.83	123.2	128.56	33.67	19.62	34.38	62.43	19.4	17.36	21.99	52.44	116.9	197.87	123.55	69.74	222.78	417.96	795.28	509.18	186.19	116.2	49.21	128.12	92.17	3611
KWH	8248	4585	3078	2197	1374	971	778	1010	1451	2224	4763	10384	19547	26549	32232	36491	37988	38455	38356	33726	30486	24882	16021	11445	387241
Average	16135	16135	16135	16135	16135	16135	16135	16135	16135	16135	16135	16135	16135	16135	16135	16135	16135	16135	16135	16135	16135	16135	16135	16135	



Ayun-Ch	itral	N	/lay 2	2007							W	ind Po	ower C	Output	of Bo	nus 6	00/44	Turbii	ne (Mo	nth's	Sumr	mary)			
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
10	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
11	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
12	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
13	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
14	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
15	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	134.8	273.2	164.3	4.6	2.9	580
16	0.0	0.0	7.8	1.2	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	9
17	0.0	0.8	1.6	0.8	0.4	0.0	0.0	0.4	0.0	0.0	2.5	0.4	0.4	12.4	66.6	64.2	122.0	98.2	33.6	11.7	30.1	23.0	48.0	0.0	517
18	9.2	16.6	7.1	7.1	0.4	0.4	8.0		0.4	57.7	21.1	47.9	56.0	30.2	26.2	19.4	62.0	11.6	0.4	0.0	0.4	0.0	7.4	0.0	382
19	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.8	0.0	6.1	51.8	48.1	30.6	0.8	2.9	1.2	2.9	9.2	0.8	12.0	14.9	1.2	0.0	184
20	0.0	0.0	0.0	0.4	0.0	8.0	1.2	0.0	0.0	0.0	0.0	0.0	125.3	223.2	125.7	270.5	284.6	314.0	341.2	98.1	0.4	0.0	0.0	0.0	1785
21	0.0	0.4	0.0	0.0	0.0	0.0	0.8		0.0	15.4	56.0	17.7	0.0	0.4	0.0	12.4	33.0	115.6	216.0	235.6	245.7	83.2	13.0	13.8	1059
22	18.3	10.3	1.6	1.2	0.0	0.0	0.8	8.0	0.0	0.4	0.0	2.1	73.7	154.8	323.1	252.9	318.0	307.5	226.0	241.1	51.6	0.8	1.2	1.2	1987
23	0.4	0.0	0.4	0.0		0.4			0.0	0.0			87.9	103.9	114.2	33.8	276.6	295.0	200.0	52.2	64.5	22.8	0.4	0.0	1363
24	0.0	0.0	0.0	0.8			0.0		0.0	0.4			44.3	141.0	13.8		200.6	8.2	21.2	1.6	1.2	0.8	0.4	0.0	606
25	0.0	0.0	0.0	0.0		0.0		0.0	0.0	0.4	8.9		10.8	7.1	1.2	4.1	58.5	194.3	4.2	0.0	0.0	2.9	0.0	0.0	294
26 27	0.0	0.0	2.5	0.0		0.0		0.0	24.1	36.4	2.9		0.0	113.8	250.7	240.3	207.3	230.5	145.8	122.0	45.1	19.4	0.0	0.0	1441
	0.0	0.4	0.8		0.0		0.0		1.2	1.2			137.7	331.4	304.0	331.0	234.0	259.4	328.1	302.6	208.7	131.5		2.5	2670
28	0.0	0.0	0.0	0.0			0.0		0.0	0.0			114.8	182.8	238.5		322.8	279.7	326.8	143.8	152.3	33.4	4.6	35.4	2240
29 30	0.4	0.4	0.0	0.4	1.6		0.8		0.0	6.8			21.4	17.3	73.9	195.9	10.3	0.8	0.8	0.0	0.0	0.0	0.0	0.0	348
	0.0	0.0	0.0	0.0		0.0			0.0	0.0		10.3	133.0	165.0	269.4	328.7	326.7	208.7	64.2	8.3	0.0	0.0	0.0	0.0	1515
31	0.8	0.0	0.8				0.0		0.0	0.0		2.9	47.9	87.9	122.0	145.8	99.8	114.1	130.6	183.9	160.6	93.1	15.8	26.8	1233
KWh	29	29	23	13	2	2	5	2	26	119	135	340	901	1602	1930	2419	2557	2440	2048	1536	1246	590	138	83	18215

Ayun-Cl	hitral	Jui	ne 20	07		.0																			
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	12.7	13.8	12.1	3.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4	10.4	114.1	161.1	169.7	145.9	54.6	43.6	193.6	143.7	85.6	24.5	1189
2	5.4	2.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.8	2.9	14.9	93.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	120
3	168.0	77.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	53.0	224.1	355.3	336.4	340.4	326.7	215.2	259.5	191.8	130.0	97.7	40.9	0.8	0.4	2817
4	0.4	0.8	0.8	0.0	0.0	0.0	0.0	0.4	0.0	0.4	3.7	79.0	208.6	272.5	252.2	259.8	229.7	145.0	176.7	176.7	110.1	19.0	10.8	176.7	2123
5	153.6	23.0	0.0	1.2	0.0	1.2	0.4	27.3	29.6	26.0	47.4	0.0	0.0	0.0	0.4	2.5	0.0	0.0	0.0	0.4	0.4	0.0	0.8	1.6	316
6	0.4	0.4	0.4	0.4	0.0	0.8	3.3	1.6	0.0	0.0	10.3	0.0	0.0	40.2	88.7	129.8	102.2	145.8	225.8	79.2	45.1	0.8	9.3	4.1	888
7	3.3	5.4	0.4	0.0	0.4	0.0	0.8	0.4	0.0	0.0	0.0	0.8	3.3	5.0	11.7	12.1	5.0	10.0	14.0	21.7	30.2	19.4	5.4	0.4	150
8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	28.4	36.4	24.0	22.8	2.3	0.4	3.7	37.7	92.7	78.4	36.9	20.0	27.3	10.3	421
9	3.7	0.0	2.3	4.1	26.8	16.2	3.7	0.4	0.0	0.0	15.4	43.1	43.1	18.3	21.2	8.2	0.0	0.0	5.3	19.4	10.3	0.0	0.4	0.4	242
10	0.4	0.0	1.6	2.9	0.8	0.0	1.2	3.3	0.8	1.2	40.9	54.7	39.8	33.6	4.1	0.8	0.4	0.0	2.5	21.7	13.2	4.2	12.0	0.0	240
11	0.4	0.0	1.6	8.9	5.8	0.0	0.4	0.0	0.0	0.0	0.0	0.8	0.0	25.8	48.5	35.2	46.4	92.7	22.8	42.8	94.8	40.2	38.9	47.9	554
12	18.3	12.1	7.1	7.5	0.8	0.0	0.0	0.0	0.0	7.8	2.5	0.4	88.9	48.5	60.8	70.3	73.7	68.9	87.9	102.9	85.3	82.4	7.1	9.2	842
13	24.0	24.0	20.1	5.0	2.0	1.6	0.8	0.8	0.0	2.3	7.5	16.6	5.8	13.8	44.5	59.4	73.7	49.9	36.4	10.0	11.0	25.6	7.5	0.8	443
14	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	21.7	39.8	51.3	24.0	30.2	3.3	2.5	1.6	16.5	68.9	92.0	123.6	107.7	73.7	129.8	114.1	900
15	92.7	99.8	168.7	160.9	122.0	122.0	64.2	36.4	26.8	26.8	27.4	37.7	11.7	0.4	0.8	16.6	63.2	90.3	266.7	231.3	126.0	107.7	122.7	99.8	2122
16	92.7	87.9	64.2	51.3	29.0	0.0	0.8	0.0	5.3	26.8	36.4	27.4	3.3	16.0	2.1	7.4	61.8	107.7	129.8	72.7	27.1	2.9	0.4	3.3	856
17	16.6	8.2	2.9	0.4	0.0	0.0	0.0	0.0	0.4	39.8	30.7	9.3	0.4	0.4	0.4	44.5	85.2	309.4	254.6	238.3	315.4	250.7	95.1	48.3	1751
18	9.2	12.1	18.3	12.1	1.6	3.3	1.2	0.0	0.0	0.0	0.0	6.1	24.0	71.3	80.8	184.6	168.7	258.7	302.6	252.2	292.7	284.6	130.8	133.1	2248
19	161.7	94.8	5.3	5.4	16.6				0.0		2.1	1.2	0.0	2.9	5.4	68.9			321.7	309.9	275.8	266.0	105.3	5.4	1982
20	22.2	33.6	12.1	12.7	9.3																		191.4		2520
21	130.8	30.4	17.7	14.9	5.0		0.4																	6.4	2915
22	16.6	16.5	0.0	7.1	26.8																			152.9	2720
23	75.0	33.6	24.0	11.0	13.8																		198.5	33.2	3196
24	0.4	3.7	0.0	0.0	0.0																				3711
25	249.9	243.4	245.0	168.7	65.1	5.7	43.8		201.0	290.1	174.9	3.3	4.6	1.2			62.1		40.7	7.8	86.7		144.8	153.6	2590
26	14.0	2.5	0.4	0.0	0.0	0.0	0.0		2.5	5.0	7.8	73.0	207.1	266.7			332.9			296.6			109.5	24.7	3226
27	0.0	0.0	0.0	0.0	0.0	0.0	0.0		2.0	84.0	216.8	266.0	240.5								345.7				3869
28	12.1	9.3	10.0	2.9	0.0	0.0	0.0		0.8	0.0	0.0	0.4	148.8							0.0	0.0		0.0	0.0	743
29 30	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.4	0.8	4.6	16.6			312.0										3646
KWh	141.9	48.2	5.4	0.4	0.0	0.0	0.0		1.6	0.4	2.0	8.2	117.9		259.5						231.3		30.2	2.5	2830
rvvn	1426	883	620	481	326	200	130	150	307	751	1118	1383	2310	2772	3112	3765	4109	4870	4995	4695	4776	4111	2821	2059	52171

Ayun-C	hitral	Ju	ly 20	07							Wir	nd Po	wer O	utput	of Bo	nus 60	00/44	Turbir	ne (Mo	onth's	Sumr	nary)			
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
2	243.4	184.1	176.1	230.5	41.3	0.0	0.0	0.0	0.4	1.2	36.9	79.5	216.0	279.7	307.0	347.0	256.0	254.6	333.5	279.7	272.5	184.8	145.8	114.8	3985
3	37.7	2.9	0.0	0.8	1.6	2.9	0.0	0.0	0.4	4.1	9.3	14.9	32.1	118.0	129.8	183.9	293.8	304.8	352.7	302.8	335.9	230.5	100.6	267.1	2726
4	168.9	42.2	1.2	17.7	9.3	0.4	0.4	0.0	0.0	0.4	0.0	12.1	47.9	95.1	192.0	297.6	301.0	246.5	363.2	350.1	314.0	266.0	145.9	68.9	2941
5	9.2	0.0	10.0	7.1	16.2	16.6	0.8	0.0	0.0	0.0	12.0	49.9	123.5	199.9	207.9	288.8	314.0	270.7	278.2	191.4	270.9	230.5	95.8	32.7	2626
6	2.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.0	2.5	16.6	5.8	33.6	43.1	41.1	76.1	160.6	114.8	36.4	15.8	2.5	0.0	552
7	0.4	0.8	3.3	3.7	0.8	0.8	0.4	0.0	0.0	0.4	22.8	68.9	162.0	278.2	335.9	291.8	169.7	97.9	137.9	45.4	38.3	22.2	33.0	29.6	1744
8	10.3	8.2	0.4	0.0	0.0	6.8	0.0	0.0	0.0	1.6	5.0	32.6	71.3	114.8	168.5	221.7	251.4	270.0	295.9	272.3	304.0	302.6	222.5	284.6	2844
9	262.1	0.0	20.3	0.0	1.2	4.2	0.0	0.0	0.0	5.4	2.0	0.0	0.0	38.3	114.8	237.7	272.5	309.1	251.3	336.4	293.8	229.1	30.5	0.0	2409
10	10.6	16.6	12.8	1.6	0.0	0.0	0.0	0.0	0.0	0.4	0.4	17.7	63.2	152.9	251.4	280.3	331.6	358.1	304.2	348.3	297.6	253.0	273.2	238.5	3212
11	253.0	216.0	137.6	8.7	3.7	7.1	3.3	0.0	0.4	2.5	72.7	115.6	199.9	260.2	310.4	329.6	296.5	306.1	297.6	325.1	279.7	252.2	250.7	199.9	4128
12	184.1	69.2	10.3	13.8	8.5	39.8	27.4	2.5	0.0	9.2	38.3	85.6	114.8	153.6	245.8	334.4	328.9	354.5	321.2	312.0	278.3	296.0	302.6	122.2	3653
13	12.4	0.4	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.4	36.9	67.9	121.2	183.9	317.4	332.7	307.0	254.6	354.8	355.3	278.8	245.7	184.6	176.1	3230
14	125.1	5.3	0.8	2.9	2.9	5.4	1.2	0.0	0.0	0.0	68.7	184.8	199.4	216.0	253.4	331.3	323.9	283.7	241.9	227.5	172.2	2.5	0.4	0.0	2649
15	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	5.0	1.6	24.0	38.3	129.8	221.0	282.4	285.4	287.1	352.0	342.4	282.2	191.8	59.7	0.8	2504
16	0.4	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.0	1.6	64.3	99.8	160.8	183.8	273.2	257.9	229.7	232.3	333.7	329.8	270.9	192.0	200.7	118.0	2949
17	18.8	0.0	0.0	7.1	5.8	14.5	0.0	0.0	0.0	0.8	22.8	42.3	114.1	168.7	191.8	231.3	236.3	286.8	349.1	326.7	321.2	238.5	152.7	114.8	2844
18	91.7	2.1	0.4	14.9	12.1	8.2	0.0	0.0	0.0	5.3	30.2	36.4	92.7	184.8	223.2	265.2	258.7	245.0	296.1	347.4	299.1	321.9	223.2	45.3	3004
19	0.0	0.0	14.5	13.8	2.9	4.6	0.0	0.0	0.4	41.9	122.7	169.0	238.5	264.4	291.1	291.1	307.0	296.1	342.4	334.5	353.4	241.9	161.1	83.9	3575
20	10.4	11.3	18.3	26.8	7.5	2.9	0.0	0.0	0.0	4.9	76.1	92.7	122.0	192.8	176.5	296.9	361.8	203.1	359.0	300.5	285.5	198.5	64.2	26.9	2839
21	121.1	55.6	130.8	115.7	2.5	0.4	0.0	0.0	41.6	129.8	263.7	272.5	307.5	266.0	216.0	223.2	229.7	277.4	223.2	51.3	34.8	25.2	15.8	20.9	3025
22	30.7	26.8	18.3	5.0	3.7	3.3	0.8	0.0	2.5	6.4	0.0	0.0	0.0	0.4	0.0	4.9	58.6	11.4	1.2	0.4	67.7	105.9	24.8	125.9	499
23	71.7	12.8	0.0	0.0	0.0	0.0	0.0	0.0	0.8	1.2	0.4	16.2	192.6	153.2	89.1	99.7	40.8	288.2	290.2	252.2	290.2	323.9	139.7	9.6	2272
24	0.0	0.0	0.0	0.4	0.0	0.8	0.0	0.0	0.0	0.4	16.6	34.6	137.9	223.2	153.0	21.2	2.9	129.9	126.0	43.1	65.5	77.4	2.5	0.4	1036
25	0.8	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	24.0	87.9	168.7	200.7	129.8	141.6	257.9	245.0	237.8	244.2	230.5	215.2	56.4	2241
26	22.4	0.0	0.0	2.9	0.4	4.1	3.7	0.0	0.0	0.8	74.6	153.6	237.7	259.5	253.0	305.8	317.3	319.0	339.3	305.8	266.7	184.6	54.4	1.6	3107
27	0.0	0.8	1.2	0.8	0.0	0.0	0.0	0.0	0.0	1.2	0.0	0.0	0.0	0.0	29.9	122.7	160.8	258.7	296.4	292.6	273.1	270.9	130.8	19.6	1859
28	36.4	26.8	24.5	24.0	9.6	2.0	0.8	0.0	0.0	0.0	2.0	2.0	44.5	80.8	92.7	137.0	213.8	307.2	354.2	347.2	310.8	236.9	71.0	2.1	2326
29	0.0	0.0	0.0	0.0	7.1	28.6	10.3	2.1	0.0	2.1	98.8	197.7	207.9	129.1	115.6	228.1	184.6	273.1	289.6	289.6	343.8	311.8	245.7	272.5	3238
30	115.1	0.0	0.4	0.0	0.0	0.4	2.0	0.0	0.0	21.8	145.8	206.5	325.1	301.1	298.1	303.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1719
31	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
KWh	1839	682	581	498	137	154	51	5	47	249	1224	2103	3675	4802	5693	6720	6516	7060	7890	7262	6881	5682	3549	2433	75735

Ayun-Chitral August 2007 Wind Power Output of Bonus 600/44 Turbine (Month's Summary)

Ayun-C	nıtrai	Aug	just 2	007							VV	ina PC	wer c	Julpu	OT BO	ทเนร ช	00/44	Turbii	ne (ivid	วทเท 5	Sullii	nary)			
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	48.6	0.4	0.4	0.0	0.0	9.3	5.0	0.0	0.0	0.0	73.6	152.7	152.9	228.1	349.1	312.3	341.4	337.6	326.7	328.2	310.4	296.1	192.6	145.8	3611
2	73.3	11.7	0.0	0.4	0.0	3.3	2.5	0.0	0.0	0.0	0.4	30.7	146.5	192.0	251.4	302.6	145.8	132.7	220.1	199.9	262.1	238.5	192.6	289.6	2696
3	314.0	325.1	0.0	56.0	18.6	0.0	0.0	0.0	0.0	0.0	18.0	160.6	168.7	176.7	255.6	331.6	334.5	343.5	306.1	248.4	237.8	176.1	95.1	54.7	3621
4	77.4	12.8	7.4	27.4	16.6	13.8	4.2	0.0	0.0	0.0	0.0	9.2	56.4	114.8	114.8	176.7	166.7	241.7	263.7	118.1	114.8	110.8	5.7	0.4	1653
5	22.8	5.3	10.3	2.9	0.8	0.4	2.1	0.0	0.0	0.0	0.0	82.4	152.9	152.4	106.6	56.3	0.0	98.8	303.2	331.8	238.5	152.9	137.7	48.8	1907
6	21.1	9.6	30.7	6.5	0.8	0.0	0.0	0.0	0.0	0.4	0.4	85.7	245.7	169.7	103.9	47.9	3.3	50.0	91.7	40.9	343.7	251.1	179.0	98.2	1780
7	21.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	99.8	260.2	258.7	161.6	100.6	34.3	47.4	243.4	257.9	229.1	160.8	84.5	5.0	1965
8	12.6	9.9	24.0	21.2	9.3	9.6	0.0	0.0	0.0	0.0	0.0	30.1	176.9	184.1	184.9	145.0	229.8	307.5	247.6	130.0	160.1	145.8	80.7	13.3	2122
9	43.1	0.0	18.3	7.5	5.0	3.3	0.4	0.0	0.0	10.4	160.8	229.7	184.8	236.9	182.6	286.2	270.9	313.4	335.6	230.5	199.9	43.6	36.9	7.4	2807
10	0.0	0.0	0.0	0.0	0.0	0.0	2.9	0.4	0.0	0.0	0.0	22.8	126.0	283.9	237.7	258.7	314.0	316.9	312.5	269.4	245.0	270.0	112.7	2.1	2775
11	161.6	192.6	168.8	38.6	0.4	11.0	5.4	0.0	0.0	0.0	2.9	64.2	144.8	272.5	307.5	314.0	324.8	332.5	326.2	120.4	82.8	60.8	39.8	21.7	2993
12	7.5	6.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	7.1	110.8	243.4	176.8	37.4	152.9	297.6	248.4	192.6	221.8	167.6	192.9	100.6	2164
13	30.6	20.7	34.9	45.1	5.0	0.8	0.0	0.0	0.0	0.0	18.4	215.2	184.9	238.5	231.0	311.7	315.4	278.9	337.8	300.0	321.9	186.0	53.6	10.6	3141
14	0.0	6.4	4.6	0.0	0.4	0.0			0.0	2.9	45.3	228.3	184.8	308.9	283.9	254.1	201.4	263.7	207.3	67.9	64.2	36.9	7.4	1.2	2175
15	7.8	0.0	0.0	0.0	0.4	0.4	0.0	0.0	0.0	0.0	0.8	57.0	122.0	200.7	200.7	214.4	202.2	251.5	299.0	257.9	244.2	183.3	102.2	74.2	2419
16	8.2	1.2	0.8	0.4	0.0	0.4			0.0	0.0	19.0	38.9	121.2	137.7					284.6	230.5	184.6	200.7	225.0	183.5	2476
17	42.3	75.0	4.6	0.0	2.3				0.0	0.0	13.5	92.7					228.9		218.7	216.0			145.1	99.8	2414
18	87.9	82.9	0.4	3.3	11.7	2.5			0.0	0.0	0.0	3.3		95.1			208.1		300.3	303.2	291.1		207.9		2765
19	130.8	59.4	15.8	0.0	2.5	0.4			0.0	0.0	15.2	145.6				236.1	292.7	296.1	262.9	237.8	259.5		216.0	145.0	3244
20	91.4	164.2	148.4	114.8	153.6		10.8				145.8		168.7	152.7		321.6			297.6	326.5			257.2	229.2	4385
21	145.8	83.9	60.0	7.4	0.0	0.0			0.0	0.4	2.5		88.7	168.7		258.7	302.6		244.9	255.6	297.6		285.4	286.2	3414
22	265.2	243.4	156.9	83.2	56.0	14.5			0.0	0.0	62.2	122.0	215.2	184.8		256.5		263.7	256.3	342.4	295.2		256.4	266.0	4135
23	229.1	98.9	20.0	14.8	7.4	6.4		0.0		0.4	34.9			200.0		228.9	337.5		262.9	315.4	237.4		224.0		3605
25	84.9	2.5	2.9	2.9	2.9	2.0			0.0	0.0	31.5	160.9	258.7	252.2		292.7	277.4	223.2	235.5	275.9	313.4		277.4		3497
26	120.5	13.6	0.0	0.0	0.0	0.0			0.0	0.0	0.4	37.2	54.6			277.4	248.4		293.1	301.3			252.2	231.3	3183
27	94.5	0.4	1.2	5.8	9.3				0.0	0.0	0.0			320.3		358.1	206.4	270.9	236.9	243.4	176.5		168.8	51.8	3045
28	20.1	0.0	2.1	0.0	0.4	0.4			0.0	0.0	0.0		169.7	238.5		168.3	236.9	168.0	248.5	314.0	250.7	266.0	222.5	87.9	2605
29	5.3 160.8	9.6 168.8	7.5 10.4	1.6 11.3	1.2 9.3	0.0 5.4			0.0	0.0	0.0	6.8 4.6		122.0 122.0		200.7	245.0 270.9	267.9 258.0	313.4	355.7 288.8	297.3 236.9		207.9 14.0	137.0 4.6	2569 2562
30	7.1	0.0	0.0	0.0	2.5	7.5		0.0		0.4	0.0	35.4	72.7	137.0		191.8	245.7	245.7	200.0	284.6	244.2		62.4	0.0	2154
31																									2134
-	0.0	0.0	0.0	0.0	0.0	0.0			0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0
KWh	2336	1605	731	451	316	227	63	4	0	151	645	2635	4622	5962	6412	6817	6973	7399	8025	7385	7178	6131	4536	3279	83884

Ayun-Cl	nitral	Sep	200	7							Win	d Pow	er Ou	tput c	of Bor	nus 60	0/44	Γurbin	e (Mo	nth's	Sumn	nary)			
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	9.6	0.0	12.8	8.6	9.2	0.0	0.0	2.1	0.0	0.0	0.0	23.7	177.0	192.6	261.9	220.7	292.7	328.7	258.7	253.0	224.0	192.8	21.8	4.6	2494
2	2.5	0.0	0.0	0.4	3.7	0.8	0.4	0.0	0.0	0.0	0.0	13.6	60.8	114.8	183.8	223.2	223.2	258.7	305.1	324.8	252.2	191.8	62.7	80.8	2303
3	14.0	0.8	0.0	9.3	0.4	0.4	0.0	0.0	0.0	0.0	10.0	3.7	68.8	137.0	169.6	243.4	258.7	292.7	328.7	321.9	229.8	229.1	98.1	0.8	2417
4	0.0	0.0	0.8	0.0	0.4	0.0	0.0	0.0	0.0	0.0	44.5	78.4	129.8	145.8	249.1	309.4	317.3	326.7	323.3	244.2	191.8	229.7	91.1	23.3	2706
5	0.0	9.2	0.4	0.4	0.0	0.8	0.4	0.0	0.0	0.4	0.8	33.0	99.6	244.2	223.2	290.4	283.9	257.2	335.8	332.5	279.9	236.3	237.7	286.2	3152
6	316.9	196.3	52.6	31.6	0.0	0.4	0.0	0.0	0.0	8.0	60.5	161.5	275.9	291.1	332.5	322.8	334.7	310.4	329.8	327.7	321.9	316.9	301.0	352.2	4638
7	290.1	118.1	66.9	87.9	17.7	3.7	0.4	0.0	0.0	0.0	0.0	127.5	208.7	283.9	334.5	324.5	332.7	288.8	283.0	282.4	273.2	266.0	176.7	152.7	3919
8	80.8	95.8	73.9	0.0	0.4	0.0	2.1	0.4	0.0	9.1	11.7	41.1	7.1	0.4	0.0	0.0	0.0	0.0	0.0	7.4	0.4	0.8	3.3	0.0	335
9	0.0	0.0	0.0	8.0	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	9.9	72.7	221.0	221.0	266.0	238.5	291.1	270.9	302.6	221.7	148.0	21.8	2286
10	21.2	5.0	1.6	1.6	0.4	0.0	0.0	0.0	0.0	0.0	0.4	0.4	87.9	122.0	266.9	254.1	263.7	246.8	287.3	273.2	160.9	168.8	122.0	23.3	2307
11	17.5	12.1	5.4	0.8	0.0		0.0	0.0	0.0	0.0	0.4	4.6	48.4	184.8	231.3	301.0	296.1	249.4	352.1	344.3	249.9	177.0	41.9	0.0	2517
12	2.5	1.6	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	84.1	144.8	153.6	234.7	328.1	282.9	348.6	332.5	299.0	220.4	10.3	0.0	2443
13	0.0	2.1	12.7	2.9	1.2	0.0	0.0	0.0	0.0	0.0	0.4	5.8	49.3	145.8	252.2	283.0	344.5	308.4	294.4	299.0	315.4	277.4	259.5	200.9	3055
14	53.6	0.0	0.0	4.6	7.4		0.4	0.0	0.0	0.0	0.0	98.7	223.2		297.6		278.2	324.8	329.8	334.7		237.7	207.9	213.6	3450
15	39.6	17.3	21.2	4.6	0.8		0.0	0.0	0.0	0.0	0.0	49.1	200.0		293.8			319.9	329.8	278.8		288.8		152.7	3321
16	63.5	5.0	5.4	1.2	0.4		0.0	0.0	0.0	0.0	0.8							287.3	301.8					71.4	2764
17	0.4	0.0	10.0	0.0	0.0		0.0	0.0	0.0	0.0	3.7	107.7	284.6					247.6	318.2	312.0		245.7	192.6	19.2	3148
18	1.2	0.0	0.0	0.0	0.0			0.0	0.8	4.2	0.4	0.0	0.0		216.8				4.9	6.1	0.0	0.0	0.0	0.0	403
19	2.5	2.9	0.4	1.2	8.0	0.4		0.0	0.0	0.0	0.0		207.9		284.5					211.0		51.3		39.8	2620
20	21.6	0.0	1.6	0.0	0.8		0.0	0.0	0.0	0.0	0.8				252.2			287.6	345.5	276.2	41.7	16.0		18.3	2480
21 22	5.0	12.1	2.3	0.0	0.4		0.0	0.0	0.0	0.0	0.0		221.7		231.8			321.9		80.1	48.6	0.4		0.0	1989
23	0.0	0.0	0.0	0.0	0.0		0.0	173.8	79.8	29.2	92.7	164.2	215.2		252.2				221.0	273.2		238.5		78.2	3328
24	92.0	20.7	0.0	0.0	0.0		0.0	0.0	0.0	0.0	1.2									300.8		215.2		0.4	2110
25	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.8	13.8		144.8			88.7	138.8	260.2		19.4		12.1	1178
26	2.3	1.2	0.4	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0			152.7							35.4		19.4	1400
27	11.0	1.6	0.4	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.4	114.1	146.7	132.0					98.2	7.4	0.8		13.0	989
28	13.8	3.3 1.2	30.7	9.3	5.8 0.0	0.4	0.0 4.9	0.0 5.7	0.0	0.0	193.7		260.7	216.0	153.2			47.9 27.4	26.8	7.1 23.7	0.0 1.2	0.0 1.2		9.3	1737 770
29			0.0	0.0			0.0		170.4		0.0	0.0		0.0 137.7	40.9		170.9		24.0 185.6						1226
30	0.0 16.2	0.0	0.0	7.5	0.0 2.0		0.0	0.0	0.0	0.0	0.8	8.7 0.0	145.6 27.1	95.1	86.6 59.4	66.3 52.6		280.1 5.7	7.1	23.5 30.2	0.0 25.6	0.0 12.7	0.4 18.3	36.9 2.5	401
KWh		507				9.0																			
LZAAII	1078	507	301	173	52	9	9	182	251	44	423	1512	3827	5078	6163	6531	6859	6526	7120	6647	5477	4405	2880	1833	67886

Ayun-Ch	itral	Oc	t 200)7							Win	d Po	wer O	utput	of Bor	านร 60	0/44 1	urbin	e (Mor	nth's S	umma	ary)			
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.8	0.4	0.0	0.0	0.0	40.2	145.0	141.0	207.3	275.9	149.7	17.9	0.8	2.9	4.6	6.8	0.4	995
2	0.0	0.0	0.0	0.8	0.0	0.4	0.0	0.0	0.4	0.0	0.0	23.5	71.0	13.5	5.7	110.8	86.3	129.3	31.0	9.2	0.4	10.3	7.5	3.3	503
3	0.0	0.8	0.0	0.0	0.4	0.0	0.0	0.0	0.8	0.0	0.4	24.5	106.2	144.5	243.4	295.3	332.9	133.0	11.0	0.0	0.0	0.8	35.2	14.5	1344
4	0.0	0.0	0.4	0.0	0.0	0.8	0.4	0.4	0.0	0.0	0.0	0.0	1.6	9.6	140.8	208.1	283.9	266.0	171.0	32.0	60.8	10.0	0.0	0.8	1186
5	5.0	0.8	0.0	0.0	0.0	0.0	0.0	0.8	0.4	0.0	0.0	0.8	3.7	58.6	51.7	134.9	192.2	160.8	50.7	16.6	13.7	30.2	7.1	52.6	781
6	77.4	29.0	0.4	0.0	0.0	0.0	7.1	40.0	64.3	224.0	115.6	59.8	10.4	22.8	66.5	143.6	22.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	883
7	0.0	0.4	0.8	0.0	0.0	0.0	0.4	1.2	0.0	0.0	0.0	0.0	0.0	3.3	20.0	27.5	33.4	76.1	24.1	21.2	12.7	5.4	2.0	0.4	229
8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	24.1	36.9	60.8	66.6	39.8	3.3	12.0	24.5	2.1	7.8	9.3	288
9	3.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	43.7	99.8	102.9	68.9	24.5	0.0	4.6	16.6	13.2	11.0	3.7	393
10	3.3	0.0	0.0	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5.3	17.9	99.8	85.6	71.3	65.1	1.6	0.0	6.8	4.6	12.1	7.5	382
11	0.8	0.0	0.0	0.0	0.0	0.0	0.0	1.6	4.6	0.0	0.0	0.0	11.6	102.9	67.9	83.2	35.5	2.0	0.8	2.9	33.6	18.3	14.9	5.8	386
12	0.8	0.0	0.0	0.0	0.0	0.8	8.0	0.0	1.2	0.0	0.0	0.0	0.0	42.3	47.9	58.0	0.8	2.9	8.2	27.0	13.8	26.8	18.3	7.1	257
13	7.5	1.2	0.0	0.4	1.6	0.8	0.4	0.8	0.8	0.0	0.0	0.0	0.0	0.0	23.7	76.1	64.5	9.2	12.7	7.1	10.3	22.2	19.4	0.8	259
14	0.4	0.8	0.0	5.0	0.8	1.6	1.6	1.2	1.2	0.0	0.0	0.0	4.1	48.8	207.3	216.4	184.9	312.8	94.2	10.8	4.6	9.3	5.0	1.6	1112
15	0.8	0.0	0.0	0.8	0.0	0.0	2.0	0.4	0.8	0.0	0.0	0.0	5.4	31.0	122.0	77.4	122.7	51.3	57.4	74.4	29.0	3.3	18.3	15.5	612
16	5.8	0.0	2.1	0.0	1.2	2.0	8.0	0.8	1.2	0.0	0.0	3.3	24.0	54.7	85.6	176.7	122.7	228.0	331.6	309.8	137.9	62.1	15.5	15.5	1581
17	7.8	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	13.1	137.7	160.6	160.6	176.9	246.2	328.9	256.3	152.7	168.8	95.6	11.3	1917
18	24.5	7.1	0.8	0.4	0.0	0.0	0.4	0.4	0.0	0.0	0.0	0.0	0.0	14.5	55.0	138.6	236.9	307.5	266.0	87.2	7.8	16.6	24.0	3.3	1191
19	0.0	0.0	0.0	0.8	0.8	2.0	0.0	0.0	0.0	0.0	0.0	0.0	9.6	0.8	26.0	106.9	168.8	192.8	259.5	273.8	339.5	243.7	68.2	12.4	1706
20	2.9	2.9	1.2	1.2	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	1.6	14.9	77.4	56.4	27.9	52.9	160.8	141.1	21.7	47.9	21.2	12.8	645
21	2.9	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	26.3	80.8	59.4	64.3	229.1	199.9	169.8	31.3	5.3	27.4	897
22	16.6	3.3	4.2	0.0	0.0	0.0	0.0	3.3	2.5	0.0	0.0	0.0	0.0	89.2	200.7	49.3	18.3	33.4	82.4	98.2	33.4	2.1	9.3	8.9	655
23	3.3	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	91.5	144.8	206.5	302.6	251.5	252.2	63.9	0.4	0.0	1.2	0.8	
24	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	141.0	81.5	156.1	15.6	39.7	0.0	0.0	3.3	0.8	0.0	438
25	0.4	1.6	0.8	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.0	6.8	21.1	0.0	18.4	7.4	0.0	0.0	0.0	
26	0.0	0.0	0.4	64.0	130.5	4.6	0.0	0.0	0.0	0.0	0.0	0.0	4.6	20.1	102.9	160.6	239.2	246.3	36.9	65.5	0.8	0.0	0.0	0.0	1077
27	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	12.8	16.6	0.4	1.2	1.2	0.8	0.0	0.0	0.0	34
28	1.2	3.3	1.2	0.4	1.6	1.6	1.6	1.6	2.0	0.0	0.0	0.4	25.6	25.8	8.5	0.0	7.1	0.8	5.8	7.5	1.6	0.0	0.0	0.0	97
29	0.4	2.0	1.2	5.8	1.6	0.8	1.2	2.0	0.4	0.0	0.0	0.0	0.0	0.0	11.7	52.6	44.5	17.9	0.4	5.7	18.3	13.2	1.2	0.0	181
30	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.8	1.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4	3.7	7.1	1.2	0.0	0.0	0.0	15
31	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
KWh	166	54	13	80	139	16	17	56	83	224	116	112	338	1157	2415	3171	3426	3101	2482	1754	1123	750	408	216	21418

Ayun-Chitral November 2007 Wind Power Output of Bonus 600/44 Turbine (Month's Summary)

		14070			-									 	Juipui					(<u> </u>		
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	1.6	2.3	1.6	1.2	3.3	2.3	0.0	2.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.4	3.7	3.3	0.8	0.4	1.2	0.4	25
2	1.6	0.8	1.2	2.3	2.3	0.4	0.8	1.6	1.6	0.0	0.0	0.0	0.0	0.0	0.0	5.0	0.0	0.0	0.4	0.4	0.4	0.0	0.0	0.0	19
3	0.8	2.3	0.0	0.4	2.9	1.2	1.2	1.6	2.9	2.1	0.0	0.0	0.0	6.8	39.8	5.0	51.1	58.4	3.3	0.8	0.0	0.0	0.0	0.0	180
4	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.4	0.4	0.0	0.0	0.0	0.0	0.4	0.8	60.4	14.0	0.0	0.4	1.2	0.4	0.0	0.0	79
5	0.0	0.0	0.0	0.0	0.4	0.8	0.8	1.2	1.2	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.4	9.3	7.1	3.7	0.8	0.0	0.4	0.4	27
6	0.8	0.8	1.6	0.4	1.6	1.6	3.3	0.0	0.8	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.0	11
7	0.0	0.0	2.1	1.2	0.0	0.0	2.5	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	7
8	0.0	0.8	4.2	0.8	0.0	0.4	0.0	0.4	4.2	0.4	0.0	0.0	0.0	0.0	0.0	0.0	84.5	103.7	199.4	64.5	2.9	5.8	3.7	4.2	480
9	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.4	0.0	0.4	0.0	2.3	3.7	0.4	28.3	221.8	278.5	308.4	315.4	302.6	192.6	168.7	103.7	10.3	1938
10	0.4	0.8	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	49.1	107.7	184.6	91.1	185.7	261.5	133.9	40.0	0.4	0.0	9.3	4.1	1070
11	4.1	2.5	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.0	0.0	0.0	0.0	0.0	16.6	28.8	0.8	0.0	0.0	0.0	0.4	1.2	2.1	0.0	57
12	0.0	0.0	0.0	0.0	2.1	0.0	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.9	0.0	0.0	3.7	0.8	0.0	3.7	5.4	0.4	0.0	20
13	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.8	0.0	0.0	0.0	0.0	26.9	7.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	35
14	0.0	0.0	0.0	0.0	0.4	1.2	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.4	4.2	36.4	21.2	12.8	21.8	2.5	0.0	0.0	5.4	4.6	111
15	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.2	40.3	30.2	45.9	4.6	0.0	6.1	3.7	1.2	0.4	0.0	134
16	0.0	0.0	0.0	0.0	0.4	0.8	0.4	0.4	0.4	0.0	0.0	0.0	0.4	0.0	0.0	9.6	2.9	0.0	0.8	1.2	0.0	0.0	0.0	0.4	18
17	0.8	1.2	0.4	0.8	1.2	0.4	0.4	1.2	0.4	0.0	0.0	0.0	0.0	0.0	0.0	1.6	2.9	0.0	0.0	0.0	0.0	0.0	0.0	0.4	11
18	4.2	1.6	1.2	0.0	0.8	0.8	2.5	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	11
19	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4	2.5	0.8	0.0	0.0	0.0	4
20	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.4	1.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.8	3
21	3.3	2.9	3.3	0.8	3.3	0.8	0.0	0.8	0.4	0.0	0.0	0.0	0.0	0.0	0.0	7.1	8.5	0.8	1.6	0.0	0.0	0.0	0.0	0.8	34
22	0.4	0.8	0.4	1.2	1.2	0.4	0.8	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.8	0.0	0.4	0.0	0.4	0.0	0.8	0.8	9
23	0.8	1.6	0.0	0.8	0.0	0.8	0.4	1.2	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	7
24	0.0	0.0	0.0	0.0	5.3	0.4	2.5	0.4	0.4	0.4	0.0	0.0	0.4	0.0	0.8	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	11
25	0.0	0.0	0.4	0.0	0.0	0.8	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.8	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.6	4
26	0.8	0.8	0.0	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3
27	0.0	0.0	0.4	0.0	0.0	0.4	0.0	2.1	0.0	0.8	0.0	0.0	0.0	0.0	1.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5
28	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
29	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1
30	0.0	0.0	0.0	0.0	0.4	13.0	4.2	0.4	5.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	7.5	5.0	0.0	0.0	0.4	0.0	0.0	36
KWh	20	19	17	11	26	27	22	16	19	7	0	2	54	117	348	446	744	785	694	428	208	183	127	29	4349

Wind Power Output of Bonus 600/44 Turbine (Month's Summary) Ayun-Chitral December 2007 Dt./Hrs 6 8 9 12 20 24 Hrs 15 16 19 21 22 23 1 0.0 0.0 5.4 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.8 0.0 0.8 1.2 0.0 2.0 12.1 10.0 7.5 0.0 0.0 2 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 8.2 54.7 36.4 11.7 0.0 0.0 0.0 111 3 0.0 0.0 0.0 0.4 0.0 0.4 0.0 0.0 0.0 0.0 2.5 5.4 4.2 0.0 0.0 0.0 16 0.0 4 2.0 2.5 1.2 2.5 1.2 0.4 1.6 0.4 0.8 1.2 0.0 0.0 0.0 0.0 0.0 0.0 2.9 0.0 0.0 0.0 0.8 5 1.2 2.1 0.0 0.0 0.0 0.0 0.0 0.8 0.4 1.2 0.8 1.2 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 6 0.4 0.0 2.9 0.4 0.0 0.0 0.0 0.0 0.0 0.0 9.3 0.4 0.0 0.0 0.0 0.0 0.0 0.0 15 0.0 1.2 0.0 0.0 0.0 0.4 7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 2.5 13.7 4.6 0.4 0.0 372 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 180.6 138.8 31.0 8 0.0 0.0 0.0 0.4 0.0 0.0 6.8 0.8 0.4 0.0 0.0 0.0 0.0 16.9 6.9 0.4 2.9 2.9 7.5 9.3 0.0 0.0 0.4 0.0 55 9 0.0 0.0 0.0 0.0 0.0 0.0 0.0 24.0 39.8 0.0 0.0 0.0 0.0 0.0 0.0 13.1 0.8 22.6 2.1 121 0.0 0.0 0.0 15.5 2.9 10 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 105.3 266.0 26.8 0.4 0.0 0.4 598 0.8 0.0 0.0 14.8 31.8 30.7 0.0 121.3 11 0.0 0.0 0.0 0.0 0.4 0.0 0.4 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.4 9.3 2.1 0.8 13.7 0.4 28 0.4 0.0 12 25 8.0 0.0 0.0 0.4 0.0 0.0 0.0 0.0 0.0 1.2 1.6 5.4 2.0 1.6 0.8 9.3 0.8 0.0 0.0 0.0 0.0 0.0 0.4 1.2 13 7.8 102.9 102.7 1.6 5.8 0.8 0.0 0.0 15.5 18.3 76.1 0.0 17.5 35.8 0.0 0.0 0.0 0.0 0.0 0.0 436 12.1 30.6 0.8 14 0.8 21.2 0.0 0.0 0.0 0.0 1.6 7.5 2.5 0.0 0.0 0.0 0.0 0.4 0.0 0.0 5.0 18.3 13.8 18.3 7.5 11.0 4.1 112 15 0.0 0.0 0.4 0.0 0.0 0.4 12.1 2.5 0.8 0.4 0.0 0.4 0.0 0.4 0.0 0.0 0.0 0.0 0.0 0.8 12.7 11.0 11.0 9.3 62 16 0.0 0.0 0.4 0.0 0.0 0.4 1.2 0.0 0.8 0.4 0.0 0.0 0.0 11.0 15.5 12.1 9.3 0.8 3.3 0.4 0.0 0.0 0.0 0.8 17 0.4 0.4 0.4 0.0 0.4 0.0 0.0 0.0 0.0 2.0 0.0 1.6 10.3 9.3 4.1 0.8 1.2 33 0.4 0.4 1.2 0.0 0.0 18 1.2 0.0 0.8 0.0 7.5 40.5 0.0 0.0 0.8 0.4 0.0 1.6 0.8 0.0 0.4 0.0 0.0 7.8 0.4 12.6 43.1 0.0 0.0 0.0 118 19 0.0 0.0 0.0 0.0 0.0 0.0 0.4 0.4 0.4 0.0 27 0.0 0.0 0.0 0.0 0.0 0.0 0.4 0.0 0.4 7.1 4.6 0.0 0.0 13.0 20 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.2 0.0 0.8 0.0 62.7 71.3 110.1 38.6 5.4 0.0 5.3 49.8 68.9 414 21 55.1 7.5 17.7 13.8 2.9 13.3 41.7 8.2 2.9 4.2 5.7 41.1 35.2 99.8 78.4 39.8 0.0 0.0 0.0 0.0 0.0 0.0 481 22 0.0 0.0 0.4 0.0 1.2 0.0 0.8 0.4 0.0 0.0 0.0 0.0 0.4 7.1 0.0 0.0 0.8 0.4 0.0 0.0 0.0 12 0.4 0.0 0.0 23 0.0 0.0 0.4 0.0 0.4 0.0 0.0 0.0 8.0 0.0 8.7 36.4 33.0 22.2 16.6 7.5 5.4 0.4 0.0 0.0 0.4 0.8 0.0 0.0 133 24 0.0 0.0 0.0 0.4 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.4 0.4 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.6

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70

0.0

1.2

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0.0

2.3

0.4

0.0

223

5.4

3.3

7.1

0.0

1.2

3.7

0.0

418

15.5

15.5

12.7

0.0

1.2

11.0

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795

11.0

18.3

15.5

0.0

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509

7.1

11.0

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186

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52

2.5 1.6

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198

0.0

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1.2

0.0

0.0

0.0

124

5.8 5.4

11.0 3.7

11.0 7.1

0.0 0.0

4.6 0.0

3.7 1.2

0.0

116

4.1

1.6

1.2

0.4

0.0

0.4

0.0

128

1.6

1.2

0.4

0.4

0.0

0.0

0.0

75

29

3611

25

26

27

28

29

30

31

KWh

0.0

3.3

0.4

0.0

0.0

0.8

8.0

73

0.0

2.0

0.0

8.0

0.0

5.4

123

0.0

1.2 0.4

0.0

1.6 1.2

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0.4

129

0.0

0.0

0.0

0.4

0.4

34

0.0

2.3

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20

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0.0

0.0 1.2 0.4 0.4

2.9 7.1

0.4 1.2 0.0 0.0

1.2 0.8 0.4 1.2

1.2 0.8 0.8 2.9

0.0 0.0 0.4 0.0

Ayun-Chitral January 2008 Wind Power Output of Bonus 600/44 Turbine (Month's Summary)

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Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	0.0	0.0	0.0	0.4	0.0	0.0	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.9	5.4	12.7	7.5	3.3	0.8	0.4	0.0	34
2	0.4	0.0	0.8	0.8	1.2	0.0	0.8	0.8	1.2	1.2	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	7
3	0.4	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.1	0.0	0.0	0.0	0.0	4
4	0.0	3.7	19.0	0.0	1.2	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	19.5	91.1	87.9	52.9	4.6	0.0	0.0	0.0	0.0	0.0	280
5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.8	3.7	0.0	2.9	3.3	0.0	0.0	0.0	0.0	0.0	11
6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
8	0.0	0.0	0.0	0.0	0.0	0.8	0.0	0.0	2.5	0.4	11.2	31.1	20.7	2.9	2.9	0.0	0.0	0.0	0.0	0.0	5.3	97.5	41.1	156.9	373
9	146.6	0.0	15.2	0.0	0.4	0.0	0.0	14.5	0.8	0.0	0.0	0.0	0.0	8.3	22.4	38.8	152.9	20.2	0.0	0.0	0.0	0.4	0.0	0.0	420
10	0.0	0.0	0.0	0.0	0.0	0.0	173.8	305.2	283.9	165.1	80.8	38.3	3.3	3.7	0.4	53.2	59.4	36.4	52.6	51.3	51.3	60.8	85.6	27.6	1533
11	1.6	0.0	0.0	0.0	0.4	1.2	0.4	6.8	0.8	0.8	0.0	0.0	0.0	0.4	0.0	1.2	0.8	0.0	0.4	1.2	2.3	2.0	3.7	7.5	31
12	5.8	3.7	2.0	1.2	0.0	1.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	8.7	36.4	9.3	1.2	0.4	1.6	2.0	1.6	2.0	1.2	2.0	80
13	0.0	0.0	0.4	0.4	1.2	0.8	0.4	0.4	1.2	0.8	0.4	0.4	0.8	0.8	1.2	0.4	0.0	0.0	0.0	0.0	0.8	0.4	0.0	0.8	11
14	1.6	0.8	0.4	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	3.3	1.2	0.8	2.9	0.0	0.0	0.0	0.4	0.4	1.6	1.6	0.4	16
15	0.8	2.9	0.0	0.8	0.4	0.0	0.4	0.4	1.2	1.6	0.4	7.1	11.0	6.4	0.0	0.0	0.0	0.0	0.4	0.4	0.0	1.6	3.7	0.0	39
16	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
17	0.4	8.3	145.8	63.4	17.4	0.0	0.0	0.4	2.5	1.6	61.3	107.7	106.9	95.1	82.9	114.8	87.9	133.1	123.3	11.3	20.7	0.4	0.0	0.0	1185
18	2.5	0.4	0.8	0.0	0.0	2.5	0.0	0.0	0.0	0.0	0.4	10.3	12.1	43.1	60.8	35.5	49.3	7.4	0.4	1.6	0.0	0.4	0.0	2.1	230
19	15.5	3.3	1.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.8	0.0	0.4	1.2	0.0	2.0	0.4	18.6	0.0	0.0	0.0	0.0	0.4	44
20	2.9	1.2	0.4	7.1	12.7	18.3	15.5	7.5	7.5	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.4	11.7	18.3	16.6	15.5	15.5	9.3	12.1	173
21	11.0	24.0	29.6	26.8	18.3	19.4	15.5	12.7	5.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.8	11.0	11.0	11.0	7.1	3.3	207
22	5.4	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	1.6	0.4	0.4	0.0	0.0	0.0	1.2	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	10
23	2.3	7.5	2.3	0.8	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	2.3	13.4	0.4	5.8	12.7	11.0	12.1	11.0	82
24	4.1	7.5	7.5	3.3	0.8	0.4	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.0	7.1	9.3	5.8	9.3	57
25	5.8	1.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	12.4	39.8	43.1	27.4	0.4	0.0	0.0	0.0	130
26	1.2	2.3	7.5	2.0	1.6	1.2	1.2	0.8	0.8	0.0	0.4	0.0	4.9	44.5	43.1	33.6	8.9	1.6	5.8	11.0	13.8	11.0	4.1	12.7	214
27	7.5	18.3	12.7	15.5	13.8	12.7	13.8	7.5	3.7	0.0	0.0	0.4	0.0	0.0	0.0	11.7	2.9	0.0	1.6	1.6	0.4	0.0	0.4	0.4	125
28	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.8	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.8	1.2	4
29	0.0	0.0	0.0	7.5	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.4	37.2	35.5	60.8	32.4	5.8	8.2	1.6	5.8	9.3	15.5	6.8	0.4	227
30	0.0	0.0	0.4	0.0	0.8	2.9	4.1	5.8	0.0	0.0	0.0	31.8	81.6	129.8	38.9	43.1	46.5	2.9	1.2	5.8	15.5	0.8	13.8	11.0	437
31	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
KWh	216	85	246	130	70	62	227	365	312	173	156	230	282	381	372	473	524	337	291	165	171	242	197	259	5964

Ayun-Ch	itral	Fe	b 200	8							Wir	nd Pov	wer O	utput	of Bo	nus 6	00/44	Turbir	ne (Mo	onth's	Sumn	nary)			
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	0.4	0.8	0.8	0.0	1.6	0.8	1.2	3.3	1.6	0.8	0.0	0.0	0.0	0.8	4.9	2.5	0.0	5.8	9.3	11.0	9.3	0.4	0.8	1.6	57
2	0.0	0.8	0.0	0.8	0.4	1.2	0.4	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4
3	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5.0	30.7	51.3	23.5	2.9	0.0	0.0	0.0	0.0	0.0	114
4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.3	0.4	0.8	5.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	10
5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.8	0.0	0.0	0.0	1.2	2.3	4.1	8
6	2.0	1.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3
7	0.0	0.4	0.0	0.0	0.4	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.8	0.0	0.0	0.0	0.0	2
8	0.8	0.0	0.0	0.0	0.0	4.6	0.0	0.4	11.3	11.3	20.7	64.2	67.9	145.8	168.7	137.0	59.4	6.4	0.0	0.0	0.0	0.0	0.0	0.0	698
9	0.0	0.0	0.0	5.8	3.7	1.6	2.0	4.1	2.9	1.2	0.4	0.0	0.0	0.0	0.0	0.0	9.6	4.6	0.0	2.5	2.0	1.6	8.9	1.6	52
10	3.7	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.8	0.4	108.9	176.7	85.6	76.1	54.7	18.9	3.3	4.1	12.7	12.7	11.0	5.4	575
11	3.7	3.3	4.1	7.5	5.4	5.8	9.3	3.7	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.8	5.4	2.9	15.5	2.3	5.8	2.3	78
12	3.3	1.2	1.2	3.3	2.3	4.1	1.6	0.8	5.0	0.4	0.0	0.4	28.9	118.0	66.6	39.8	12.1	0.8	7.5	12.7	13.8	7.5	12.8	11.0	355
13	3.7	10.6	16.6	7.1	24.0	13.8	15.5	5.8	1.2	0.0	0.0	0.0	0.8	1.6	0.0	2.5	2.1	0.0	3.7	12.1	7.1	4.1	3.7	0.4	136
14	0.4	0.0	1.2	0.4	0.0	0.4	0.0	1.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4	13.9	36.4	140.8	49.9	23.9	10.3	0.0	0.0	279
15	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	2.1	0.0	0.0	5.0	0.8	0.0	0.0	0.0	0.0	0.0	0.0	8
16	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.4	1.2	2.0	5.0	0.8	0.4	1.6	0.0	10.4	32.7	0.4	1.6	0.0	0.0	57
17	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.8	0.0	0.0	11.7	11.0	15.5	7.5	12.7	2.5	1.6	63
18	9.6	0.4	4.2	21.2	15.5	30.2	18.3	18.3	19.4	35.5	100.3	85.6	95.8	51.6	102.9	64.5	79.8	68.9	9.6	0.0	11.7	8.9	2.1	0.8	855
19	1.6	4.6	0.4	15.5	16.6	21.2	20.0	0.8	0.0	0.0	5.0	153.6	176.1	216.0	224.0	129.1	99.8	64.2	36.9	13.8	9.3	7.1	2.3	21.2	1239
20	17.3	11.0	9.3	5.4	2.9	0.4	1.6	1.6	1.6	0.8	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.4	7.1	11.0	3.3	8.2	1.2	0.4	84
21	2.1	2.1	14.4	3.3	0.4	0.0	0.0	0.0	0.0	0.4	10.8	206.6	257.2	314.0	294.1	331.8	308.9	345.7	287.3	227.5	108.4	102.9	115.7	118.0	3052
22	81.7	43.1	45.3	0.4	7.8	14.5	13.7	29.0	35.8	6.4	2.9	87.9	245.4	98.2	180.7	172.2	93.4	65.5	52.6	4.2	0.0	0.0	0.0	0.0	1281
23	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.4	1.6	1.6	3.3	9.3	11.7	0.4	4.1	18.3	21.2	18.3	21.2	11.0	123
24	8.5	2.9	0.0	0.0	0.0	0.8	0.0	0.0	0.0	0.0	0.0	10.4	49.8	0.4	0.4	11.0	9.3	1.2	19.4	7.5	11.0	4.1	7.5	2.0	146
25	2.3	3.3	2.5	3.3	1.6	3.3	0.8	0.4	0.0	0.0	0.4	22.7	200.0	176.7	92.7	92.7	71.3	33.6	7.5	6.8	0.4	0.0	35.0	85.6	843
26	40.5	2.5	2.0	12.7	11.0	27.4	24.0	19.0	5.0	57.9	145.8	184.8	216.0	231.3	266.0	302.6	248.4	176.7	51.2	6.8	11.7	9.6	13.8	14.9	2081
27	8.9	13.8	24.0	21.2	13.8	25.6	30.2	24.5	16.6	36.1	30.2	66.2	102.9	68.9	85.6	95.1	42.0	2.9	11.0	9.3	9.3	5.4	4.1	2.0	749
28	0.4	5.4	7.1	7.5	5.0	4.1	0.8	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.6	7.5	24.0	18.3	12.7	5.8	5.0	107
KWh	191	108	133	115	112	160	140	113	102	151	321	885	1554	1614	1582	1497	1174	871	689	473	297	232	256	288	13060

Ayun-Ch		Marc	1									1		r Outp			1			1					
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	24.5	1.2	6.5	5.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	19.5	41.1	30.7	0.4	3.7	7.5	10.3	16.6	7.5	2.0	177
2	1.2	7.1	0.4	1.6	0.8	0.0	0.0	0.0	2.1	7.8	39.8	118.0	176.7	192.6	98.5	20.0	1.2	0.4	0.0	2.9	1.2	9.3	1.2	1.2	684
3	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.0	149.2	277.2	153.2	209.5	350.5	216.5	80.8	67.1	3.3	0.0	11.3	1520
4	0.0	0.4	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.6	20.5	208.1	215.2	192.6	207.3	129.1	63.2	39.8	7.1	11.0	7.5	3.3	1107
5	1.2	0.0	0.0	0.0	0.4	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	116.5	329.8	248.4	98.1	1.2	83.2	62.1	2.0	0.8	0.0	0.4	944
6	4.9	61.7	0.0	0.0	0.0	0.0	0.4	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.8	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	70
7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.8	1.6	15.4	64.2	46.0	9.3	36.9	57.4	7.5	9.2	5.0	0.0	0.0	0.0	2.1	255
8	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.8	0.8	5.0	11.0	15.5	12.7	11.0	7.1	64
9	2.9	0.0	0.0	0.0	0.0	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.6	7.5	7.5	12.1	7.8	5.0	45
10	2.5	0.0	0.0	0.0	0.0	0.0	0.4	0.8	0.0	0.0	0.0	0.0	0.0	0.8	3.3	60.0	150.6	7.1	1.6	10.6	9.3	9.3	5.8	5.8	268
11	7.5	1.2	0.4	0.0	0.0	0.0	0.4	0.4	0.4	0.0	0.0	0.0	0.4	5.4	0.0	0.0	0.0	0.4	2.5	9.3	11.0	21.2	12.7	6.8	80
12	1.2	3.3	2.0	1.2	2.0	1.6	1.6	1.6	1.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	7.8	11.0	9.3	15.5	18.3	11.0	88
13	9.3	0.4	1.2	1.2	0.8	1.2	1.2	2.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	12.8	46.5	20.7	0.8	2.3	5.0	5.8	0.4	0.8	112
14	0.0	0.0	5.0	9.3	12.7	9.3	1.6	3.3	0.0	0.0	0.0	8.3	0.8	0.0	0.0	30.2	68.9	43.7	8.2	9.3	12.7	9.3	12.7	4.1	249
15	5.0	5.8	0.8	0.4	0.4	0.8	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	10.8	95.8	106.9	95.1	24.7	25.0	176.6	295.3	10.0	2.9	857
16	46.7	7.8	14.1	12.4	0.0	0.0	0.0	0.0	0.0	0.4	5.8	2.0	27.9	98.9	92.4	33.6	33.6	1.6	1.2	17.9	281.1	269.4	46.4	61.7	1055
	317.5	151.5	51.3	38.9	12.0	0.4	0.0	0.0	0.0	0.4	11.7	1.2	30.1	122.9	275.0	138.0	60.8	19.4	2.0	0.4	0.4	0.0	0.0	0.4	1234
18	0.0	0.0	0.0	0.0	0.0	0.0	0.4	1.2	1.2	0.0	1.2	0.4	0.0	0.4	0.4	14.5	10.3	3.3	0.0	1.6	5.4	7.5	7.5	7.5	63
19	7.5	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4	2.9	0.8	0.0	0.0	0.0	19.0	1.2	0.0	3.3	4.1	3.7	9.3	12.1	65
20	7.5	2.9	0.4	1.2	0.0	0.4	0.0	0.8	0.0	0.0	0.0	0.0	0.0	13.3	68.9	83.2	122.2	254.2	258.7	114.1	9.6	11.7	13.8	4.1	967
21	3.3	5.4	6.8	3.7	38.3	10.0	2.5	0.4	0.4	0.0	0.0	18.0	68.9	122.7	114.1	122.0	114.8	137.0	95.8	33.8	4.1	7.1	1.6	1.6	912
22	1.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.1	34.1	46.5	47.9	13.0	7.5	7.8	18.3	18.3	7.5	205
23	4.1	7.5	2.0	0.4	0.4	0.4	0.4	0.0	0.0	0.0	0.0	0.0	60.6	35.5	34.3	7.8	0.0	1.2	5.0	7.5	13.8	9.3	5.8	4.6	201
24	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4	6.5	18.5	0.4	0.0	0.0	41.7	47.9	24.0	0.8	5.8	15.5	12.7	7.5	5.4	187
25	5.8	0.8	0.0	0.4	0.0	0.4	1.2	1.2	0.0	0.0	0.0	0.0	0.0	17.0	54.7	51.3	121.1	102.9	165.0	215.2	309.1	310.4	68.8	6.8	1432
26	0.0	0.0	0.0	0.0	0.0	0.8	8.0	0.0	0.0	0.0	2.9	48.8	279.4	56.6	12.1	7.1	0.4	0.0	0.0	0.0	0.0	0.8	0.0	0.4	410
27	0.0	0.8	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	16.6	28.6	25.6	0.0	0.8	0.8	2.3	7.5	3.7	1.2	88
28	0.4	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.0	8.7	95.1	60.8	57.4	47.9	40.2	54.7	92.7	122.0	76.1	51.3	64.2	87.9	80.8	940
29	61.8	31.8	43.7	34.9	2.9	0.4	0.0	1.2	0.4	2.5	0.0	0.0	0.0	0.0	0.0	12.4	49.9	39.8	0.4	6.5	11.0	5.8	2.3	2.5	310
30	0.4	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.8	2.9	10.4	138.5	129.1	33.8	45.6	112.3	39.0	90.7	1.2	38.3	13.4	3.7	660

0.0

802

865

15250

31

KWh

Ayun-Cl	nitral	Аp	ril 20	80						Wi	nd P	ower	Outp	ut of	Bonu	ıs 600	0/44 7	Γurbin	ne (M	onth'	s Sur	mmar	y)		
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	9.3	12.7	15.5	11.0	5.4	5.4	0.8	0.8	0.8	0.0	0.0	0.0	0.0	15.4	64.2	99.8	122.0	153.6	184.1	265.2	257.2	223.2	128.6	264.4	1839
2	178.8	83.8	27.5	7.1	11.7	5.8	4.1	0.8	0.0	41.5	92.7	176.9	248.2	300.5	298.0	355.7	329.8	304.0	334.5	270.7	255.6	216.0	192.6	130.5	3867
3	5.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	8.7	133.0	340.7	167.7	83.2	24.0	13.8	0.4	0.0	4.9	0.4	0.0	782
4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	11.6	10.8	61.7	114.8	161.2	175.4	194.7	176.1	253.0	102.9	47.9	59.4	56.0	33.6	13.3	1472
5	80.8	28.4	31.8	49.3	63.2	24.0	15.5	3.7	3.7	1.2	0.0	0.0	0.8	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.0	303
6	0.0	0.0	0.0	0.8	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.0	14.4	184.1	107.7	71.3	50.8	0.8	1.2	0.4	0.0	0.0	432
7	0.4	0.4	3.3	0.4	0.0	0.4	7.1	20.3	2.9	0.4	0.0	0.4	144.5	175.4	224.0	306.5	342.4	223.2	222.4	45.6	1.6	0.8	2.0	0.4	1725
8	1.2	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.6	1.6	42.0	53.2	153.5	160.8	251.5	229.7	260.1	275.1	254.2	154.8	121.1	15.5	11.7	1988
9	2.1	0.0	0.0	0.0	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	11.0	14.9	94.3	68.9	44.5	24.8	5.0	0.0	0.0	0.0	0.0	0.0	266
10	0.0	0.0	0.0	0.0	0.0	0.0	0.0	7.1	0.0	0.0	0.0	0.0	0.8	4.1	16.2	16.6	45.1	85.6	36.4	39.8	57.4	38.9	30.7	45.1	424
11	0.4	0.0	0.0	0.0	0.4	0.4	0.0	0.0	0.0	0.0	5.0	1.2	11.0	18.9	56.0	106.1	266.0	277.4	318.5	348.0	175.9	40.3	10.3	0.0	1636
12	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.4	109.7	324.9	289.4	305.2	199.9	114.8	54.7	14.4	0.8	1.2	2.3	2.5	1421
13	0.0	0.0	0.0	0.4	0.0	0.8	0.4	0.8	0.0	0.0	0.0	0.0	0.0	13.6	68.9	87.9	95.1	51.3	102.9	37.2	72.4	11.2	1.2	3.3	547
14	1.2	0.0	0.0	7.5	2.5	0.0	0.0	26.2	2.5	1.6	2.1	0.0	9.6	0.0	0.0	0.0	0.0	11.7	11.7	7.8	27.9	13.8	10.8	0.8	138
15	2.1	30.5	21.6	0.0	0.0	0.0	1.2	13.1	207.9	96.7	93.4	58.4	9.2	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.4	0.0	0.0	535
16	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.8	0.4	26.2	39.8	33.0	36.9	39.8	39.8	36.4	30.3	0.4	0.0	5.4	3.7	1.2	294
17	2.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	38.1	73.7	95.1	118.0	62.1	214.5	176.7	122.0	15.5	0.4	919
18	1.6	2.0	0.4	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	11.4	56.0	54.7	80.8	43.1	39.8	41.7	5.7	10.0	5.7	21.2	374
19	5.8	4.1	2.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.0	8.7	43.1	61.7	145.6	145.0	137.9	271.5	232.5	160.9	79.8	14.1	13.8	1328
20	3.3	5.4	0.0	0.0	0.0	0.4	0.4	0.0	0.0	0.0	0.0	0.8	0.8	4.2	46.7	59.4	73.7	64.2	52.6	190.4	317.4	190.7	63.7	39.8	1114
21	20.0	0.8	0.0	0.0	0.4	1.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.5	0.0	94.6	11.2	3.7	7.4	9.5	16.2	5.7	0.4	2.1	176
22	0.0	0.0	0.0	8.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.2	43.4	34.1	2.0	12.1	0.0	7.4	9.3	2.0	0.8	0.0	116
23	8.0	0.4	0.0	1.2	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0	0.0	0.0	26.7	60.8	200.9	106.1	40.3	14.9	17.3	18.3	16.6	9.3	514
24	2.9	1.2	0.4	8.0	0.8	0.8	0.8	0.0	0.0	5.3	59.4	51.3	14.9	2.3	0.4	0.0	0.0	4.6	6.4	18.3	3.3	0.8	5.0	16.6	196
25	8.6	3.3	7.4	0.4	0.0	0.0	0.0	0.0	0.0	0.0	36.9	9.3	0.8	0.4	0.0	9.2	32.1	53.9	34.5	23.7	2.9	2.9	8.9	2.3	237
26	0.4	0.0	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.8	6.4	21.2	30.2	11.0	5.0	0.4	1.6	11.3	14.0	34.1	11.0	1.6	8.2	3.3	161
27	3.7	14.9	30.2	13.3	16.0	12.1	2.1	3.3	61.7	160.8	183.9	270.9	152.7	41.1	38.9	19.4	21.1	7.5	27.4	25.6	21.2	22.2	0.4	0.0	1150
28	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	11.0	5.8	0.8	0.0	0.0	0.0	0.0	0.4	0.4	7.1	33.0	24.5	5.8	89
29	5.4	0.4	0.0	0.0	0.0	1.2	5.8	5.4	0.0	0.0	0.0	0.0	8.3	49.3	46.7	14.8	76.4	184.8	130.6	152.7	145.8	95.0	2.9	19.0	944
30	19.4	11.0	9.3	7.1	1.2	0.4	0.4	2.0	0.0	0.0	0.0	0.0	0.4	39.8	122.0	137.0	137.0	137.7	50.6	30.2	1.6	0.0	0.4	3.7	711
KWh	356	200	150	100	102	53	39	84	279	323	493	731	984	1559	2325	2888	2958	2776	2481	2329	1960	1317	599	610	25698