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AN INVESTIGATION OF WIND POWER POTENTIAL AT Paddar(Bagh)- AJK

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Executive Summary

Pakistan Meteorological Department (PMD) conducted a wind power potential survey of the northern areas of Pakistan. Funding for this project was provided by the Ministry of Science & Technology. Under this project wind data was collected at 42 sites in the Northern parts of the Country.

In this report the analysis based on one year wind data has been presented along with the wind generated electric power at Paddar (Bagh), AJK. Wind data with ten minute average speed and direction were collected at 10 meters and 30 meters height and 50 meters values were computed from models.

At 50 meters we have the annual average wind speed of 2.22 m/s during twelve months May-2007 to April-2008 the highest of 2.89 is observed in May 07. Seasonal Diurnal Wind variation indicates that maximum wind speed is available in the Day through-out the year. Wind frequency distribution shows that during 14.5% of the time wind speed is 5 m/s or above.

Sometimes simply wind speed averages do not give the true picture of the wind power optional of an area. For the purpose it is common to assign areas to one of the seven wind classes based on "wind power density" of the area. Monthly and annual wind power density has been computed and added in the report. The annual power density of Bagh is 26.29 w/m^2 according to international wind classification, this power density categorize Bagh as a below marginal site for wind power generation.

Wind generated electric power has as also been computed on hypothetical 600Kw wind turbine and its hourly, monthly and annual values has been added in this report. The annual power production form a single 600kw wind turbine come out to 113,467 kWh which shows the capacity factor of 2% for Bagh. Internationally it is accepted that if any site has a capacity factor of 25% and above than that site is suitable for installation of economically viable wind power farms. As such Bagh and surrounding areas can be classified as no suitable site for installing big economically viable wind farms.

1. Introduction:

Wind energy is the fastest growing renewable energy source today. A continued interest in wind energy development worldwide has produced steady improvements in technology and performance of wind power plants. New wind power projects have proven that wind energy not only is cost competitive but also offers additional benefits to the economy and the environment.

A steady supply of reasonably strong wind is necessary requirement for utilizing the power in the wind. Development of wind energy depends upon a clear understanding of wind resources. Site location, turbine performance and physical effects of turbulence and energy extraction represent a few of the issues that must be addressed by anyone interested in developing wind energy.

As such any plan to develop wind energy must begin by understanding the wind resource. Where are the best potential wind sites located? How much energy could be extracted from the wind at those sites?

1.1 **Characteristic of wind:**

The global winds are caused by pressure differential across the earth's surface. The amount of solar radiation absorbed at the earth's surface is greater at the equator than at the poles. This variation in incoming heat sets up convective cells in the lowest layer of the atmosphere. In the simplest form air rises at the equator and sinks at the poles. However the rotation of the earth complicates this simple heat transfer. A series of circulations are set up in both northern and southern hemispheres.

The areas of the globe where air is descending are zones of high pressure and where the air is ascending, low-pressure zones are formed. The pressure gradient drives the flow of air from high to low pressure, thus causing the wind. The wind is then acted on the corriolis force due to the earth's rotation. The resultant wind is turned easterly or westerly. On a smaller scale, wind is created because of temperature difference between land and sea and mountains and valleys. The local topographical features and roughness of the terrain also cause air movements.

2.0 <u>Wind Mapping Project of Pakistan Meteorological Department:</u>

As any plan to develop wind energy must begin by understanding the wind resources. Where are the best potential wind sites located? How much energy could be extracted from the wind at those sites? Will the wind turbine performance be affected by the turbulence or other wind resource characteristics?

To answer these questions and to provide wind resource database for the different potential parts of the country, Pakistan Meteorological Department prepared a phased programme. Government of Pakistan, Ministry of Science and Technology provided the necessary funding for undertaking the Phase II. Second phase covers the Northern areas of Pakistan.

2.1 Study Area:

The project area for the wind mapping Phase-II covers the Northern areas of Pakistan including Districts are Swat, Dir, Chitral, Gilgit, Skardu, Haripur, Shangla, Buneer, Nowshara, Peshawar, Mohmad Agency, Khyber Agency and Azad Kashmir.

Forty-Two stations for collecting wind data have been installed to study the wind regime as shown in Map-1. The list of stations is given below:

Fatehpur, Bahrain, Kalam, Khawazakhaila, Malamjabba, Tahash, Khungipayan, Dir, Tarbella, Nizampur, Warsak, Chitral City, Drosh, Mirkhani, Shagore, Garam Chasma, Khagozi, Reshan, Mastuj, Kalash, Ayune, Astore, Bunji, Chillas, Gilgit, Barapayan, Gupis, Sost, Passu, Aliabad. Shigar, Sermik. Lowaramaina. Ramatkore, ShahidaSir, Danakool, Bagh, **Bagh-Paddar**, Moorti Pahari, Lempiapatian, Dargaye.

Pedder (Bagh) is situated in, AJK. Latitude & Longitude of Paddar Bagh is: Latitude = 34.01°, Longitude = 73.78°, Elevation =4530 Ft.

2.2 **Data source:**

To undertake this study 30-meter high towers are erected at the locations mentioned above. On each of these high towers two wind speed anemometers are installed at the height of 10 meters and 30 meters, respectively; wind vane for recording wind direction is installed at 30 meters height. NRG automatic data loggers have been installed to record data at each site. These data loggers are recording, ten-minute average wind speed at both level, ten-minute average wind direction, and 10-minute average minimum and maximum wind speed. While selecting the above-mentioned locations for wind monitoring; the main objective was to identify potentially windy areas that also possess other desirable qualities of wind energy developed site. Further following guidelines as far as possible were also kept in mind while choosing an exact location for monitoring towers.

- Towers are placed as far as possible away from the local obstruction to the wind
- Selected location should be representative of the majority of the site.

Since sating a tower near obstructions such as trees or building can adversely affect the analysis of the site's wind characteristics such as magnitude of wind resource, wind shear and turbulence levels the tower in most cases are placed as far as possible away from local obstructions to the wind. But where this rule could not be followed, the tower was placed at horizontal distance of 10 times the height of the obstruction in the prevailing wind direction as required internationally. The following parameters have been recorded during the study.

- i. Wind speed ten minute average at 10 & 30 meters
- ii. Maximum wind speeds during 10 minutes
- iii. Minimum wind speeds during 10 minutes
- iv. Wind direction ten minutes average at 30 meters

Every month a team of observers and Maintenance Engineers visit site to inspect the instruments and to download the data on a laptop. Finally, the data is compiled and analyzed at Renewable Energy Research Cell established at Meteorological Department Islamabad.



Map-1: Shows 42-Towers Installed in Wind Mapping Project in Northern Areas

3.0 Methodology; Analysis & Discussion:

3.1 Wind speed variation with height:

Wind speed tends to increase with height in most locations, a phenomenon known as wind shear. The degree of wind shear depends mainly upon on two factors, atmospheric mixing and the roughness of the terrain.

Atmospheric mixing typically follows a daily cycle driven by solar heating. At the hub height of a wind turbine, this cycle often causes wind speeds to increase in the daytime and decrease at night. However, the range of variation between night and day typically diminishes as hub height increases. At a height of approximately 50 meters, it weakens or may even disappear in some cases.

Terrain roughness also affects wind shear by determining how much the wind is slowed near the ground. In areas with a high degree of roughness, such as forests or cities, near- surface wind speeds tend to be low and wind shear high, whereas the converse is true in areas of low roughness such as flat, open fields. Wind shear may be greatly reduced or eliminated where there is an abrupt change in terrain height such as a sea cliff or mountain ridge.

To save money wind measurements sometimes are taken at a lower height than the wind turbine tower. In that case, it is essential to measure wind shear at different times of day in different seasons to accurately predict the performance of a wind power plant. The shear can be measured by monitoring wind speeds at two or three heights on a tower. Since wind turbines produce much more power in stronger winds, wind turbine designers try to put turbines on the tallest possible towers. At some point, however, the increased cost of towers outweighs the benefits. With current wind turbine technology, the optimum tower height for large wind machines appears to be approximately 40 to 50 meters.

For saving money in this survey also the wind has been recorded at 10 & 30 meters and for calculating the wind speed at 50 meters the following two methods has been used in this study.

3.1.1 Log Law:

The turbulent mixing in the atmosphere may be considered in a similar way to molecular mixing (this is called k theory). Assuming the mixing is dominated by mechanical mixing due to shear forces a relationship of wind speed with height is derived.

$$u = \frac{u_*}{k} \ln \left(\frac{z - D}{z_o} \right)$$

Where

 U_* is the friction notify

k is the von Karman constant

 Z_0 is the roughness length

D is the displacement height

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The von Karman constant is generally taken as 0.4. The roughness length Z_o is related to the vegetation cover of the area. The values of roughness length are given in Table-1. The displacement height D is the height above the roughness elements where the flow is free. For most vegetation it is small and is generally treated as zero. For large roughness elements like trees and building in towns it is not negligible and is the order of the average height of the elements. The **log law** may only be used for heights above D. Turbines are rarely sited in forests or towns, so D is usually taken as zero.

The wind speed at any height z can then be computed provided that the wind speed at a height Z_R is known. Thus:

$$\frac{u}{u_{R}} = \frac{\ln \left(\begin{array}{c} z \\ z_{o} \end{array} \right)}{\ln \left(\begin{array}{c} z \\ z_{o} \end{array} \right)}$$
Where
U_R is the wind speed at reference height Z_R

The reference height is usually 10m or 30m as this is the height at which mean wind data is generally collected.

3.1.2 Power Law:

Engineers often prefer to use a <u>Power Law</u> to describe the increase in wind speed with height, as it is easier to evaluate.

$$\frac{U}{U_R} = \left(\frac{z - D}{z_R}\right)^{\alpha}$$
Where:
 α is the power law exponent

 α is the power law exponent U_R is the wind speed at reference height Z_R

The power law exponent typically varies between 0.1 and 0.32 depending upon the landscape type. A value of 1/7 is often quoted as a reasonable value for the power law exponent in countryside. The exponent can be calculated from the roughness length.

$$\alpha = \frac{\ln \left(\frac{\ln \left(\frac{z}{z_{o}} \right)}{\ln \left(\frac{z}{z_{o}} \right)} \right)}{\ln \left(\frac{z}{z_{R}} \right)} \approx \frac{1}{\ln \sqrt{\frac{z \cdot z_{R}}{z_{o}}}}$$
Where: Z is the measurement height
Z_{R} is the reference height
Z_{0} is the roughness length

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The power law exponent therefore varies with the interval between the two measurement heights. The power law should be carefully employed since it is not a physical representation of the surface layer and does not describe the flow nearest to the ground very well. Both the log law and the power law are simplified expressions of the <u>wind profile</u>. They are valid in flat homogeneous terrain. So they do not include the effects of topography, obstacles or changes in roughness or stability.

Table 1: Typical values of surface roughness length Z_0 and power law exponent α for various types of terrain

Type of terrain	Z ₀	α
Mud Flats, Ice	10^{-5} to 3x 10^{-5}	
Calm Sea	$2x10^{-4}$ to $3x10^{-4}$	
Sand	$2x10^{-4}$ to 10^{-3}	0.01
Mown Grass	0.001 to 0.01	
Low Grass	0.01 to 0.04	0.13
Fallow Field	0.02 to 0.03	
High Grass	0.04 to 0.1	0.19
Forest and Woodland	0.1 to 1	
Built up area, Suburb	1 to 2	0.32
City	1 to 4	

3.2 Average Wind Speed:

By using above mentioned methods the wind speed at 50 meters has been computed and monthly average of these wind speed at 50 meters height have been given in Fig 2 in graphical as well as tabular form.

Fig-1 shows monthly average wind speed at height of 10 meters, 30 meters and 50 meters from May 2007 to April 2008. At 30 meters height, we have the maximum average wind speed of 2.11 m/s during May, 2007. At 50 meters we have the annual average wind speed of 2.22 m/s from May-2007 to April 2008 and the highest average wind speed of 2.89 m/s is observed during May 2007.



3.3 Diurnal Wind speed Variation:

Fig-2 shows the annual diurnal wind speed variations at Bagh. The wind speed is generally equal during day and night time, it reaches maximum in evening which is around 2.93 m/s and 4.13 m/s at 30 meters and 50 meters height respectively.



Fig-3, Fig-4, Fig-5 and Fig-6 shows the seasonal diurnal wind speed variations at Bagh for (Mar-May), (Jun-Aug), (Sep-Nov) and (Dec-Feb) respectively. Seasonal wind speed is generally higher during daytime and low during night in Bagh.









3.4 Wind speed Frequency Distribution:

Wind speed frequency distribution can simply be obtained by plotting the different wind speeds against their frequencies / relative frequencies. For obtaining frequency distribution the following two procedures are necessary.

3.4.1 Binning of Data:

The sorting of the data into narrow wind speed bands is called binning of the data. In our case a bin width of 1m/sec has been used e.g. a measured wind speed of 3.5 m/sec would be placed in 3 < X <= 4 m/sec bin. The central value of each bin i.e. 0.5 m/sec, 1.5 m/sec etc has been used in calculations and frequency distribution group.

3.4.2 *Relative Frequency:*

It is proportional wind speed in each bin. It can be viewed as the estimate of probability of given wind speed in the bin. Relative frequency is defined as

R.F = probability P (Vi_{j} = Frequency of given wind speed / Total period

3.4.3 Annual Cumulative Wind Frequency:

Fig-7 shows the Annual Cumulative Wind Frequency distribution at three heights 10, 30 and 50 meters. The analysis indicate that in a year at a height of 30 meters during 135 hours the wind speed is greater than equal to 5 m/s whereas at 50 meters, during one year 719 hours the wind speed is equal or greater than 5m/s.



3.4.4 Wind Frequency Distribution:

Fig-8 shows the Annual wind frequency distribution at Bagh. We can see that at 50 meters during 324 hours wind speed is 5 m/s, 185 hours speed is 6 m/s, 103 hours speed is 7 m/s, 51 hours speed is 8 m/s and during 28 hours the wind speed is 9m/s and so on. This indicates wind potential in this area.



Fig-9 gives the frequency distribution in percentage. At 50 meters we find that during 6.1% of time wind is 5m/s, 3.7% of the time 6m/s and 2.1% of the time it is 7m/s. whereas at 30 meters height we get 2.9% of the time wind speed 5m/s, 0.9% of the times 6m/s and 0.4% of the time 7m/s.



3.4.5 Seasonal Wind Frequency Distribution:

Figures 10–17 gives seasonal wind frequency distribution and percentage wind frequency distribution.

March-May

Fig-10 shows frequency distribution during the months of Mar to May. We can see that in this period at 30 meters height during 42 hours we get 5m/s, 21 hours 6m/s, 10 hours 7m/s. Similarly at 50 meters we get 116 hours 5m/s, 72 hours 6m/s, 47 hours 7m/s, 26 hours 8m/s, 16 hours 9m/s, 08 hours 10m/s.

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Similarly the above mentioned seasonal frequency distribution percentage terms have been presented in figure 11. Jun–Aug





September – November

Fig-14 and 15 shows wind frequency distribution and percentage frequency distribution during the months of September to November respectively.





<u>Dec – Feb</u>

Fig-16 shows frequency distribution during the months of December to February. We can see that in this period at 30 meters height during 10 hours we get 5m/s, 4 hours 6m/s.

Similarly at 50 meters we get 56 hours 5m/s, 23 hours 6m/s, 9 hours 7m/s, 3 hours 8m/s, 1 hours 9m/s.

Similarly the above mentioned seasonal frequency distribution percentage terms have been presented in figure 17.





3.5 Wind Rose:

Fig-18 shows the Wind Rose Graph based on 12 months data from May 2007 - April 2008 collected at 30 meters height. Wind Rose indicates that most of the time the wind direction is North-East and South . The average wind speed is 1.67 m/s and the percentage of wind speed greater than 3m/s is 13.2%.



Wind Rose at Bagh (30m height during 12 months)

Average Wind Speed	Wind greater than 3 m/s	Comments
1.67 m/s	8%	

3.6 Wind speed statistic:

3.6.1 *The statistical Mean:*

It is the average of a set of n numbers. Mathematically, we can write

$$M \ e \ a \ n \ = \ \frac{\left\lfloor \sum_{i=1}^{n} x_i \right\rfloor}{N}$$

The Mean Wind Speed V can be calculated by the formula.

$$\mathbf{V} = \sum_{i=1}^{n} \mathbf{V}_{i} \mathbf{P} (\mathbf{V}_{i})$$

Where Vi is the central wind speed of bin 1 and P(Vi) is the probability/relative frequency that the wind speed has in bin i.

3.6.2 Variance:

It is one of the several indices of variability that statistician, use to characterize the dispersion among the measures in a given set of data. Mathematically, variance is written as

Variance =
$$\sigma^2 = \sum (X_i - V)^2$$

Where V is mean of data set

In case of wind speed data, we can write it, as

$$\sigma^2 = \sum V_i^2 P(Vi) - (V)^2$$

3.6.3 Standard Deviation

It is the square root of the variance, denoted by σ

$$\sigma^{2} = (\sigma)^{\frac{1}{2}} = \sum \left(V_{i}^{2} P(V_{i}) - (V)^{2} \right)^{\frac{1}{2}}$$

3.7 Wind power density:

While investigating a wind power potential of an area, the average values of wind speed does not truly represent this potential because lot of information regarding frequency distribution of wind speed is suppressed in the process of averaging wind speed. As such the most important values for estimating the wind power potential of a given site is the value of the wind power density or the available theoretical instantaneous power from the wind. This available wind power in the wind is the flux of Kinetic Energy crossing the wind energy conversion system and its cross – sectional area.

Like water flowing in the river, wind contains energy that can be converted to electricity using wind turbines. The amount of electricity that wind turbines produce depends upon the amount of energy in the wind passing through the area swept by the wind turbines blades in a unit of time. This energy flow is referred to as the wind power density.

A key aspect of wind power density is its dependence on wind speed cubed. This means that the power contained in the wind increases very rapidly with wind speed; if the speed doubles, the power increases by a factor of eight. In practice, the relationship between the power output of a wind turbine and wind speed does not follow a cubic relationship. Below a certain minimum speed, the turbine does not have enough wind to operate, whereas above a certain speed its output levels off or begins to decline. In very high winds the turbine may even be shut down to prevent damage to it.

Wind power density also depends on air density. At higher attitudes, air density decreases and, as a result, so does the available power. This effect can reduce the power output of wind turbines on high mountains by as much as 40 percent compared to the power that could be produced at the same wind speeds at sea level. Air density depends inversely on temperature: colder temperatures are favorable for higher air densities and greater wind power production.

3.7.1 Wind power classes:

To simplify the characterization of the wind power potential, it is common to assign areas to one of seven wind classes, each representing arrange of wind power density at the special height above the ground. The standard International wind power classifications are shown in Table 2.

	Deseumee	30m I	leight	50m H	leight
Class	Potential	Wind Speed	Wind Power	Wind Speed	Wind Power
		m/s	W/m²	m/s	W/m²
1		0 - 5.1	0 - 160	0-5.6	0 - 200
2	Marginal	5.1 - 5.9	160 - 240	5.6 - 6.4	200 - 300
3	Moderate	5.9 - 6.5	240 - 320	6.4 - 7.0	300 - 400
4	Good	6.5 - 7.0	320 - 400	7.0 - 7.5	400 - 500
5	Excellent	7.0 - 7.4	400 - 480	7.5 - 8.0	500 - 600
6		7.4 - 8.2	480 - 640	8.0 - 8.8	600 - 800
7		8.2 - 11.0	640 - 1600	8.8 - 11.9	800 - 2000

Table-2:International Wind Power Classification

By and large, the areas being developed today using large wind turbine are ranked as class 5 and above. Class 4 areas are also being considered for further development as wind turbines are adopted to run more efficiently a lower wind speeds. Class1 and class2 areas are not being deemed suitable for large machines, although a smaller wind turbine may be economical in areas where the value of the energy produced is higher

3.7.2 Power of wind Energy:

A parcel of Wind possesses kinetic energy

$$E = \frac{1}{2}mV^2$$

From this, power density is calculated as

$$P = \frac{e}{t} = \frac{1}{2} \frac{dm}{dt} V^2$$

Where $\frac{dm}{dt}$ is the mass of air following time. From fluid dynamics, it can be proved that

$$\frac{dm}{dt} = \varphi A V$$

Volume of cylindrical cross section can be written as

Where r is radius of cylinder and L is length of it. The wind moving with velocity V travels this distance L in time t so

$$S = L = Vt$$
,

So equation L takes the form

$$V = \pi r^2 V t$$

Now mass of wind can be written as

$$M = \varphi A v t$$

Differentiating

$$dm/_{dt} = \varphi AV d/_{dt(t)} = \varphi AV$$

Where φ is density of wind and others parameters have been defined in diagram.



So the power is then,

$$P = \frac{1}{2} \frac{dm}{dt} V^2 = \frac{1}{2} \varphi AVT / t V^2$$
$$= \frac{1}{2} \varphi AV^3$$

And power density

$$P_A = \frac{1}{2} \varphi V^3$$

Density of wind at mean sea level is 1.225 kg/m³

At 15° C, The area depends upon the size of the rotor. Therefore, it is clear that power density chiefly depends on wind velocity and goes up as a cube of it.

3.7.3 Wind power calculation using Mean wind Speed:

Wind power calculated from Mean wind speed is not true representative of wind power. In real world, the wind varies constantly. Actual wind power density at most sites can rang from 1.0 to 3 times greater then that calculated. For example, we take wind speed of 5, 7 and 8 m/sec respectively the respective power densities are 76 wat/m², 210 watt/m² and 313 watt/m². The average of which is 200 watt/m². On the other hand, the average wind speed is 6.7 m/sec and power density of average wind is 181 watt/m². So the power of wind calculated by mean wind speed is less than the actual power present in wind i.e. Mean wind speed is not true representative for the wind power calculations.

To overcome this drawback we find some alternative arrangement, which reduces the deficit. The Weibull distribution is the best fit of wind data to calculate wind power based on mean wind speed and variance/standard deviation.

3.7.4 Weibull distribution:

The Weibull distribution (named after the Swedish physicist W. Weibull, who applied it when studying material strength in tension and fatigue in the 1930s) provides a close approximation to the probability laws of many natural phenomenons. It has been used to represent wind speed distribution for application in wind loads studies for sometime. In recent years most attention has been forced on this method for wind frequency applications not only due to its greater flexible and simplicity but also because it can give a good fit to experimental data.

The Weibull distribution function, which is a two-parameter function, has been found to fit much wind data with acceptable accuracy is expressed mathematically as

$$\phi(u) = \frac{k}{c} \left(\frac{u}{c}\right)^{k-1} \exp\left(-\left(\frac{u}{c}\right)^k\right)$$
u is the wind speed
c is the scale parameter with units of speed
k is the shape parameter and is dimensionless

When k = 2 the distribution reduces to Rayleigh distribution and if k=1 an exponential distribution is found. These are special cased of Weibull distribution.

Solving the equation, we find that the scale factor c is closely related to the mean wind speed for the site.

$$\overline{u} = c \tau \left(1 + \frac{1}{K} \right)$$

Where τ is the complete gamma function Similarly

$$\overline{u^n} = c^n \tau \left(1 + \frac{n}{k} \right)$$

And so

Where:

$$\overline{u^3} = c^3 \tau \left(1 + \frac{3}{k} \right)$$

The available power density is obtained:

$$E = \frac{1}{2}\varphi c^{3}\tau \left(1 + \frac{3}{k}\right)$$

Where

E is the power density in watts / m^2

The shape factor k is related to the variance of the wind

$$\sigma^{2} = C2\left[\left(1 + \frac{2}{k}\right) - \left(\tau\left(1 + \frac{1}{k}\right)\right)^{2}\right]$$

The two Weibull parameters k and c may be derived from site data.

A measure of the confidence of the fit of the Weibull curve to the real data is also returned. Often the Weibull curve is a good fit to the most of the data, but a poor fit to some. If the poor fit is in the low wind speed range, i.e. below cut in it may be possible to ignore the poor fit as this portion of wind does not contribute greatly to the overall power production.

The mathematical description of the wind frequency allows us to match with the turbine power curve. Thus a measure of the average total power capture in a year is achieved. Additionally the choice of turbine cut in and furling speed may be chosen to maximum the total energy capture.

3.7.5 Weibull Parameters:



Fig-19 shows the Weibull fit to the relative frequency of wind speed.

The Weibull parameters for three different heights 10 meters, 30 meters and 50 meters are given in Table-3 along with other key results of analysis. If we look at the shape parameters K and scale parameter C for 50 meters height we can find that the shape parameter K varies over a wind range from the lowest of 1.14 during June to the highest of 1.45 during the month of October with a annual value of K being 1.28.

The lowest values of the scale parameter C 1.78 is observed in January while the highest value of 3.08 is obtained in May and with an annual value of 2.38.

3.7.6 Average Wind Speed & Standard Deviation:

In Table-3 monthly average wind speed and standard deviation at three different heights are also given. The average wind speed values for 10 meters and 30 meters height have been obtained from the recorded data, whereas the values for the 50 meters height have been computed by using the power law as explained in the earlier section.

At 10 meters height the annual average wind speed is 0.65 m/s with Standard deviation of 0.42, at 30 meters this average speed is 1.6 m/s with Standard deviation of 1.2.

At 50 meters the monthly average wind speed varies from the lowest of 1.66 m/s in January to highest of 2.88 m/s during May. Whereas the average wind speed is 2.21 m/s with Standard deviation of 1.77.

3.7.7 Power Density:

The monthly power densities for three different heights 10 meters, 30 meters and 50 meters have also been given in Table-3. At 10 meters this power density varies between 0.36 W/m^2 January to 0.32 W/m^2 in December with Average of 0.51 W/m^2 .

At 30 meters height the power density varies from 4.15 W/m^2 in January to 3.92 W/m^2 in December and the average values is about 8.8 W/m^2 .

At 50 meters height the power density of Bagh varies from 10.84 W/m^2 in January to 10.21 W/m^2 in December. The average power density of the area is 26.29 W/m^2 .

		10 m			
	Avg V (m/s)	St Dev	C (m/s)	K	P/A (w/m ²)
January	0.63	0.40	0.71	1.67	0.36
February	0.74	0.55	0.82	1.39	0.77
March	0.87	0.73	0.93	1.21	1.57
April	0.67	0.46	0.74	1.50	0.49
Мау	0.77	0.63	0.82	1.23	1.04
June	0.67	0.49	0.74	1.41	0.56
July	0.55	0.28	0.62	2.03	0.19
August	0.53	0.19	0.59	3.01	0.13
September	0.56	0.28	0.64	2.16	0.20
October	0.62	0.33	0.70	1.96	0.28
November	0.60	0.31	0.68	2.04	0.25
December	0.62	0.36	0.70	1.79	0.32
Average	0.65	0.42	0.72	1.78	0.51
		30 m			
	Avg V (m/s)	St Dev	C (m/s)	к	P/A (w/m²)
Januarv	1.28	0.97	1.40	1.35	4.15
February	1.57	1.18	1.71	1.36	7.46
March	1.96	1.54	2.12	1.30	15.81
April	1.74	1.32	1.90	1.35	10.39
Mav	2.06	1.60	2.24	1.32	18.07
June	1.87	1.48	2.02	1.29	13.96
July	1.65	1.18	1.82	1.45	7.96
August	1.50	1.07	1.66	1.44	6.02
September	1.64	1.08	1.82	1.57	6.81
October	1.67	1.05	1.87	1.65	6.81
November	1.32	0.89	1.46	1.53	3.69
December	1.28	0.94	1.40	1.39	3.92
Average	1.6	1.2	1.8	1.4	8.8
		50 m			
	AvgV (m/s)	St Dev	C (m/s)	К	P/A (w/m²)
January	1.66	1.38	1.78	1.22	10.84
February	2.06	1.63	2.22	1.29	18.67
March	2.62	2.13	2.81	1.25	40.47
April	2.40	1.99	2.56	1.23	32.34
Мау	2.88	2.41	3.08	1.22	57.20
June	2.63	2.32	2.76	1.14	48.97
July	2.28	1.81	2.46	1.28	25.51
August	2.04	1.63	2.19	1.27	18.47
September	2.24	1.66	2.45	1.38	21.26
October	2.30	1.64	2.54	1.45	21.48
November	1.74	1.30	1.90	1.37	10.09
December	1.68	1.34	1.81	1.28	10.21
Average	2.21	1.77	2.38	1.28	26.29

Table-3:Monthly Average Wind, St. Deviation and Wind Power Density at Bagh

ESTIMATING WIND GENERATED ELECTRIC POWER OUTPUT

Appendix-I

Monthly Average Diurnal Variation of Wind Generated Electric Power Output.

Appendix-II

Hourly Wind Generated Electric Power Output

4.0 Estimating Wind Generated Electric Power Output

The average power output of wind energy conversion technologies (WECT) is a very important parameter since it determines the energy output over time thereby influencing the economic feasibility of a wind project. It is by far more useful than the rated power, which does not account for the variability of wind velocity thereby easily overestimating energy revenues. The average power of wind turbine, $\overline{P_{WT}}$, is the power produced at each wind speed multiplied by the fraction that wind speed is experienced, integrated over all possible wind speeds. In integral form this can be expressed as (Manwell et al., 2002; Borowy and Salameh, 1996):

$$\overline{P_{WT}} = \int_{0}^{\infty} P_{WT}(v) df(v)$$

This integral can be replaced with a summation over bins, $N_{B_{s}}$ to calculate the average wind turbine power (Manwell et al., 2002).

$$\overline{P_{WT}} = \sum_{j=1}^{N_B} \left\{ \exp\left[-\left(\frac{v_{j-1}}{c}\right)^k\right] - \exp\left[-\left(\frac{v_j}{c}\right)^k\right] \right\} P_{WT}\left(\frac{v_{j-1}+v_j}{2}\right)$$

Please note that the relative frequency, f_j/N , corresponds to the term in brackets and the power output is calculated at the midpoint between v_{i-1} and v_i .

The available power at any given wind speed v that is convertible by a turbine is defined by (Manwell et al., 2002 Johnson, 1985)

$$P_{WT}(v) = \frac{1}{2} \rho A C_p \eta v^3$$

Where η is the drive terrain efficiency (i.e. generator power/rotor power), C_p, is the machine power coefficient. In an idealized wind turbine no losses are experienced and the power coefficient, C_p, is equal to Betz' limit (i.e. C_{p,Betz} = 16/27) and η = 1. Of course, in reality both the drive terrain efficiency and the power coefficient cannot be maximized. The extent to which the power output is limited by physical laws as well as engineering inefficiency is dependent on the specific characteristics of individual wind turbine types. This aspect will be discussed further in the analysis of the case study.

WECTs have a range of different power output performance curves, which need to be recognized when estimating the potential power output. The power output performance curves are not only defined by parameters such as the power coefficient and the drive terrain efficiency but also constrained by cut-in speed, furl-out speed and rated wind speed. Where the cut-in wind seed, v_c , is the minimum wind velocity to generate power from a turbine, the rated wind speed, v_R , is the wind speed at which the 'rated power' of a WETC is achieved and generally corresponds to the point at which the conversion efficiency is near its maximum and furl-out wind speed, v_F , is the wind speed at which the turbine shuts down to prevent structural damage.

To account for the above-mentioned constraints we can formulate a novel formula for the average electrical power output of a turbine, $\overline{P_{WTA}}$:

$$\overline{P_{WTA}} = \begin{cases} \sum_{j=1}^{N_B} \left\{ \exp\left[-\left(\frac{v_{j-1}}{c}\right)^k\right] - \exp\left[-\left(\frac{v_j}{c}\right)^k\right] \right\} P_{WT}\left(\frac{v_{j-1}+v_j}{2}\right) & (v_c \le v \le v_R) \\ \\ \sum_{j=1}^{N_B} \left\{ \exp\left[-\left(\frac{v_{j-1}}{c}\right)^k\right] - \exp\left[-\left(\frac{v_j}{c}\right)^k\right] \right\} P_{WT}(v_r) & (v_R \le v \le v_F) \\ \\ 0 & (v < v_c \text{ and } v > v_F) \end{cases}$$

The energy production of the wind turbine WE(t) over time t can thus be calculated as

WE(t) =
$$\overline{P_{WTA}}t$$

Another way of stating the energy output from a wind turbine is to look at the capacity factor for the turbine in its particular location. The capacity factor CF, is the actual energy output over a given period of time, WE(t), divided by the theoretical maximum energy output (i.e. this means that the machine is constantly running at its rated output) during the selected time-span, RO(t). This can be formulated as

$$CF = \frac{WE(t)}{RO(t)}$$

Theoretically capacity factor vary from 0 to 100%. In practice they usually range from 20 to 70% and mostly be around 20-30 percent. However, the economic feasibility of a wind turbine does not of course depend on the capacity factor of a wind turbine alone but also depends on the costs of alternative power systems. Therefore, a low capacity factor does not automatically render a wind turbine project unfeasible.

In order to maximize the energy output of a given wind regime the optimum wind speed, v_{opt} , needs to be determined. The optimum wind speed indicates at what wind velocity most energy is available in a given wind regime. It is at this particular wind speed that engineers should ensure that the power coefficient is most efficient to allow for the highest energy conversion of a turbine. The optimum wind speed can be calculated as follows (Lu et al., 2002):

$$v_{opt} = c \left(\frac{k+2}{k}\right)^{\frac{1}{2}}$$

In this regard, the power density of a turbine is a good comparative indicator to show the average power output per m^2 of wind swept area, A, at a given site. This can be defined as

Power Density =
$$\frac{\overline{P_{WTA}}}{A}$$

Another important aspect of that critically determines the energy output of a turbine is elevation. In many cases the available recorded wind speed data has been measured at a lower level than the planned hub height of the wind turbine. As wind velocity increases vertically the recorded wind speed data can be adjusted using the following standard formula (Borowy and Salameh, 1996.) where v is the projected wind speed, v_i the wind speed at reference height, H the hub height of a turbine, Hi the reference height and α the power-law exponent.

$$v = v_i \left(\frac{H}{H_i}\right)^{\alpha}$$

 α is often quoted to have a value of 1/7 and is seen as a reasonable power law exponent for even and unobstructed landscapes. However, where WECT development is planned either offshore or near woodlands or close to any other non flat terrains this value can differ subsequently and a more through analysis of α is necessary. Justus as well as Counnihan offer mathematical solution for 'fitting' α to these environments (Manwell et al., 2002).

4.1 **Hypothetical Wind Generated Electric Power**:

A wind turbine is a machine for converting the kinetic energy in wind into mechanical energy. If the mechanical energy is used directly by machinery, such as a pump or grinding stones, the machine is usually called a windmill. If the mechanical energy is then converted to electricity, the machine is called a wind generator.

Hypothetical wind generated electric power output at Bagh has been estimated by using the 600KW wind turbine bonus 600/44 MK IV type. The cut in wind speed of this turbine is 3m/s and cutout wind speed is 25m/s. Rotor diameter of this turbine is 44 meters and hub height has been taken as 50 meters. The monthly and annual wind generated electric power outputs at Bagh are shown below in graphs and table-4.

	PMD (Calculator (using	g 50M)	
Month	Input W/m ²	Output W/m ²	C.F.	KWh / Month
January	11	4	1%	3,963
February	20	7	2%	7,056
March	43	15	4%	17,344
April	34	12	3%	13,318
May	60	21	5%	23,940
June	52	18	5%	19,592
July	27	9	2%	10,730
August	19	7	2%	7,463
September	22	8	2%	8,415
October	23	8	2%	8,752
November	11	3	1%	3,335
December	11	3	1%	3,607
Annual	24	9	2%	113,467

Table-4: Hypothetical wind generated electric energy output & capacityFactor for a Bonus 600/44MK IV Turbine at Bagh.

Wind Turbine spec	ification
Turbine	Bonus 600 / 44 MK IV
Power	600 KW
Cut in Wind	3 m/s
Cut out wind	25 m/s
Rotor Diameter	44 m
Hub height	50 m

Figure 20 shows the average diurnal variation of wind generated electric energy output at Bagh (May-Apr). The graph shows that the maximum power is produced at about 3 PM; of course, this is the same time when we have the maximum wind speed in 24 hours. Figure 21 & 22 shows the monthly and daily wind generated electric power output. Figure 21 depicts that at Bagh the wind have more potential in the month of May as compared to other months. Figure 23 to 34 shows the monthly average diurnal variation of wind generated electric energy output.





















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Appendix-I

Bagh

May 2007 to April 2008

Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
Мау	259	109	268	556	226	167	40	24	16	169	601	1084	1242	1219	1202	1344	1179	1034	1563	1179	453	343	259	399	14937
Jun	53	164	88	70	237	121	137	135	172	338	610	880	1114	1394	1421	1532	1584	1637	676	339	321	82	24	32	13160
Jul	87	105	74	26	175	60	35	17	85	123	383	595	728	894	831	1008	582	572	251	320	141	148	228	21	7488
Aug	146	80	34	31	25	18	29	18	26	64	290	648	548	658	855	824	522	302	65	68	91	17	118	84	5564
Sep	30	31	22	36	23	79	28	15	36	62	305	647	834	744	1015	940	325	138	177	98	48	57	63	36	5788
Oct	39	30	31	22	30	33	34	15	0	1	45	356	973	1156	983	777	219	290	422	142	34	24	22	35	5713
Nov	16	28	10	21	13	23	12	12	5	0	12	78	347	666	617	110	20	72	30	29	42	51	42	31	2287
Dec	19	16	48	43	23	9	10	10	35	40	63	97	226	494	647	440	226	162	48	20	45	29	26	11	2790
Jan	25	13	25	3	15	86	121	53	24	28	48	77	176	369	519	464	267	132	164	62	49	59	63	48	2892
Feb	32	64	33	46	41	20	23	44	73	113	148	304	633	720	878	824	536	363	221	114	61	56	30	29	5407
Mar	234	907	364	55	61	54	72	106	128	193	331	556	889	1016	1244	1394	796	903	1138	629	540	573	560	312	13054
Apr	212	134	254	222	181	47	61	37	42	84	218	489	938	1027	845	768	441	709	727	603	376	215	211	377	9214
KWH	1153	1681	1251	1130	1048	718	601	487	641	1215	3055	5811	8648	10357	11056	10424	6699	6313	5484	3604	2201	1654	1647	1415	88294
Average	3679	3679	3679	3679	3679	3679	3679	3679	3679	3679	3679	3679	3679	3679	3679	3679	3679	3679	3679	3679	3679	3679	3679	3679	



Appendix-II

Bag	h	N	l ay 20	07							Wind	d Pow	/er Oı	utput	of Bo	nus 6	600/44	l Turk	oine (l	Month	n's Su	ımma	ry)		_
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.2	0.7	27.7	48.4	13.1	74.5	59.2	13.1	11.8	0.7	1.3	0.7	4.2	0.7	260
5	1.3	0.0	0.7	0.7	1.3	0.7	0.0	0.7	0.0	0.0	0.0	0.7	0.7	21.3	5.5	10.8	2.6	0.7	4.2	14.4	5.5	0.7	0.0	0.0	72
6	2.6	0.7	2.0	0.7	4.8	0.7	0.7	0.0	0.0	0.0	1.3	23.0	25.9	12.6	27.7	25.9	27.7	4.2	5.5	14.8	2.6	0.0	0.7	0.0	184
7	0.0	0.7	0.0	0.0	0.7	1.3	0.7	0.0	0.0	0.0	23.0	44.6	37.1	66.3	67.2	77.6	38.0	7.1	0.7	6.1	0.0	8.4	1.3	1.3	382
8	1.3	37.2	10.2	8.2	12.4	13.1	0.7	0.0	0.0	7.1	21.3	27.0	33.3	40.9	43.7	35.3	12.4	0.7	1.3	23.7	89.3	2.0	3.5	2.6	427
9	1.3	15.8	3.3	0.7	0.0	1.3	0.0	0.0	0.0	6.8	40.9	60.6	50.3	45.6	83.2	138.6	43.7	24.8	23.0	20.6	8.4	4.8	1.3	0.0	575
10	0.0	0.0	0.0	0.0	0.0	2.0	0.0	0.0	0.0	0.0	4.2	18.3	40.9	6.8	2.6	20.6	222.7	364.5	367.2	68.2	30.7	1.3	0.7	0.0	1151
11	1.3	0.0	0.0	0.0	0.0	0.0	0.7	0.0	2.0	8.4	0.7	0.7	11.3	66.3	79.8	66.3	30.6	16.6	4.2	23.0	0.7	3.3	0.0	0.0	315
12	0.0	0.7	0.7	0.7	1.3	0.0	0.0	0.0	0.0	0.7	20.1	25.9	35.3	30.6	25.9	29.5	20.1	4.8	0.7	24.2	7.7	7.7	0.7	1.3	238
13	0.0	0.0	0.0	0.0	0.7	0.0	0.7	0.0	0.0	7.7	54.0	51.2	36.2	40.9	45.6	27.7	15.9	14.8	0.7	23.0	9.5	2.6	0.0	0.0	331
14	1.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.8	44.6	66.3	71.9	61.6	68.5	40.9	50.3	12.4	1.3	33.3	2.0	1.3	1.3	0.0	462
15	0.7	0.0	0.7	0.0	0.0	0.7	0.0	0.0	0.0	0.7	30.6	55.9	85.5	51.2	71.9	53.0	40.9	8.4	0.0	0.7	2.6	0.0	0.0	239.8	643
16	202.5	33.8	20.6	0.7	69.2	77.4	23.5	4.2	1.3	64.3	1.3	24.2	32.7	64.8	67.2	30.6	20.1	18.8	0.7	26.3	0.0	0.0	2.6	1.3	788
17	0.7	0.0	0.7	0.7	0.0	0.0	0.0	0.0	1.3	37.1	66.3	55.0	60.6	50.3	77.6	55.9	42.7	24.2	4.2	37.1	13.7	0.7	0.0	0.0	528
18	0.0	2.0	0.0	2.0	0.0	0.0	0.0	0.0	0.0	0.0	28.8	60.6	30.6	41.9	29.5	37.1	60.6	55.9	371.9	109.1	16.6	1.3	9.7	8.9	866
19	16.4	2.0	15.9	11.9	3.5	0.7	0.0	0.0	0.0	0.0	2.6	15.4	15.4	29.5	5.5	17.7	6.1	0.0	4.2	23.0	3.3	0.0	0.7	0.0	174
20	0.7	0.7	0.0	66.1	66.3	35.1	2.0	8.9	0.0	14.1	4.2	17.2	27.7	39.9	24.2	24.7	7.1	14.8	267.3	256.5	170.3	171.6	215.1	68.2	1502
21	3.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.8	15.4	20.1	42.7	47.7	142.2	38.0	98.6	17.4	0.0	25.6	20.9	1.3	9.5	488
22	9.5	0.0	0.7	112.9	17.7	3.5	0.0	0.0	1.3	3.5	166.0	281.1	184.7	27.7	106.7	52.5	72.3	56.3	13.1	0.0	4.8	67.5	0.7	0.7	1183
23	1.3	0.0	0.0	0.7	2.6	0.7	0.7	3.5	1.3	0.0	16.6	32.4	61.9	38.5	11.3	56.4	107.0	64.8	27.7	14.8	0.7	4.2	0.7	1.3	449
24	0.0	1.3	1.3	0.0	0.0	0.0	0.0	0.0	0.0	11.8	23.0	5.5	90.0	48.7	2.0	0.0	0.0	107.0	269.2	267.7	41.1	36.0	10.6	59.2	974
25	10.2	10.6	93.8	345.5	45.5	23.5	10.2	7.1	8.4	0.7	4.8	1.3	5.5	0.7	29.5	52.4	68.5	19.5	2.0	0.0	4.2	0.7	0.0	0.0	744
26	0.7	0.0	117.5	4.8	0.0	4.2	0.0	0.0	0.0	0.0	7.1	23.0	121.1	37.1	4.8	0.0	11.3	20.6	23.0	14.4	0.7	0.0	2.6	0.0	393
27	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	93.4	23.5	0.0	0.0	0.0	3.5	60.6	110.9	116.9	0.7	0.0	0.0	0.0	410
28	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	9.0	32.4	22.2	107.5	54.7	139.2	67.2	0.7	0.0	0.0	0.7	1.3	0.7	1.3	437
29	0.7	0.0	0.0	0.0	0.0	0.7	0.7	0.0	0.0	0.0	0.0	8.4	38.0	122.8	144.9	20.6	0.7	0.0	0.0	0.0	2.0	0.0	0.0	2.0	341
30	2.0	0.7	0.0	0.0	0.0	0.7	0.0	0.0	0.7	1.3	19.5	25.9	32.4	42.7	41.3	113.2	98.5	4.2	0.0	40.8	1.3	4.2	0.7	1.3	431
31	1.3	2.6	0.0	0.0	0.0	1.3	0.0	0.0	0.0	0.0	1.3	18.3	20.1	32.4	20.6	1.3	11.9	16.4	31.6	20.1	7.7	2.0	0.7	0.0	190
KWh	259	109	268	556	226	167	40	24	16	169	601	1084	1242	1219	1202	1344	1179	1034	1563	1179	453	343	259	399	14937

Bagh	<u> </u>		June	2007	7					Win	d Pow	ver O	utpu	t of Be	onus (600/44	Turb	ine (N	lonth'	's Sun	nmary)			
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	0.0	1.3	0.0	1.3	0.0	0.0	0.0	0.0	0.0	7.7	27.7	49.3	66.3	47.7	44.0	22.4	9.0	4.2	0.0	2.0	6.1	7.7	0.7	0.0	297
2	2.6	0.0	32.7	9.5	154.6	101.1	119.8	113.2	154.5	146.6	105.3	55.9	18.4	105.3	96.6	40.1	60.6	40.6	0.7	5.5	0.7	0.7	1.3	0.0	1366
3	1.3	0.7	0.0	5.5	19.5	4.8	1.3	2.6	0.7	1.3	24.2	4.8	32.4	86.1	128.6	403.2	150.4	18.7	3.5	0.0	0.7	14.4	0.0	3.5	908
4	1.3	0.0	0.0	0.0	8.2	1.3	0.7	0.0	0.0	4.8	0.0	43.0	18.8	53.4	58.0	15.9	4.2	49.3	23.0	24.8	6.1	5.5	0.7	1.3	320
5	0.0	0.0	0.0	0.0	0.0	0.0	0.7	0.0	1.3	2.6	15.4	11.5	71.9	54.4	8.4	0.7	3.5	21.9	39.9	44.0	0.7	0.0	0.0	0.0	277
6	0.0	42.5	31.3	2.0	6.1	0.0	0.7	1.3	0.7	35.5	40.9	61.6	55.0	40.9	15.4	36.2	32.4	25.9	0.0	9.0	19.5	3.3	0.0	0.0	460
7	3.3	0.7	1.3	0.7	0.0	0.0	0.0	0.0	0.7	6.1	29.5	44.6	37.1	6.1	25.9	12.6	45.6	18.4	4.8	15.4	11.9	3.5	0.0	0.0	268
8	0.0	2.6	1.3	0.7	2.0	1.3	1.3	0.0	0.0	1.3	30.6	49.3	85.5	79.8	92.1	55.9	40.9	34.5	10.6	15.4	11.9	3.3	1.3	0.0	521
9	2.0	0.7	0.7	0.0	0.7	4.2	4.8	0.7	0.0	0.0	9.0	21.3	87.7	88.1	74.2	77.6	40.9	13.1	11.9	12.6	4.8	3.3	0.0	3.9	462
10	0.0	1.3	0.0	1.3	1.3	0.7	0.0	0.0	0.0	0.0	7.7	39.9	51.2	61.6	48.4	95.7	69.5	28.2	18.8	6.8	9.7	2.6	0.0	0.7	445
11	2.0	0.7	0.0	7.7	1.3	0.7	0.7	0.7	0.0	1.3	4.2	50.3	66.3	60.6	126.8	110.8	24.8	1.3	4.2	3.3	2.0	4.8	0.0	0.0	474
12	0.0	0.0	0.0	0.0	0.7	0.0	0.7	0.0	0.0	3.5	107.0	35.1	71.9	66.3	121.1	196.6	268.0	101.3	58.2	0.7	0.0	0.0	0.7	0.0	1031
13	1.3	85.2	3.5	0.7	0.0	2.6	0.7	0.0	0.0	4.8	44.6	44.6	40.9	126.8	134.7	100.6	216.4	167.6	76.4	128.4	205.2	13.9	0.7	0.0	1399
14	0.0	0.0	0.0	0.7	0.7	0.0	0.7	3.5	7.7	0.0	0.0	11.8	43.0	106.5	40.1	0.7	0.7	215.9	44.8	5.5	0.0	0.7	4.2	4.8	492
15	28.8	3.5	8.9	4.8	4.2	2.6	4.8	1.3	0.7	2.0	21.9	60.6	79.8	87.0	58.7	44.6	110.0	194.1	4.8	8.4	0.0	1.3	0.0	5.5	738
16	0.7	0.0	0.7	0.7	0.0	0.0	0.0	8.2	0.7	29.5	1.3	0.0	5.5	9.7	9.0	8.9	115.9	26.9	0.7	10.2	0.0	0.7	0.0	0.7	230
17	1.3	15.9	0.0	4.2	16.6	0.0	0.0	0.0	0.7	0.0	0.7	17.2	51.2	55.9	53.0	63.8	71.9	102.1	27.0	3.5	6.1	0.0	0.0	0.7	492
18	2.0	0.7	0.0	0.0	5.5	0.0	0.0	0.0	0.0	0.0	9.7	45.6	43.7	11.9	55.9	44.6	107.0	295.0	236.7	7.1	2.6	1.3	0.0	6.1	875
19	2.0	4.2	0.7	4.2	0.0	0.0	0.0	0.0	0.0	0.7	1.3	32.4	35.3	54.0	40.9	40.9	51.6	142.5	4.2	1.3	6.1	1.3	2.6	0.7	427
20	1.3	1.3	2.0	1.3	4.8	0.0	0.0	0.0	0.0	0.7	2.0	15.9	11.9	9.0	23.0	15.4	23.0	31.0	0.7	21.9	5.5	6.1	0.0	0.0	177
21	2.6	0.7	2.0	0.0	1.3	0.0	0.0	0.0	0.0	5.5	43.7	24.8	52.2	31.5	51.2	27.7	32.4	25.9	0.0	7.1	0.7	0.0	0.7	0.0	310
22	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.0	9.0	9.7	20.1	0.7	0.0	0.7	4.8	27.7	91.6	1.3	18.8	4.2	7.7	1.3	200
23	0.7	2.0	1.3	0.7	0.7	0.7	0.0	3.3	4.2	60.6	40.9	16.6	0.7	14.8	39.9	55.9	51.6	3.5	0.0	1.3	0.7	0.0	2.0	1.3	303
24	0.0	0.0	0.0	0.0	0.0	0.7	0.0	0.0	0.0	18.3	15.4	39.9	25.9	49.3	49.3	55.0	12.6	27.7	5.5	0.0	0.0	0.0	0.0	0.0	299
25	0.0	0.0	0.0	23.5	8.4	0.0	0.0	0.0	0.0	0.7	3.3	42.7	23.5	14.5	20.6	0.0	31.0	0.0	0.0	0.0	0.7	1.3	0.0	0.7	171
26	0.0	0.7	1.3	0.7	0.7	0.0	0.0	0.7	0.0	2.0	15.4	48.4	1.3	23.0	0.0	0.0	4.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	98
27	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	0.0	1.3	3.3	7.1	0.0	0.0	1.3	4.2	8.4	4.2	0.7	1.3	0.0	0.7	33
28	0.0	0.0	0.0	0.0	0.0	0.7	0.0	0.0	0.0	0.0	0.0	2.0	13.1	42.4	4.2	4.8	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	68
29	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	15.3	0.0	0.0	0.0	0.0	0.0	0.0	15
30	0.0	0.0	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.7	2.0	0.0	5
KWh	53	164	88	70	237	121	137	135	172	338	610	880	1114	1394	1421	1532	1584	1637	676	339	321	82	24	32	13160

Bagh	n	Ju	ly 200 ⁻	7							Wind	Pow	er Ou	utput	of Bo	onus 6	00/44	Turbir	ne (M	onth's	Sum	mary)		
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	0.0	0.0	0.0	1.3	0.0	0.0	0.0	0.0	0.0	0.0	10.6	25.9	12.6	27.0	30.6	44.6	33.3	55.0	29.5	0.0	0.0	0.0	0.0	0.0	270
2	0.0	49.5	24.2	0.7	2.0	0.0	0.0	1.3	4.8	1.3	0.0	15.3	1.3	24.8	8.4	0.7	14.1	19.5	21.3	0.0	0.0	0.7	0.0	0.0	190
3	0.0	0.0	0.0	1.3	0.7	0.0	1.3	0.0	0.0	1.3	27.7	29.5	77.6	31.6	20.0	5.5	8.4	0.0	0.7	2.6	0.0	2.0	0.0	0.7	211
4	0.7	0.0	0.0	0.0	0.7	0.7	0.7	0.0	0.0	3.3	15.4	31.7	51.2	27.7	11.3	11.3	2.0	15.4	0.0	0.0	0.0	0.0	0.0	0.0	172
5	0.0	1.3	2.6	0.0	0.0	0.7	0.0	0.0	0.7	20.1	12.6	15.4	13.7	27.7	46.6	79.8	30.5	10.8	9.0	0.7	0.0	0.0	200.5	7.1	480
6	9.0	0.7	4.8	4.8	0.0	1.3	0.7	2.6	4.8	4.2	6.1	30.5	25.9	36.2	39.9	21.2	27.7	1.3	0.0	2.0	0.0	0.7	0.0	0.7	225
7	0.7	0.0	0.0	0.7	0.7	1.3	11.9	0.0	3.5	4.2	55.9	45.6	6.1	71.9	94.9	72.7	2.0	8.9	0.0	0.0	0.0	0.0	0.0	2.6	383
8	0.7	2.6	0.7	1.3	142.0	35.5	1.3	2.0	50.0	12.4	11.3	5.5	40.1	4.8	11.9	30.6	44.6	5.5	0.0	4.2	0.0	0.0	0.0	0.0	407
9	2.6	1.3	4.8	4.2	1.3	1.3	1.3	0.0	0.0	1.3	6.8	19.5	35.3	50.3	50.3	41.7	12.6	19.5	0.0	4.2	0.7	0.0	3.3	0.0	262
10	1.3	2.6	0.0	2.6	0.7	0.0	0.7	0.0	0.0	0.0	9.0	44.6	44.6	32.4	35.3	30.6	6.1	11.3	4.8	0.0	0.0	0.0	0.0	0.7	227
11	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	0.0	9.0	55.0	27.7	15.4	12.6	21.9	7.1	0.0	12.4	0.7	0.0	0.0	0.0	0.0	0.0	162
12	0.0	2.0	9.5	0.0	1.3	0.0	0.0	0.0	0.0	0.0	8.4	8.4	5.5	2.0	16.6	9.0	0.7	20.6	27.7	106.0	9.0	19.5	1.3	0.7	248
13	15.3	15.9	9.5	4.2	2.0	0.0	4.2	2.0	0.0	0.0	1.3	3.3	36.1	44.6	6.1	9.0	6.1	111.3	69.2	1.3	0.0	1.3	0.0	2.0	345
14	2.0	0.0	0.0	0.7	7.1	0.7	1.3	0.0	3.5	9.7	35.3	9.7	16.6	1.3	27.7	7.7	12.6	4.2	20.0	133.6	60.7	2.0	0.7	0.7	357
15	0.7	15.9	5.5	0.7	0.0	0.0	0.0	0.0	0.0	2.6	12.6	14.4	27.7	9.7	39.9	132.0	69.8	4.8	0.7	1.3	0.0	1.3	0.7	0.0	340
16	2.0	0.7	0.7	0.0	1.3	0.7	0.0	0.0	0.0	0.0	5.5	2.0	20.1	44.6	30.6	29.5	44.6	28.8	0.0	4.8	9.0	2.0	0.0	1.3	228
17	0.7	0.0	0.0	0.7	0.7	4.8	0.0	0.0	13.9	11.8	25.8	2.0	42.7	35.3	9.0	2.6	20.1	11.8	0.7	14.4	0.0	2.6	2.6	0.0	202
18	1.3	0.0	1.3	0.7	1.3	3.5	2.6	0.0	0.0	3.5	6.1	6.8	39.9	25.9	26.6	87.7	10.6	4.2	8.4	12.6	3.5	0.0	0.0	0.7	247
19	0.0	0.0	0.0	0.0	0.7	0.0	0.0	0.0	0.0	0.0	8.4	11.9	3.3	42.7	36.6	43.7	30.6	13.7	0.0	0.0	1.3	0.0	0.0	0.0	193
20	0.7	0.0	0.0	0.0	0.0	2.0	0.0	0.0	0.0	0.0	6.1	21.9	8.4	86.3	51.2	45.6	4.8	0.0	0.7	0.0	0.0	0.0	0.0	0.0	228
21	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.8	0.7	0.0	0.7	0.0	17.4	12.4	12.6	49.3	50.3	24.8	20.9	3.5	11.8	17.2	1.3	0.0	228
22	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	28.2	20.6	45.8	7.7	55.9	5.5	0.0	2.6	2.6	0.0	0.0	2.0	0.7	172
23	0.0	0.0	0.7	0.0	0.0	0.0	0.0	0.0	0.0	5.5	6.1	0.0	18.8	15.4	1.3	0.0	0.0	0.0	0.0	0.0	9.0	1.3	0.0	1.3	59
24	0.0	2.0	2.0	0.7	1.3	1.3	0.0	0.0	0.0	0.7	6.1	35.3	27.7	44.6	44.6	11.3	3.9	2.6	2.0	3.5	30.6	95.8	10.2	1.3	327
25	4.2	1.3	1.3	0.0	1.3	0.7	4.8	0.7	0.0	18.3	9.7	39.9	42.7	48.4	48.4	3.5	29.8	5.5	0.7	1.3	0.0	0.0	1.3	0.0	264
26	0.0	2.0	0.7	0.0	1.3	2.0	0.0	0.0	0.0	1.3	6.1	20.1	12.6	6.8	15.4	61.9	39.9	170.4	31.0	7.1	1.3	0.0	0.0	0.0	380
27	2.6	0.0	0.7	0.7	0.7	1.3	1.3	0.7	0.0	1.3	3.5	9.7	0.7	4.2	0.7	0.0	0.0	0.0	1.3	5.5	2.0	2.0	4.2	0.7	43
28	1.3	2.0	4.8	0.0	0.7	1.3	0.0	0.0	0.0	0.0	12.6	27.7	18.3	20.1	39.9	50.3	19.0	0.7	0.0	2.6	0.7	0.0	0.0	0.0	202
29	38.5	4.2	0.0	0.0	1.3	0.0	0.7	0.0	1.3	3.5	3.5	9.0	1.3	8.2	27.7	0.7	0.0	0.0	0.0	2.0	1.3	0.0	0.0	0.0	103
30	2.6	1.3	0.0	1.3	6.1	0.0	0.7	2.0	0.0	2.0	0.0	3.5	4.2	1.3	0.0	33.5	35.3	0.7	0.0	4.2	0.0	0.0	0.0	0.0	99
31	0.0	0.0	0.0	0.0	0.0	1.3	1.3	0.0	2.0	6.1	15.4	50.3	39.9	47.4	17.2	28.8	17.2	8.9	0.0	0.0	0.0	0.0	0.0	0.7	237
KWh	87	105	74	26	175	60	35	17	85	123	383	595	728	894	831	1008	582	572	251	320	141	148	228	21	7488

Bagh	ı	Augu	ust 20	007							Win	d Pov	ver Ou	utput	of Bo	nus 60	0/44 T	urbin	e (Mo	nth's	Sumn	nary)		
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	2.0	0.0	2.0	1.3	0.7	0.7	9.0	8.4	0.7	7.7	9.7	55.9	27.7	6.1	0.7	0.7	0.0	1.3	0.7	33.7	21.6	4.2	4.2	0.7	199
2	0.0	1.3	1.3	0.7	2.6	0.7	0.0	0.7	2.0	0.0	0.7	52.1	0.0	1.3	0.0	2.0	0.0	0.0	0.7	6.1	0.0	0.0	0.7	2.6	75
3	2.0	0.0	0.0	0.7	0.7	1.3	0.0	0.7	0.0	0.0	5.5	4.8	3.5	3.5	1.3	2.0	0.7	0.0	0.0	0.0	0.7	0.0	7.7	17.4	52
4	0.7	0.7	0.7	0.0	0.7	0.0	0.7	0.0	0.0	0.7	2.0	30.6	20.1	15.4	53.5	103.4	13.1	3.3	3.5	8.4	0.0	0.0	25.6	14.1	297
5	2.0	9.7	3.9	1.3	0.7	0.0	1.3	0.0	0.0	0.0	1.3	9.7	12.6	1.3	27.7	13.1	19.5	3.5	0.0	0.0	1.3	0.0	0.0	5.5	114
6	17.7	0.7	1.3	2.0	2.0	0.0	2.0	0.0	2.0	2.0	0.0	0.0	5.5	1.3	22.7	37.1	24.8	0.7	0.0	3.5	7.1	1.3	5.5	0.0	139
7	0.0	0.0	0.0	0.7	0.7	0.0	0.7	2.0	6.1	0.0	0.0	0.0	2.0	0.7	0.0	0.0	0.0	0.0	0.0	0.0	2.6	0.0	6.8	0.7	23
8	1.3	0.0	2.0	0.0	2.6	0.0	1.3	0.0	0.0	0.0	0.0	14.8	9.7	32.4	21.3	30.6	9.7	8.4	0.0	0.0	2.0	0.0	3.9	3.5	143
9	0.0	0.0	0.0	0.0	0.0	0.0	0.7	0.0	0.0	0.0	8.2	29.5	29.2	6.1	35.3	50.3	27.7	4.2	0.0	0.0	0.0	0.0	0.0	0.0	191
10	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.2	11.3	9.0	2.6	0.0	25.6	45.6	61.6	10.6	1.3	0.0	0.0	0.0	0.0	0.0	172
11	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.0	27.7	18.3	2.0	0.7	0.7	11.3	9.7	7.1	0.7	0.0	0.0	0.0	0.0	0.0	80
12	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	2.0	20.1	27.7	29.5	74.2	26.9	119.7	40.8	10.2	0.7	2.0	12.4	4.8	1.3	0.7	373
13	0.0	1.3	8.9	0.0	0.0	3.5	0.0	0.0	0.0	0.0	2.0	2.0	1.3	4.8	25.9	27.7	35.3	33.3	1.3	4.8	0.0	0.0	54.5	19.4	226
14	84.0	8.4	0.0	0.0	1.3	0.0	0.0	0.0	0.7	0.0	2.0	6.8	23.0	21.3	32.4	32.4	14.8	0.7	0.0	0.0	0.0	0.0	0.0	0.0	227
15	0.0	45.2	0.7	1.3	0.7	3.5	3.5	0.7	0.0	0.0	0.0	2.0	3.3	18.3	39.9	20.1	27.7	0.0	0.0	0.0	0.0	0.0	0.0	0.7	167
16	0.0	0.7	0.7	0.0	0.7	0.0	1.3	0.0	0.0	0.0	15.9	9.7	15.4	20.1	32.4	15.4	6.1	5.5	0.0	0.0	0.0	0.0	0.0	0.0	124
17	0.0	0.0	0.7	4.2	4.2	0.7	2.6	1.3	0.0	0.0	7.7	35.3	49.3	66.3	44.6	30.6	37.1	12.4	5.5	1.3	11.9	0.7	0.7	1.3	318
18	8.4	0.0	0.0	0.0	0.7	0.0	2.0	0.0	0.0	0.7	20.1	19.5	23.0	40.9	15.4	1.3	9.0	4.2	0.0	0.0	0.7	0.0	0.7	0.0	146
19	0.0	0.0	2.0	0.0	0.7	0.0	0.0	0.0	0.0	6.1	12.6	39.9	14.8	13.7	27.7	20.1	24.2	9.7	1.3	4.2	23.0	0.0	0.0	14.5	214
20	27.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.6	4.8	2.0	63.8	83.2	27.7	2.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	214
21	0.0	0.0	0.0	0.7	0.7	0.0	0.0	0.0	0.0	2.0	9.0	30.6	55.0	74.2	79.8	30.6	33.3	18.1	4.2	0.7	0.7	0.0	0.0	0.0	339
22	0.0	2.6	0.0	0.0	0.0	1.3	0.0	0.0	0.0	0.0	2.0	15.4	27.7	50.3	45.6	55.9	1.3	0.0	0.7	0.0	0.0	0.0	0.0	0.0	203
23	0.0	0.0	0.0	0.0	0.0	0.7	0.0	0.0	0.0	4.8	23.0	30.6	2.6	31.0	27.7	20.6	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	142
24	0.0	0.0	0.0	0.0	0.0	0.0	0.7	0.0	0.0	0.7	0.0	3.5	40.9	6.1	20.1	39.9	4.8	0.0	0.0	0.0	0.0	0.0	0.0	0.7	117
25	0.0	0.7	2.6	1.3	1.3	4.8	0.0	0.0	2.0	3.5	50.3	19.5	8.9	0.0	77.4	27.0	61.6	43.0	8.4	0.7	0.0	1.3	0.0	0.0	314
26	0.0	0.7	1.3	5.5	0.0	0.0	1.3	3.5	0.0	0.0	7.7	40.1	24.8	16.6	68.5	7.1	0.7	95.2	29.8	0.0	2.6	2.6	1.3	0.7	310
27	0.7	5.5	2.0	3.5	0.7	1.3	2.6	0.0	11.8	0.0	3.3	45.6	15.2	9.0	9.0	23.0	16.6	0.0	0.0	1.3	0.7	1.3	2.0	0.0	155
28	0.0	2.6	3.5	7.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	3.3	0.7	8.4	23.0	20.1	4.8	2.0	1.3	0.7	0.0	1.3	0.7	0.0	81
29	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	24.2	20.1	39.9	9.7	35.3	20.1	9.0	20.6	6.1	4.2	0.7	0.0	0.0	0.7	0.0	191
30	0.0	0.0	0.0	0.0	3.5	0.0	0.0	0.7	0.0	0.0	2.0	20.1	9.7	4.2	0.0	4.8	5.5	10.2	0.0	0.0	0.0	0.0	0.0	0.0	61
31	0.0	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	1.3	21.2	30.6	15.4	11.9	21.9	20.1	10.8	12.4	1.3	0.0	4.2	0.0	2.0	2.0	156
KWh	146	80	34	31	25	18	29	18	26	64	290	648	548	658	855	824	522	302	65	68	91	17	118	84	5564

Bagh	Sentember	2007
Dayn	September	2001

Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	0.0	1.3	0.0	2.6	2.0	0.0	2.0	3.5	0.0	0.7	0.0	4.2	49.3	16.6	14.4	12.6	1.3	0.0	0.0	0.7	2.0	0.7	0.0	0.0	114
2	2.0	0.0	0.0	0.7	0.0	0.0	0.0	0.0	0.0	0.0	18.3	66.3	8.9	4.8	9.7	0.0	0.0	0.0	4.2	1.3	0.0	0.0	0.0	0.0	116
3	0.0	0.0	0.0	3.5	0.7	2.6	0.0	3.5	1.3	9.5	25.9	12.6	35.3	6.8	53.0	9.7	22.4	0.0	4.2	0.7	0.0	1.3	0.0	0.0	193
4	0.0	0.0	1.3	0.7	0.7	4.2	2.0	0.7	0.0	4.2	21.2	6.1	14.8	15.2	18.7	0.7	1.3	0.0	2.0	28.2	1.3	3.3	0.0	3.3	129
5	0.0	0.7	1.3	1.3	0.0	0.7	0.7	0.0	2.6	0.7	0.7	0.0	18.3	1.3	0.0	4.8	0.0	0.7	6.1	0.0	0.7	1.3	0.0	2.0	44
6	1.3	0.0	5.5	0.0	2.0	0.0	0.0	0.7	0.0	8.4	45.3	117.2	69.2	24.2	32.4	28.7	0.7	1.3	0.0	0.0	1.3	0.7	0.7	1.3	340
7	0.0	5.5	0.0	2.6	0.7	4.2	2.6	3.5	13.7	7.7	2.6	0.7	6.8	45.6	93.4	45.6	4.2	0.0	1.3	1.3	0.0	1.3	0.7	0.7	244
8	2.0	0.7	2.0	0.7	0.0	0.0	2.0	0.0	0.0	0.0	2.0	3.3	3.9	6.8	20.1	116.0	15.3	0.0	0.7	1.3	0.7	1.3	8.4	0.0	187
9	0.0	0.0	0.7	0.7	0.7	0.7	0.0	0.0	1.3	0.0	2.0	9.7	3.9	23.0	27.7	27.0	38.0	0.0	0.7	0.7	10.6	1.3	2.6	1.3	152
10	0.7	1.3	0.0	2.6	1.3	0.0	0.0	0.0	0.0	0.0	12.6	29.8	76.0	39.0	99.2	16.6	4.2	1.3	0.0	5.5	0.7	4.8	1.3	1.3	298
11	3.3	0.0	2.0	0.7	0.7	0.7	0.0	0.7	11.3	0.7	0.0	2.0	2.0	5.5	17.2	1.3	0.0	4.2	17.2	2.0	0.0	1.3	6.1	5.5	84
12	1.3	0.0	0.7	0.0	2.0	2.0	0.7	0.0	0.0	2.6	1.3	15.4	30.6	25.9	30.6	30.6	12.6	0.7	0.0	0.0	0.7	0.7	2.0	0.0	160
13	3.3	0.0	0.0	2.6	0.7	0.0	0.0	0.0	4.8	0.7	18.3	18.3	20.1	35.3	71.9	55.9	24.8	28.8	3.5	0.0	0.0	0.0	0.0	0.0	289
14	0.0	0.0	0.7	0.0	0.0	1.3	0.7	0.0	0.0	2.6	24.8	44.6	25.3	18.4	27.7	2.0	0.0	0.0	0.0	1.3	4.2	0.0	3.3	0.0	157
15	0.0	2.6	0.0	2.0	2.6	0.0	2.0	0.0	0.7	0.7	23.0	15.4	6.8	23.0	32.4	47.4	42.7	24.2	11.9	0.7	7.1	0.0	1.3	0.7	247
16	1.3	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.8	6.8	24.8	20.1	51.2	70.1	107.5	26.0	0.0	8.4	18.1	2.0	0.0	2.6	0.7	345
17	1.3	2.0	0.0	0.7	0.0	0.0	8.4	0.7	0.7	8.4	6.8	30.5	51.2	2.6	0.0	5.5	0.0	0.0	0.0	2.0	0.0	5.5	0.7	0.7	127
18	0.7	0.7	0.7	4.8	0.0	0.7	0.0	0.0	0.0	0.0	5.5	30.6	25.9	44.6	18.3	32.4	12.4	0.0	2.6	0.0	2.6	0.7	0.7	2.0	186
19	0.0	0.0	0.0	0.0	0.0	0.7	0.0	0.0	0.0	0.0	2.0	18.3	39.9	67.2	55.9	59.2	0.7	0.7	0.0	0.7	0.0	0.7	0.0	0.7	246
20	0.7	0.0	0.7	1.3	0.0	0.0	0.0	0.0	0.0	0.0	1.3	56.9	36.6	0.7	9.0	1.3	1.3	0.7	0.7	0.0	1.3	1.3	2.0	0.0	116
21	3.3	2.6	0.7	0.7	2.0	0.0	0.7	0.0	0.0	0.0	2.6	24.8	50.3	55.9	20.1	0.7	4.2	1.3	24.2	2.0	2.0	1.3	1.3	0.7	201
22	0.0	2.0	0.7	2.6	2.0	56.3	0.0	0.0	0.0	0.0	0.0	4.2	0.0	0.7	0.7	0.7	11.8	0.7	1.3	8.4	0.7	4.2	5.5	1.3	103
23	1.3	1.3	0.7	0.0	0.0	0.7	0.7	0.0	0.0	0.0	0.0	0.7	9.7	12.6	29.2	111.3	40.9	22.7	0.7	4.8	0.0	1.3	2.0	0.7	241
24	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	0.0	2.6	18.3	12.6	39.9	32.4	50.3	66.3	11.8	5.5	6.1	5.5	2.6	0.7	0.7	2.0	258
25	0.7	2.0	0.0	0.0	0.7	1.3	0.7	0.0	0.0	0.0	3.3	5.5	30.6	21.2	25.9	49.3	8.9	0.0	3.9	4.8	3.9	0.7	0.0	0.0	163
26	0.7	0.7	0.0	0.0	0.7	0.0	0.0	0.0	0.0	0.0	12.6	27.7	49.3	39.9	60.6	55.0	6.1	4.8	11.3	1.3	0.7	0.7	0.0	0.7	272
27	1.3	0.0	2.6	0.7	0.0	1.3	2.0	0.0	0.0	7.1	44.6	31.5	55.0	55.0	58.7	15.9	4.2	11.3	7.1	1.3	0.0	19.0	18.1	5.5	342
28	5.5	3.5	0.7	1.3	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.7	18.3	18.3	23.0	5.5	4.8	17.1	11.9	0.7	2.0	1.3	0.0	5.5	123
29	0.0	3.3	0.0	1.3	1.3	0.7	1.3	0.0	0.0	0.7	3.3	23.0	21.2	23.0	22.4	19.5	24.5	0.0	27.7	4.8	1.3	0.0	2.0	0.0	181
30	0.0	0.7	1.3	2.0	2.6	0.7	1.3	0.0	0.0	0.7	0.7	9.7	15.4	27.7	23.0	11.3	0.7	11.9	19.5	0.0	0.0	2.0	1.3	0.0	132
KWh	30	31	22	36	23	79	28	15	36	62	305	647	834	744	1015	940	325	138	177	98	48	57	63	36	5788

Bagh		Oct	ober 2	007							W	ind Po	ower (Output	of Bor	us 60	0/44 T	urbin	e (Moi	nth's S	Summ	nary)			
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	0.0	1.3	1.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	3.3	14.8	15.4	14.8	9.0	0.0	2.6	25.9	14.8	1.3	1.3	0.0	1.3	108
2	1.3	0.7	1.3	2.0	0.0	2.0	1.3	1.3	0.0	0.0	1.3	12.6	21.2	30.6	18.3	4.8	0.0	13.1	27.7	1.3	1.3	2.0	4.2	0.0	148
3	0.0	2.0	0.0	0.7	0.0	2.6	1.3	0.0	0.0	0.0	1.3	6.1	23.0	24.2	44.8	86.6	19.5	31.7	4.8	0.7	0.7	2.6	1.3	11.3	265
4	4.2	0.7	1.3	0.7	0.0	1.3	1.3	0.7	0.0	0.0	0.0	0.0	19.5	59.2	16.6	9.5	13.7	18.4	12.6	4.2	0.0	0.0	1.3	0.7	166
5	6.1	0.7	0.7	0.7	1.3	0.0	0.0	0.0	0.0	0.0	0.0	6.1	24.2	15.4	22.4	9.0	0.0	1.3	25.9	4.8	0.7	0.0	1.3	1.3	122
6	7.1	0.0	6.1	0.0	2.0	0.0	0.7	0.0	0.0	0.0	0.0	11.3	30.6	39.9	25.9	27.7	46.6	35.3	15.4	4.8	2.6	4.2	0.7	0.7	261
7	0.7	4.8	2.6	0.0	2.0	0.0	0.0	2.6	0.0	0.0	0.0	9.7	39.9	25.9	42.7	9.5	0.7	30.6	27.7	15.4	0.0	1.3	0.7	0.7	217
8	2.0	0.7	0.7	2.0	0.0	8.4	0.0	0.0	0.0	0.0	1.3	3.3	12.6	32.4	23.0	19.5	0.7	9.7	9.7	0.7	0.0	2.6	0.7	0.0	129
9	2.6	0.7	0.0	0.0	1.3	2.6	7.7	0.0	0.0	0.0	0.0	6.1	25.9	32.4	12.6	9.0	0.0	13.7	39.9	0.7	0.0	0.0	0.0	0.0	155
10	0.7	0.0	6.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	6.1	25.9	35.3	25.9	27.7	24.8	0.7	2.0	30.6	17.2	0.0	0.7	0.0	0.7	204
11	0.7	0.0	2.0	0.7	0.7	0.0	0.0	0.0	0.0	0.0	2.6	18.3	15.4	27.7	32.4	21.3	3.5	7.1	21.2	4.2	0.0	0.0	0.0	3.3	161
12	1.3	0.0	0.0	0.7	1.3	0.0	0.0	0.7	0.0	0.0	0.0	26.6	49.3	45.6	38.0	31.7	0.0	5.5	17.2	0.7	0.0	0.0	1.3	0.7	220
13	0.0	0.0	0.7	0.7	2.6	0.7	0.7	0.0	0.0	0.0	0.0	1.3	8.4	32.4	13.1	5.5	0.0	2.6	14.4	5.5	0.0	0.7	0.7	0.0	90
14	2.0	0.7	1.3	0.0	0.0	2.6	0.0	2.0	0.0	0.0	0.7	3.9	21.2	40.8	21.3	48.4	2.0	7.7	15.4	0.0	0.0	0.7	2.0	1.3	174
15	2.0	3.3	2.0	2.0	0.0	1.3	0.0	0.0	0.0	0.0	0.0	6.1	21.3	27.0	29.2	26.9	31.0	9.7	8.4	4.2	2.6	1.3	2.0	2.0	182
16	0.0	2.0	0.0	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.7	24.8	71.9	67.2	71.9	71.6	12.4	0.7	13.7	8.4	2.0	0.0	1.3	2.6	353
17	1.3	2.0	0.0	0.7	1.3	0.7	4.8	0.7	0.0	0.7	23.0	61.6	79.8	85.5	105.3	74.2	8.9	0.0	15.9	20.1	13.7	1.3	0.0	0.0	501
18	0.0	0.0	0.7	2.0	0.7	0.0	1.3	0.0	0.0	0.0	2.0	9.7	25.9	45.6	44.6	30.6	0.0	0.7	3.9	0.0	0.7	0.0	0.0	0.0	168
19	3.3	0.0	0.0	0.0	1.3	0.7	0.0	0.0	0.0	0.0	0.0	3.9	30.6	25.9	9.7	13.7	0.0	4.2	1.3	0.0	0.7	0.0	0.0	0.0	95
20	0.0	0.0	0.0	2.0	0.0	0.0	0.7	0.0	0.0	0.0	0.0	8.4	23.0	30.6	23.0	9.0	30.6	11.8	5.5	0.7	3.3	0.0	0.0	0.0	148
21	0.0	0.0	2.6	0.0	0.7	0.0	3.3	3.5	0.0	0.0	0.7	2.0	18.3	25.9	8.4	9.0	0.0	4.8	12.6	0.7	0.0	0.7	0.7	0.0	94
22	0.7	0.0	0.0	2.6	0.7	0.0	0.0	2.6	0.0	0.0	2.0	15.4	39.9	55.9	60.6	26.3	0.7	9.5	5.5	0.0	0.0	0.0	0.0	2.0	224
23	0.7	3.3	0.7	0.0	1.3	2.0	0.7	0.0	0.0	0.0	0.0	2.0	36.4	21.2	27.7	61.6	22.7	6.1	6.8	3.9	0.0	0.7	1.3	0.0	199
24	2.0	0.0	0.0	0.0	0.7	0.7	4.2	0.0	0.0	0.0	0.0	2.6	35.3	35.3	12.6	0.7	0.0	7.7	9.0	2.6	0.7	0.0	0.0	0.0	114
25	0.0	0.7	0.7	0.0	9.0	4.2	0.7	0.0	0.0	0.0	0.7	20.1	39.9	40.9	13.1	0.0	0.0	2.0	0.7	9.0	0.0	0.7	0.0	0.0	142
26	0.0	2.0	0.0	0.0	1.3	0.0	1.3	0.0	0.0	0.0	0.0	2.0	27.7	39.9	33.3	66.3	26.0	2.0	9.0	2.6	1.3	0.0	0.7	0.0	215
27	0.0	0.0	0.0	0.7	0.7	0.7	0.0	1.3	0.0	0.0	2.6	23.0	35.3	55.0	53.5	23.5	0.0	13.1	12.6	3.5	1.3	0.7	1.3	2.0	230
28	0.0	3.3	0.0	1.3	0.0	0.0	1.3	0.0	0.0	0.0	0.0	9.0	24.8	44.6	15.4	7.7	0.0	6.1	11.9	4.2	0.0	0.0	0.0	0.0	130
29	0.0	0.0	0.0	0.7	0.0	2.0	0.0	0.0	0.0	0.0	0.0	23.0	66.3	49.3	44.6	28.8	0.0	14.1	12.6	3.9	0.7	0.0	0.0	2.0	248
30	0.0	0.0	0.0	0.0	0.7	0.0	2.6	0.0	0.0	0.0	0.0	6.1	45.6	27.7	27.7	7.1	0.0	14.8	4.8	0.7	0.0	1.3	0.0	2.0	141
31	1.3	1.3	0.7	2.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.0	9.7	30.6	49.3	3.5	0.0	2.0	0.0	3.3	0.7	2.0	1.3	0.7	110
KWh	39	30	31	22	30	33	34	15	0	1	45	356	973	1156	983	777	219	290	422	142	34	24	22	35	5713

Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	1.3	4.8	0.0	1.3	0.0	1.3	0.0	0.0	0.0	0.0	0.7	2.0	23.0	25.9	25.9	7.7	0.0	2.0	0.7	1.3	0.0	2.0	1.3	0.7	102
2	0.0	1.3	0.0	2.0	0.0	2.0	1.3	0.0	0.0	0.0	0.0	3.3	30.6	50.3	35.3	10.6	0.7	1.3	0.0	2.6	0.0	0.0	0.0	0.0	141
3	0.7	0.7	0.0	0.0	1.3	0.0	0.0	2.6	0.0	0.0	8.4	28.7	3.9	4.8	8.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	59
4	0.0	0.0	0.0	0.7	1.3	0.0	0.7	0.7	0.0	0.0	0.7	0.7	4.2	0.0	3.5	1.3	0.0	0.7	0.7	0.7	1.3	0.0	3.9	0.0	21
5	1.3	2.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	1.3	9.0	11.3	0.0	0.7	9.0	0.7	2.0	0.7	3.3	0.7	3.9	46
6	0.0	2.0	0.0	2.0	0.7	0.7	1.3	0.0	0.0	0.0	0.0	0.7	12.6	6.8	39.9	11.3	0.7	1.3	0.0	2.0	0.7	1.3	0.7	5.5	90
7	0.7	1.3	0.0	2.6	0.0	2.6	0.0	0.0	0.0	0.0	0.0	2.0	34.2	30.6	32.4	4.8	0.0	2.0	1.3	0.7	0.7	0.7	0.0	0.0	116
8	0.7	1.3	0.7	0.0	0.0	1.3	0.7	1.3	0.0	0.0	0.0	2.6	15.4	23.0	11.9	1.3	0.0	2.6	1.3	1.3	0.0	0.0	0.0	0.0	65
9	0.7	0.0	0.7	1.3	0.0	0.7	0.0	0.0	0.0	0.0	0.7	21.9	20.1	18.3	12.6	3.5	0.0	4.2	1.3	0.0	0.0	0.0	0.0	0.0	86
10	0.0	1.3	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	14.8	23.0	15.9	3.3	14.8	0.7	6.8	1.3	0.0	0.0	0.0	0.0	83
11	0.0	0.0	0.0	0.0	0.0	0.7	0.0	0.0	0.0	0.0	0.0	2.0	6.1	15.4	21.2	0.7	0.0	2.6	0.7	0.0	0.0	0.0	0.0	0.7	50
12	0.0	0.0	1.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	23.0	20.1	49.3	7.7	0.0	5.5	1.3	2.0	4.2	0.0	5.5	2.0	122
13	0.0	0.7	0.7	0.0	4.8	0.0	1.3	3.3	0.0	0.0	0.0	4.2	33.3	49.3	44.6	7.1	0.0	0.0	0.0	3.3	0.0	1.3	0.0	1.3	155
14	1.3	0.0	1.3	0.0	0.0	1.3	0.0	1.3	0.0	0.0	0.0	4.2	39.9	44.6	17.2	1.3	0.0	0.0	0.7	3.3	0.0	2.0	0.0	1.3	120
15	0.0	0.0	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.3	18.3	30.6	18.3	7.1	0.7	2.6	0.0	2.0	0.7	0.7	0.0	6.1	89
16	0.0	1.3	0.7	0.0	0.0	0.0	0.7	0.7	0.0	0.0	0.0	0.0	5.5	30.6	21.2	4.2	0.7	12.6	2.0	0.0	0.0	0.0	2.0	0.7	82
17	1.3	2.0	0.0	1.3	0.0	1.3	0.7	0.7	0.0	0.0	0.0	0.0	14.8	39.9	25.9	7.1	0.0	6.1	2.0	0.7	0.0	1.3	0.7	0.7	106
18	0.7	0.7	0.0	1.3	0.0	0.0	0.0	0.0	0.0	0.0	0.7	1.3	9.0	30.6	21.2	2.0	0.0	1.3	0.7	0.7	2.0	0.0	0.0	0.0	72
19	0.0	0.0	0.0	0.0	0.7	4.2	0.0	0.0	0.0	0.0	0.0	0.0	11.9	39.9	44.6	7.1	0.0	2.0	0.0	1.3	0.0	1.3	0.0	0.0	113
20	0.7	0.0	0.0	0.0	0.0	0.0	1.3	0.7	0.0	0.0	0.0	0.0	2.0	47.4	25.9	12.4	0.0	1.3	0.7	1.3	0.0	2.0	0.7	2.0	98
21	0.7	0.7	2.0	0.0	0.0	2.6	0.0	1.3	0.0	0.0	0.0	0.7	4.8	9.7	37.1	0.0	0.0	2.0	1.3	0.0	0.7	0.0	2.0	0.0	65
22	0.0	2.0	0.7	0.7	0.0	0.0	0.7	0.0	0.0	0.0	0.0	0.0	4.2	3.3	6.1	0.0	0.0	2.6	0.0	0.7	0.7	1.3	2.0	2.0	27
23	0.7	2.6	0.0	0.7	0.0	0.7	1.3	0.0	0.0	0.0	0.0	0.0	0.7	0.7	1.3	0.0	0.7	2.0	0.0	0.0	0.0	3.3	0.0	0.0	14
24	1.3	2.0	0.0	0.7	2.6	0.7	0.0	0.0	0.0	0.0	0.7	0.0	0.0	0.0	5.5	0.0	0.7	2.0	0.7	0.0	0.0	1.3	0.7	0.7	19
25	3.3	0.0	1.3	0.0	0.0	0.0	1.3	0.0	0.0	0.0	0.0	0.0	0.7	0.7	0.0	0.0	0.0	3.3	6.8	0.0	0.7	2.0	0.0	2.0	22
26	0.7	0.0	0.0	0.0	0.0	2.6	0.7	0.0	0.0	0.0	0.0	0.0	0.7	14.1	2.0	0.0	0.0	3.3	0.7	0.0	0.0	2.0	1.3	0.0	28
27	0.0	0.7	0.0	1.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	6.1	1.3	0.0	0.0	0.0	0.0	1.3	0.0	0.0	0.0	0.0	11
28	0.7	0.0	0.0	0.0	0.0	0.7	0.0	0.0	0.0	0.0	0.0	0.7	1.3	30.5	50.3	9.7	0.7	0.0	0.0	1.3	0.0	0.7	0.7	0.0	97
29	0.0	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	8.9	60.6	26.9	0.0	0.0	0.0	0.7	0.0	30.0	25.3	20.0	0.7	174
30	0.0	0.0	0.0	5.5	1.3	0.0	0.0	0.0	4.8	0.0	0.0	0.0	2.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.3	15
KWh	16	28	10	21	13	23	12	12	5	0	12	78	347	666	617	110	20	72	30	29	42	51	42	31	2287

Bagh	December 2007	
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Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	0.0	0.0	1.3	0.0	0.0	0.0	0.0	0.7	0.0	1.3	15.4	9.7	9.7	2.6	17.2	21.3	0.0	0.0	0.0	0.0	0.0	2.0	1.3	0.0	82
2	0.7	0.0	0.0	0.0	0.0	0.7	1.3	0.7	0.0	0.0	0.0	1.3	13.7	23.0	15.4	6.1	0.0	0.0	9.0	0.0	1.3	0.0	2.0	0.0	75
3	0.0	0.0	0.0	2.0	0.7	0.0	0.0	0.7	0.0	0.0	0.0	0.0	6.8	35.3	19.5	0.0	2.0	2.6	1.3	1.3	4.8	0.7	0.0	2.0	79
4	0.7	0.0	0.0	0.0	0.0	1.3	1.3	0.7	0.0	0.0	0.0	0.0	0.0	0.0	1.3	0.0	0.7	2.0	0.0	0.0	1.3	0.7	1.3	0.0	11
5	0.7	2.0	0.0	0.0	1.3	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.7	0.7	4.8	1.3	0.0	0.0	3.3	0.0	0.7	0.0	1.3	0.0	17
6	0.0	0.0	0.0	0.0	0.0	0.7	0.7	2.6	4.2	0.0	0.7	0.0	0.0	0.0	14.4	0.0	0.0	0.0	0.7	0.7	1.3	0.0	1.3	2.0	29
7	0.0	0.0	1.3	0.7	0.0	0.0	0.0	0.0	0.7	0.0	0.0	0.7	11.9	23.0	6.8	7.1	0.0	1.3	0.0	0.0	0.7	0.0	0.7	0.0	55
8	0.7	1.3	2.0	0.7	0.0	1.3	0.0	0.0	0.0	0.0	0.0	0.7	1.3	16.6	35.3	1.3	0.0	3.3	0.0	0.0	2.0	0.0	0.0	0.0	66
9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	9.5	21.6	0.7	4.8	4.8	0.7	31.6	0.7	2.0	0.0	0.0	0.0	4.2	12.6	2.6	0.0	96
10	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.6	0.0	0.0	24.2	4.2	1.3	0.0	0.0	0.0	1.3	0.7	0.0	0.7	35
11	0.0	0.0	0.7	2.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	9.5	50.3	55.0	50.3	40.9	18.8	0.7	0.0	2.0	0.0	0.0	0.0	0.0	230
12	1.3	0.0	0.0	14.8	4.2	0.0	0.0	0.0	14.1	3.5	14.5	4.8	4.8	2.0	0.0	4.2	4.8	0.0	0.0	0.0	0.7	0.0	0.0	0.0	74
13	0.0	0.0	1.3	0.7	0.0	0.0	0.0	0.0	0.7	7.7	19.5	25.1	17.4	8.4	7.7	0.7	0.0	1.3	0.7	0.0	0.0	0.0	0.7	0.0	92
14	0.0	0.0	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	0.0	3.3	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5
15	0.0	0.0	0.0	0.0	0.0	0.7	1.3	3.3	3.9	5.5	9.7	23.0	24.0	71.9	66.3	114.9	77.6	61.6	3.5	0.7	0.0	0.0	0.0	0.0	468
16	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	0.0	0.0	0.0	0.7	4.8	23.0	21.2	4.2	0.0	6.8	2.0	0.0	0.0	0.7	1.3	0.0	65
17	0.0	0.0	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	6.1	21.2	35.3	12.4	138.6	113.2	52.7	0.0	0.0	0.0	0.0	0.0	0.0	381
18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.3	0.7	0.0	0.0	2.0	1.3	0.7	0.0	0.0	0.0	1.3	0.0	0.0	0.0	0.7	0.0	0.0	8
19	1.3	4.8	2.0	0.0	0.0	0.0	0.7	0.0	0.0	0.0	0.0	3.3	3.3	21.2	55.0	8.9	0.0	1.3	1.3	7.7	18.4	1.3	3.5	0.0	134
20	1.3	3.5	36.1	9.0	4.2	1.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	1.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.3	0.7	59
21	1.3	1.3	0.7	9.0	6.8	0.7	3.3	0.0	1.3	0.0	0.0	0.0	0.0	0.7	2.0	0.0	0.7	2.0	0.7	0.7	0.0	0.7	3.3	0.0	35
22	1.3	0.0	1.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.3	12.6	4.2	23.5	0.0	4.8	1.3	2.0	0.0	1.3	2.0	2.0	0.0	57
23	1.3	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.3	0.0	0.0	0.0	0.7	1.3	5
24	3.5	0.7	0.0	0.0	0.0	2.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	5.5	2.0	18.3	0.0	0.0	2.0	0.0	0.0	0.7	0.0	0.7	36
25	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	1.3	12.6	15.4	9.7	4.8	0.0	2.0	0.0	0.0	1.3	0.0	0.0	0.0	48
26	0.0	0.0	0.0	0.0	2.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	16.6	49.3	39.9	7.7	0.0	2.6	0.0	1.3	0.0	0.0	0.7	0.7	121
27	0.0	0.0	0.0	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.3	6.1	18.3	4.2	0.0	2.6	4.8	0.0	0.7	0.7	0.0	1.3	41
28	0.0	0.0	0.7	0.7	2.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	15.9	61.6	40.9	0.7	0.7	5.5	4.8	1.3	0.7	2.0	1.3	140
29	1.3	0.0	0.0	2.0	0.0	0.0	0.0	0.0	0.0	0.7	1.3	0.0	2.0	29.5	36.2	4.8	0.0	2.6	1.3	0.7	2.6	0.0	0.7	0.0	85
30	4.2	0.7	0.0	0.7	1.3	0.0	1.3	0.0	0.0	0.0	0.0	0.0	2.0	23.0	25.9	0.7	0.0	12.6	2.0	0.7	0.0	0.0	0.0	0.0	75
31	0.0	1.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	1.3	24.8	39.9	4.2	0.0	1.3	6.8	0.0	1.3	5.5	0.0	0.7	88
KWh	19	16	48	43	23	9	10	10	35	40	63	97	226	494	647	440	226	162	48	20	45	29	26	11	2790

Bagh	1	Jani	uary 2	800							Wind	Pow	er Out	tput o	f Bon	us 60	0/44 Tı	ırbine	(Mor	nth's	Sum	mary)			
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	0.0	2.0	0.0	0.0	0.0	0.0	0.0	0.7	2.0	0.0	0.0	0.0	0.7	20.1	4.8	0.0	0.0	0.0	2.6	1.3	5.5	0.7	0.0	0.7	41
2	0.0	0.0	1.3	0.7	0.0	1.3	0.0	0.0	0.0	0.0	0.0	0.7	3.3	9.7	25.9	15.9	0.0	6.1	1.3	2.6	0.7	2.6	0.0	2.0	74
3	0.0	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.7	0.0	0.0	0.0	0.0	0.7	0.0	0.7	0.0	0.0	0.0	1.3	0.7	3.3	0.0	4.8	13
4	1.3	0.0	0.0	0.0	0.0	0.0	5.5	0.0	0.7	0.0	0.7	0.0	0.0	0.0	2.6	1.3	0.0	0.0	1.3	4.8	2.0	0.0	0.0	0.7	21
5	7.7	4.2	7.7	0.0	2.6	0.7	0.0	0.7	0.0	0.0	0.0	0.7	0.0	0.0	0.0	0.0	0.7	0.0	0.0	0.0	0.0	0.0	1.3	0.7	27
6	0.0	0.0	4.2	0.0	0.0	6.1	0.7	0.0	0.0	0.0	0.7	0.0	0.0	2.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	0.7	0.0	0.0	15
7	0.0	0.0	0.0	0.0	0.7	8.4	7.1	0.7	0.7	0.7	0.0	1.3	0.0	0.7	3.5	0.0	3.5	8.9	8.9	0.0	1.3	15.8	34.8	3.5	100
8	0.0	2.6	0.7	0.7	0.7	1.3	2.0	0.7	0.0	0.0	1.3	15.4	11.3	0.7	13.7	45.6	22.4	5.5	0.7	3.5	0.0	0.7	0.7	0.7	130
9	1.3	0.7	0.7	0.7	0.0	4.2	0.0	22.7	4.8	12.4	8.9	2.6	0.0	0.0	0.0	0.0	0.0	0.7	8.4	4.8	5.5	19.4	1.3	23.5	122
10	1.3	0.7	4.2	0.0	0.0	0.0	0.0	2.0	0.0	0.0	0.0	0.0	3.5	3.5	51.4	25.3	36.1	15.9	11.3	0.7	0.7	0.0	0.0	0.0	156
11	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.3	0.0	1.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3
12	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	0.7	0.0	0.0	0.0	0.0	1.3	0.0	3.9	2.0	0.0	0.0	0.0	8
13	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.3	4.8	9.7	30.6	4.2	4.2	9.7	3.3	2.0	0.0	0.0	0.0	0.0	70
14	0.0	0.0	0.0	0.0	0.0	0.0	0.7	0.0	0.7	0.0	0.7	0.0	0.7	2.0	15.9	0.0	0.0	0.7	0.0	1.3	0.0	0.0	0.7	0.0	23
15	0.0	0.0	0.0	0.0	1.3	0.7	4.8	3.5	0.0	0.0	0.0	0.0	11.9	4.8	12.6	2.6	0.7	2.0	0.0	0.0	0.0	0.0	2.0	0.0	47
16	0.0	0.0	0.0	0.0	0.7	1.3	17.7	4.2	4.8	11.9	0.0	2.6	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	44
17	0.0	0.0	4.2	0.0	1.3	0.0	0.0	0.0	7.1	1.3	1.3	0.7	0.0	0.0	0.0	1.3	0.0	0.0	0.0	0.0	21.6	4.8	4.8	0.7	49
18	11.3	1.3	0.7	0.7	0.0	0.0	1.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	0.0	1.3	1.3	1.3	0.0	0.0	0.0	0.0	20
19	0.0	0.0	0.0	0.0	0.0	0.7	2.6	0.0	0.0	0.7	0.0	0.0	2.0	5.5	6.1	2.0	1.3	1.3	11.9	9.0	1.3	1.3	2.0	1.3	49
20	2.0	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	6.1	12.6	30.6	19.5	27.7	0.7	0.0	0.0	0.0	0.0	4.8	6.1	2.6	114
21	0.0	0.0	1.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.3	1.3	1.3	12.6	5.5	0.0	8.4	17.2	1.3	2.0	0.0	0.0	0.0	52
22	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.3	15.3	54.5	23.0	5.5	17.7	0.7	0.0	5.5	2.0	0.0	0.0	0.7	126
23	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.3	12.6	27.7	53.5	20.1	12.6	8.4	0.0	0.7	0.7	0.0	0.7	2.6	141
24	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.2	17.2	44.6	30.6	2.6	4.2	0.0	0.0	0.7	0.0	0.0	0.0	0.0	104
25	0.0	0.0	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.0	20.1	23.0	51.2	55.9	24.2	0.0	0.0	0.7	0.0	0.0	0.0	0.7	179
26	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.0	3.3	23.0	49.8	39.2	13.7	11.3	1.3	0.0	0.0	1.3	4.8	0.0	150
27	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.3	6.8	5.5	24.8	33.3	74.2	101.3	29.2	66.3	3.5	0.7	0.0	0.7	2.0	349
28	0.7	0.0	0.0	0.0	5.5	61.3	77.8	15.9	2.0	0.0	0.0	0.7	9.0	35.3	25.9	50.3	5.5	4.2	8.4	0.7	0.7	2.6	0.7	0.0	307
29	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	1.3	30.3	18.4	14.8	4.2	5.5	15.3	1.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	92
30	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.0	6.1	15.4	18.3	11.9	16.6	20.1	9.7	0.7	0.0	0.0	1.3	102
31	0.0	0.7	0.0	0.0	2.0	0.7	0.7	2.0	0.0	0.0	2.0	7.7	23.0	35.3	30.6	50.3	4.2	0.0	0.0	3.3	0.7	1.3	2.6	0.0	167
KWh	25	13	25	3	15	86	121	53	24	28	48	77	176	369	519	464	267	132	164	62	49	59	63	48	2892

Bagh		Febr	uary 2	2008							Wind	Pow	er Ou	tput of	Bonu	s 600/4	4 Turb	ine (N	lonth	's Sur	nma	ry)			
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	4.8	0.7	0.0	0.0	0.7	0.7	0.0	0.0	0.0	0.0	0.0	1.3	20.1	30.6	39.9	12.6	0.7	0.0	6.1	0.7	1.3	0.0	1.3	2.0	123
2	0.7	1.3	1.3	4.2	1.3	2.0	0.0	0.0	0.0	0.0	2.0	0.0	1.3	4.8	30.5	4.8	26.3	1.3	5.5	0.0	6.8	0.7	4.8	1.3	101
3	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1
4	0.0	0.0	0.0	0.0	7.1	0.0	0.7	1.3	0.0	0.7	0.0	4.2	0.0	0.0	3.3	0.0	1.3	0.0	2.6	4.8	9.0	19.5	3.5	0.0	58
5	4.2	2.0	4.2	4.2	4.2	1.3	8.4	0.0	0.0	0.0	0.0	0.0	0.0	4.2	3.9	6.8	1.3	0.0	1.3	0.0	0.7	0.0	0.0	0.7	47
6	1.3	0.0	0.7	0.0	0.0	1.3	1.3	0.0	0.0	0.0	1.3	4.8	30.5	17.2	44.6	20.1	12.6	15.9	0.0	0.0	0.0	0.0	2.0	2.0	155
7	0.7	0.7	0.0	0.0	2.0	0.0	0.0	26.3	16.4	4.2	0.0	0.0	0.7	3.5	0.0	0.7	0.0	0.0	0.7	0.0	0.0	0.0	0.0	0.0	56
8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	8.4	23.0	35.3	12.6	6.1	2.0	0.0	0.0	2.0	0.7	0.0	0.0	90
9	0.0	0.7	0.0	0.7	0.0	0.0	0.0	0.0	0.0	0.7	1.3	9.0	21.2	21.2	15.4	11.9	0.0	0.7	15.4	4.2	0.0	0.0	0.0	0.0	102
10	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	9.0	39.9	44.6	40.9	12.6	0.0	1.3	1.3	2.6	0.0	0.0	0.7	0.0	153
11	0.0	0.7	0.0	0.0	0.7	0.0	0.0	0.0	0.0	0.0	0.0	5.5	9.0	12.6	67.9	0.7	5.5	1.3	0.7	4.2	2.0	2.0	0.7	0.0	113
12	0.0	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	11.3	15.4	5.5	40.8	45.3	76.4	71.9	58.7	20.1	26.3	0.0	0.0	0.7	2.0	376
13	0.0	0.7	0.0	0.0	1.3	0.0	0.0	0.0	0.0	0.0	7.7	66.3	71.9	20.1	99.6	182.2	85.5	85.5	2.0	0.0	0.0	2.6	1.3	0.7	627
14	0.7	11.9	0.0	0.7	2.0	0.0	0.0	0.0	0.0	0.0	0.7	1.3	8.4	27.7	61.9	10.6	4.2	3.5	8.4	14.4	3.5	2.0	0.0	0.0	162
15	1.3	0.7	0.0	0.7	1.3	0.0	1.3	0.0	0.0	1.3	0.7	2.0	42.7	39.9	30.6	17.2	10.2	0.7	11.3	0.7	1.3	1.3	1.3	2.0	168
16	0.0	0.0	1.3	7.1	0.7	1.3	0.0	0.7	34.2	92.1	13.7	3.5	0.0	0.0	0.0	0.0	0.0	0.7	1.3	6.1	0.0	0.0	0.0	0.0	163
17	0.0	0.0	0.0	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.3	24.8	25.9	29.5	12.6	9.0	0.0	16.6	8.4	0.0	0.0	0.0	0.0	129
18	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	11.9	23.0	23.5	20.1	9.0	15.9	23.0	27.7	14.1	2.6	9.7	2.0	1.3	1.3	186
19	2.0	0.7	0.0	1.3	0.0	0.0	0.0	7.7	5.5	7.7	3.3	12.6	69.3	134.7	80.4	68.5	83.2	3.5	5.5	6.8	9.0	0.7	0.0	0.7	503
20	0.7	0.7	0.7	0.0	5.5	2.0	0.0	2.0	0.0	0.0	2.0	12.6	79.8	38.0	66.3	49.3	3.5	1.3	0.0	1.3	1.3	3.3	1.3	0.7	272
21	1.3	4.8	0.0	1.3	2.0	0.0	0.7	1.3	3.5	0.0	0.0	8.9	23.0	8.4	7.1	1.3	0.0	0.0	0.7	0.7	0.0	4.2	0.7	4.8	74
22	9.5	31.5	18.8	21.3	8.4	8.4	9.5	4.8	12.4	1.3	7.1	2.0	11.3	5.5	0.7	51.1	18.1	10.2	2.6	7.7	0.0	4.2	1.3	4.8	252
23	0.7	0.0	3.5	4.2	1.3	0.0	0.0	0.0	0.7	4.8	12.4	7.7	0.0	1.3	4.8	17.1	7.1	30.5	4.2	1.3	0.0	0.0	7.1	0.7	109
24	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.2	18.3	14.8	9.0	0.0	0.0	6.1	3.3	0.0	0.7	0.0	0.0	56
25	0.0	1.3	0.0	0.0	0.0	1.3	0.0	0.0	0.0	0.7	39.9	25.9	39.9	6.1	10.2	30.5	8.4	0.0	7.1	9.5	8.2	4.2	0.0	0.0	193
26	0.0	0.0	0.0	0.0	0.7	0.0	0.0	0.0	0.0	0.0	1.3	37.1	6.8	37.1	28.8	24.8	35.1	83.6	58.7	0.7	0.7	0.0	0.7	0.0	316
27	0.0	0.0	0.7	0.0	1.3	0.0	0.0	0.0	0.0	0.0	31.7	45.6	79.8	79.8	42.7	112.2	110.9	32.4	1.3	1.3	1.3	0.0	0.0	1.3	542
28	2.0	5.5	1.3	0.0	0.7	1.3	1.3	0.0	0.0	0.0	0.0	2.6	2.0	3.9	24.8	23.0	0.0	1.3	15.4	6.1	0.0	0.7	0.0	0.0	92
29	1.3	0.0	0.0	0.0	0.0	0.7	0.0	0.0	0.0	0.0	0.0	2.6	9.0	50.3	39.9	39.9	12.4	0.7	12.6	0.7	4.8	8.2	2.0	4.2	189
KWh	32	64	33	46	41	20	23	44	73	113	148	304	633	720	878	824	536	363	221	114	61	56	30	29	5407

Bag	h	Mai	rch 20	08							Wind	Pow	er O	utput	of Bo	nus 6	00/44	Turbir	ne (Mo	onth's	Sumr	nary)			
Dt./Hrs	0	1	2	З	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	9.5	12.4	14.4	17.2	0.7	4.8	0.7	7.1	0.0	0.0	0.0	3.3	3.3	23.0	23.0	18.3	2.6	11.9	14.4	3.3	5.5	0.7	2.0	0.0	178
2	0.7	0.0	0.0	0.0	0.0	0.7	0.7	0.0	0.0	0.0	0.7	2.6	4.8	45.3	45.6	9.0	0.0	0.0	2.0	6.1	11.9	0.7	0.0	0.0	131
3	0.0	0.0	0.0	4.8	0.0	1.3	0.0	0.0	0.0	0.0	2.0	5.5	6.8	23.0	2.0	7.7	61.7	2.0	0.7	2.6	0.0	1.3	0.0	0.0	121
4	0.0	1.3	18.7	4.8	2.0	1.3	0.0	7.1	0.0	4.8	0.7	0.7	0.0	27.7	8.9	3.5	8.9	4.2	0.0	2.6	1.3	0.7	0.0	0.0	99
5	0.0	0.7	1.3	1.3	0.0	0.7	0.0	0.0	0.0	0.0	0.0	4.2	12.6	20.1	39.9	23.0	1.3	0.0	0.0	0.7	0.0	0.0	0.0	0.7	106
6	0.0	0.0	2.6	0.0	1.3	0.7	0.0	0.0	0.0	0.0	0.0	9.0	8.4	42.1	48.7	19.5	4.2	0.0	0.0	0.0	0.0	1.3	0.0	0.0	138
7	0.0	0.0	0.0	0.0	0.7	1.3	4.8	0.7	0.7	0.7	13.1	8.4	7.7	11.9	26.0	2.6	1.3	0.0	0.7	4.2	34.8	89.6	8.9	0.7	218
8	8.4	192.0	204.5	8.9	0.7	0.0	1.3	1.3	0.7	11.9	32.4	44.6	11.3	5.5	18.3	24.8	2.6	0.0	2.6	24.8	4.2	1.3	0.7	0.0	602
9	5.5	1.3	0.0	0.0	0.0	0.0	0.0	1.3	0.0	0.0	0.7	18.3	38.0	39.9	51.2	17.2	39.8	36.2	13.1	1.3	1.3	0.0	2.0	0.0	267
10	0.7	0.0	0.7	0.0	0.7	0.7	0.0	0.0	0.0	0.0	0.0	8.4	44.6	50.3	18.3	6.1	2.6	0.7	20.1	2.0	0.0	0.0	0.7	2.0	158
11	1.3	0.0	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	12.6	6.8	35.3	32.4	36.2	23.0	48.4	122.8	14.4	26.9	0.0	0.0	0.0	0.0	362
12	0.0	0.0	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.6	25.9	21.2	27.7	21.2	2.6	0.0	13.1	9.7	6.1	0.0	0.0	3.9	135
13	1.3	0.0	0.0	1.3	0.7	0.0	0.0	0.0	0.0	0.0	15.4	15.4	50.3	45.6	35.3	22.7	11.8	0.0	4.8	14.8	3.9	6.1	1.3	0.0	231
14	0.0	0.7	0.0	0.0	1.3	0.7	0.0	0.0	0.0	0.7	11.9	63.8	66.3	60.6	74.2	97.4	101.3	56.3	1.3	8.4	0.7	3.5	0.0	0.0	549
15	0.0	0.7	1.3	1.3	0.0	6.1	0.0	0.0	0.0	0.0	1.3	29.5	61.6	74.2	79.8	77.6	25.9	0.0	11.3	2.6	2.0	0.0	2.0	0.0	377
16	0.0	2.6	2.0	1.3	0.0	6.8	0.0	0.0	0.0	0.0	1.3	17.2	40.9	50.3	34.5	29.8	27.7	7.7	0.7	3.9	5.5	2.6	0.0	0.7	235
17	0.7	1.3	0.7	4.2	21.3	0.0	10.6	8.2	3.5	0.7	0.0	1.3	23.5	39.9	54.5	118.8	85.5	4.2	0.0	97.5	83.4	169.3	127.6	9.0	866
18	0.0	2.0	2.6	0.7	0.7	6.1	4.8	0.7	2.0	4.2	0.0	4.8	25.9	30.6	45.6	234.4	33.3	73.8	3.5	15.3	9.5	107.5	132.0	177.8	918
19	191.4	204.5	8.9	1.3	7.7	17.2	38.2	79.5	118.8	118.8	101.3	57.8	38.0	42.4	215.4	71.4	43.4	81.2	230.8	174.4	346.5	178.2	267.7	112.5	2747
20	0.7	0.7	0.7	0.0	0.7	0.7	0.0	0.0	0.7	21.9	25.9	14.8	1.3	5.5	46.1	137.0	4.2	0.0	13.7	31.7	1.3	0.0	0.7	0.0	308
21	0.0	0.0	0.0	0.0	0.0	0.0	4.2	0.0	0.0	0.0	0.0	2.6	4.2	21.9	39.0	14.8	8.4	0.0	9.0	0.0	0.7	0.0	0.0	1.3	106
22	0.0	0.0	3.3	0.0	1.3	0.0	4.8	0.0	0.7	1.3	1.3	31.3	51.1	7.7	18.4	29.8	86.3	15.4	2.0	2.6	0.0	0.7	4.8	0.0	263
23	0.7	2.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.5	35.3	39.9	27.7	1.3	24.2	8.4	18.1	11.3	13.1	11.9	3.5	1.3	4.8	0.0	207
24	0.7	1.3	0.7	0.0	0.0	0.0	0.0	0.0	0.0	15.4	5.5	11.3	3.5	20.1	26.6	29.5	17.2	0.0	4.8	14.8	2.0	0.0	0.0	0.0	153
25	0.7	2.6	2.0	0.7	2.6	0.0	0.0	0.0	0.0	0.7	3.3	21.3	51.2	51.2	36.2	8.4	0.7	3.3	7.7	9.7	2.0	0.0	2.6	0.0	207
26	2.6	0.7	0.0	2.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	18.7	37.1	38.0	1.3	23.5	50.3	130.7	93.4	26.3	0.0	0.0	0.0	0.0	425
27	2.0	0.7	0.0	0.0	0.7	0.0	0.7	0.0	0.0	0.0	2.0	26.3	50.0	71.8	54.0	153.2	14.4	5.5	144.4	70.7	0.0	0.0	0.0	0.0	596
28	2.0	0.0	1.3	0.0	2.6	0.7	0.0	0.0	0.0	4.8	18.3	35.3	45.6	6.1	4.2	43.9	13.1	0.7	21.6	0.7	6.1	0.7	1.3	2.6	211
29	2.6	0.0	6.1	0.0	0.0	2.6	0.0	0.0	0.0	0.0	2.0	32.4	21.2	18.3	14.8	14.4	20.6	0.0	4.2	7.7	0.7	2.0	0.0	0.7	150
30	1.3	0.0	0.7	2.0	0.7	2.0	0.7	0.7	0.7	1.3	0.0	0.0	24.8	45.6	40.9	14.4	5.5	0.0	0.0	9.7	6.1	4.8	0.0	0.7	162
31	1.3	480.4	90.2	2.0	14.5	0.0	0.7	0.0	0.0	2.0	43.7	17.7	66.3	42.7	53.5	88.7	53.1	335.4	491.2	42.4	1.3	0.7	1.3	0.0	1829
KWh	234	907	364	55	61	54	72	106	128	193	331	556	889	1016	1244	1394	796	903	1138	629	540	573	560	312	13054

Bag	h	Α	pril 20	800							Wir	nd Po	wer O	utput	of Bo	onus	600/4	44 Tur	bine (l	Month	's Sun	nmary))		
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	1.3	4.2	0.7	7.7	12.4	16.6	4.2	0.0	0.0	0.0	0.0	12.6	36.2	61.6	37.1	37.1	61.6	0.7	4.2	18.8	5.5	0.7	0.7	0.0	323
2	0.7	4.2	6.1	7.1	2.6	1.3	8.9	22.2	2.0	3.5	0.0	2.6	0.0	0.7	0.0	0.0	1.3	0.0	0.0	2.0	1.3	3.5	0.0	0.0	70
3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.2	0.7	7.7	14.5	101.3	20.6	50.3	0.7	0.0	0.0	0.0	0.0	0.0	2.0	0.0	202
4	0.0	0.0	0.0	0.0	1.3	0.0	0.0	0.0	0.0	0.0	0.7	80.6	47.4	7.1	6.1	9.7	8.4	1.3	0.0	0.0	1.3	0.7	0.0	1.3	166
5	0.0	0.0	0.7	0.7	0.7	0.0	0.7	0.0	0.0	0.0	0.0	0.7	0.0	0.0	0.0	0.0	0.0	18.8	13.9	1.3	0.0	13.1	1.3	0.7	52
6	0.0	0.0	0.0	0.0	0.0	0.7	0.0	1.3	0.0	1.3	4.2	3.9	0.7	0.7	0.0	0.0	0.0	0.0	0.7	1.3	0.0	1.3	0.7	4.8	21
7	0.7	5.5	0.0	0.7	0.0	0.0	0.7	0.0	0.0	0.0	0.0	0.7	0.0	0.0	1.3	6.1	0.7	0.0	0.0	0.7	1.3	0.7	2.6	0.0	21
8	0.0	0.0	6.1	0.0	20.9	4.2	1.3	0.0	0.0	0.7	0.0	8.4	23.0	51.2	20.1	11.9	0.0	2.0	0.7	0.7	2.0	1.3	1.3	2.6	158
9	0.0	0.0	1.3	0.7	0.0	1.3	0.0	0.0	0.7	0.7	31.7	12.6	0.7	0.0	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.7	0.0	51
10	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	0.0	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.3	0.7	1.3	4.8	0.7	10
11	0.0	2.0	1.3	3.5	0.0	0.0	0.0	1.3	0.0	0.0	26.9	43.7	6.1	61.6	27.7	1.3	7.1	17.1	24.8	12.4	2.0	0.7	0.0	0.0	239
12	0.0	0.0	0.0	0.0	0.7	0.7	2.0	0.0	0.0	1.3	22.9	45.6	17.2	26.9	34.2	36.1	2.0	46.6	0.0	1.3	0.7	0.7	8.4	0.7	248
13	2.0	1.3	0.0	1.3	0.0	0.0	0.0	0.0	0.0	1.3	0.0	20.1	30.6	3.9	3.3	21.2	15.3	0.0	9.0	9.0	9.7	4.2	0.7	1.3	134
14	0.7	0.7	0.0	2.6	0.7	4.2	12.4	0.0	0.0	0.7	6.8	45.5	8.9	67.2	31.7	4.2	15.9	34.8	1.3	19.4	1.3	0.0	0.0	3.5	262
15	0.7	0.7	0.0	0.0	0.7	0.0	12.4	4.2	3.5	37.9	0.0	0.7	29.0	2.0	7.1	1.3	3.3	37.9	122.4	40.1	16.5	0.7	0.0	0.0	321
16	0.0	1.3	0.7	4.8	4.2	0.0	0.0	0.0	0.0	22.7	66.3	14.8	55.9	22.9	48.2	6.1	2.0	1.3	0.0	0.0	1.3	0.7	0.0	1.3	254
17	0.7	1.3	1.3	1.3	1.3	0.0	0.7	0.0	0.0	0.0	2.0	0.0	1.3	9.0	11.9	14.4	11.9	0.0	11.3	1.3	0.0	0.7	0.7	18.3	89
18	2.0	0.7	0.7	0.7	0.0	0.7	0.0	0.0	0.0	0.0	2.6	6.1	35.3	21.2	24.2	24.8	2.0	6.1	12.6	25.9	5.5	1.3	0.7	3.3	176
19	1.3	0.7	0.0	2.0	0.0	0.7	0.0	0.7	0.0	0.0	0.0	14.8	14.8	40.9	46.6	13.1	2.0	0.7	5.5	2.6	2.0	0.0	0.0	0.0	148
20	0.0	0.0	0.7	0.7	0.0	0.0	0.7	0.0	0.0	0.0	12.4	34.2	50.3	29.8	42.7	50.3	24.8	0.7	14.1	23.0	3.9	0.7	2.0	1.3	292
21	1.3	4.8	0.7	1.3	0.7	1.3	0.0	1.3	0.0	0.7	2.0	2.0	27.0	61.6	27.7	38.0	51.2	0.7	9.5	72.7	191.4	50.3	8.4	0.0	554
22	0.0	0.0	1.3	2.0	0.7	9.7	7.1	0.7	0.0	0.0	0.7	2.6	45.6	4.8	11.9	11.9	50.8	48.4	9.7	9.7	2.0	0.7	2.0	2.0	224
23	2.0	0.0	2.6	5.5	11.3	1.3	0.0	0.0	0.0	0.0	0.0	1.3	13.1	22.4	22.4	8.2	4.8	1.3	0.0	23.0	12.6	0.7	2.6	0.7	135
24	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.3	9.7	6.1	39.9	26.6	34.2	34.5	0.0	0.0	19.4	56.3	9.5	12.6	0.0	3.3	254
25	0.7	0.0	0.7	2.6	0.7	0.7	0.7	0.7	0.0	0.0	0.0	16.6	48.4	16.6	56.3	38.0	16.6	72.3	176.8	121.6	38.2	0.7	4.8	0.7	614
26	9.0	9.5	67.6	4.2	0.7	1.3	1.3	2.0	34.8	0.0	15.9	0.0	11.9	48.7	44.6	60.6	12.6	79.5	83.1	61.9	55.0	109.2	154.0	307.9	1175
27	179.5	95.7	159.7	170.3	119.4	1.3	4.2	2.6	0.0	6.8	5.5	56.9	196.6	173.1	83.1	55.9	31.5	0.0	0.7	15.4	3.3	4.8	0.7	2.6	1369
28	0.7	0.7	2.0	0.0	0.0	1.3	1.3	0.0	0.0	0.0	7.1	18.3	39.9	32.4	29.2	71.9	67.0	125.6	130.6	42.7	0.0	0.7	9.7	0.7	581
29	8.4	0.7	0.0	2.6	2.0	0.0	1.3	0.0	0.0	0.7	0.0	10.2	71.9	77.4	97.4	95.7	38.0	4.8	0.7	4.2	9.0	3.3	0.7	1.3	430
30	0.0	0.0	0.0	0.0	0.0	0.0	2.0	0.0	0.0	0.0	0.0	20.0	71.9	55.9	75.1	64.8	9.5	208.6	76.2	34.2	0.7	0.0	2.0	18.1	639
KWh	212	134	254	222	181	47	61	37	42	84	218	489	938	1027	845	768	441	709	727	603	376	215	211	377	9214