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AN INVESTIGATION OF
WIND POWER POTENTIAL AT
RANGLA - AJK

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(Project is financed by Ministry of Science & Technology)

Executive Summary

Pakistan Meteorological Department (PMD) conducted a wind power potential survey of the northern areas of Pakistan. Funding for this project was provided by the Ministry of Science & Technology. Under this wind data was collected at 42 sites along the Northern parts of the Country.

In this report the analysis based on one year wind data has been presented along with the wind generated electric power at Rangla, AJK. Wind data with ten minute average speed and direction were collected at 10 meters and 30 meters height and 50 meters values were computed from models.

At 50 meters we have the annual average wind speed of 3.62 m/s during twelve months May-2007 to April-2008 the highest of 4.3 is observed in May 07. Seasonal Diurnal Wind variation indicates that maximum wind speed is available in the Day through-out the year. Wind frequency distribution shows that during 15.3% of the time wind speed is 5 m/s or above.

Sometimes simply wind speed averages do not give the true picture of the wind power optional of an area. For the purpose it is common to assign areas to one of the seven wind classes based on "wind power density" of the area. Monthly and annual wind power density has been computed and added in the report. The annual power density of Rangla is 65.73 w/m² according to international wind classification, this power density categorize Rangla as a below marginal site for wind power generation. Though monthly power density values indicates that the power density is blow marginal category but this is compensated by very high values during summer months especially in June and July.

Wind generated electric power has as also been computed on hypothetical 600Kw wind turbine and its hourly, monthly and annual values has been added in this report. The annual power production form a single 600kw wind turbine come out to 332,976 kWh which shows the capacity factor of 6% for Rangla. Internationally it is accepted that if any site has a capacity factor of 25% and above than that site is suitable for installation of economically viable wind power farms. As such Rangla and surrounding areas can be classified as no suitable site for installing big economically viable wind farms.

1. **Introduction:**

Wind energy is the fastest growing renewable energy source today. A continued interest in wind energy development worldwide has produced steady improvements in technology and performance of wind power plants. New wind power projects have proven that wind energy not only is cost competitive but also offers additional benefits to the economy and the environment.

A steady supply of reasonably strong wind is necessary requirement for utilizing the power in the wind. Development of wind energy depends upon a clear understanding of wind resources. Site location, turbine performance and physical effects of turbulence and energy extraction represent a few of the issues that must be addressed by anyone interested in developing wind energy.

As such any plan to develop wind energy must begin by understanding the wind resource. Where are the best potential wind sites located? How much energy could be extracted from the wind at those sites?

1.1 Characteristic of wind:

The global winds are caused by pressure differential across the earth's surface. The amount of solar radiation absorbed at the earth's surface is greater at the equator than at the poles. This variation in incoming heat sets up convective cells in the lowest layer of the atmosphere. In the simplest form air rises at the equator and sinks at the poles. However the rotation of the earth complicates this simple heat transfer. A series of circulations are set up in both northern and southern hemispheres.

The areas of the globe where air is descending are zones of high pressure and where the air is ascending, low-pressure zones are formed. The pressure gradient drives the flow of air from high to low pressure, thus causing the wind. The wind is then acted on the corriolis force due to the earth's rotation. The resultant wind is turned easterly or westerly. On a smaller scale, wind is created because of temperature difference between land and sea and mountains and valleys. The local topographical features and roughness of the terrain also cause air movements.

2.0 <u>Wind Mapping Project of Pakistan Meteorological Department:</u>

As any plan to develop wind energy must begin by understanding the wind resources. Where are the best potential wind sites located? How much energy could be extracted from the wind at those sites? Will the wind turbine performance be affected by the turbulence or other wind resource characteristics?

To answer these questions and to provide wind resource database for the different potential parts of the country, Pakistan Meteorological Department prepared a phased programme. Government of Pakistan, Ministry of Science and Technology provided the necessary funding for undertaking the Phase II. Second phase covers the Northern areas of Pakistan.

2.1 Study Area:

The project area for the wind mapping Phase-II covers the Northern areas of Pakistan including Districts are Swat, Dir, Chitral, Gilgit, Skardu, Haripur, Shangla, Buneer, Nowshara, Peshawar, Mohmad Agency, Khyber Agency and Azad Kashmir.

Forty-Two stations for collecting wind data have been installed to study the wind regime as shown in Map-1. The list of stations is given below:

Fatehpur, Bahrain, Kalam, Khawazakhaila, Malamjabba, Tahash, Khungipayan, Dir, Tarbella, Nizampur, Warsak, Chitral City, Drosh, Mirkhani, Shagore, Garam Chasma, Khagozi, Reshan, Mastuj, Kalash, Ayune, Astore, Bunji, Chillas, Gilgit, Gupis, Sost, Passu, Aliabad, Shigar, Barapayan, Sermik, Lowaramaina, Ramatkore, ShahidaSir, Danakool, Rangla, Moorti Pahari, Rangla, Pedar, Lempiapatian, Dargaye.

Rangla is situated in Dhir Kot, AJK. Latitude & Longitude of Rangla is: *Latitude = 34.02°, Longitude = 73.38°, Elevation = 6290ft.*

2.2 **Data source:**

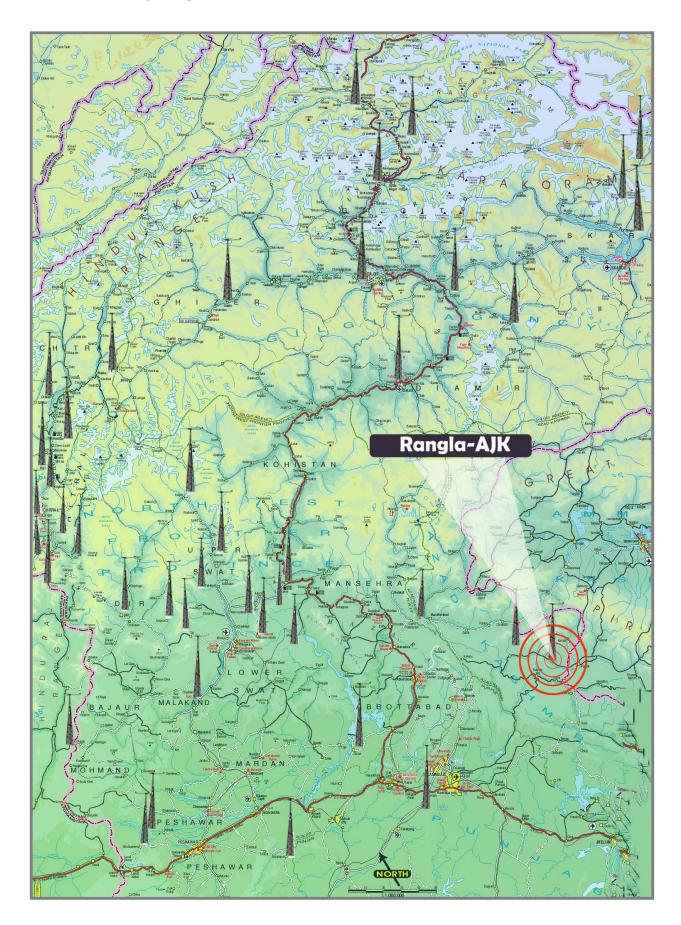
To undertake this study 30-meter high towers are erected at the locations mentioned above. On each of these high towers two wind speed anemometers are installed at the height of 10 meters and 30 meters, respectively; wind vane for recording wind direction is installed at 30 meters height. NRG automatic data loggers have been installed to record data at each site. These data loggers are recording, ten-minute average wind speed at both level, ten-minute average wind direction, and 10-minute average minimum and maximum wind speed. While selecting the above-mentioned locations for wind monitoring; the main objective was to identify potentially windy areas that also possess other desirable qualities of wind energy developed site. Further following guidelines as far as possible were also kept in mind while choosing an exact location for monitoring towers.

- Towers are placed as for as possible away from the local obstruction to the wind
- Selected location should be representative of the majority of the site.

Since sating a tower near obstructions such as trees or building can adversely affect the analysis of the site's wind characteristics such as magnitude of wind resource, wind shear and turbulence levels the tower in most cases are placed as for as possible away from local obstructions to the wind. But where this rule could not be followed, the tower was placed at horizontal distance of 10 times the height of the obstruction in the prevailing wind direction as required internationally. The following parameters have been recorded during the study.

- i. Wind speed ten minute average at 10 & 30 meters
- ii. Maximum wind speeds during 10 minutes
- iii. Minimum wind speeds during 10 minutes
- iv. Wind direction ten minutes average at 30 meters

Every month a team of observers and Maintenance Engineers visit site to inspect the instruments and to download the data on a laptop. Finally, the data is compiled and analyzed at Renewable Energy Research Cell established at Meteorological Department Islamabad.



Map-1: Shows 42-Towers Installed in Wind Mapping Project in Northern Areas

3.0 Methodology; Analysis & Discussion:

3.1 Wind speed variation with height:

Wind speed tends to increase with height in most locations, a phenomenon known as wind shear. The degree of wind shear depends mainly upon on two factors, atmospheric mixing and the roughness of the terrain.

Atmospheric mixing typically follows a daily cycle driven by solar heating. At the hub height of a wind turbine, this cycle often causes wind speeds to increase in the daytime and decrease at night. However, the range of variation between night and day typically diminishes as hub height increases. At a height of approximately 50 meters, it weakens or may even disappear in some cases.

Terrain roughness also affects wind shear by determining how much the wind is slowed near the ground. In areas with a high degree of roughness, such as forests or cities, near- surface wind speeds tend to be low and wind shear high, whereas the converse is true in areas of low roughness such as flat, open fields. Wind shear may be greatly reduced or eliminated where there is an abrupt change in terrain height such as a sea cliff or mountain ridge.

To save money wind measurements sometimes are taken at a lower height than the wind turbine tower. In that case, it is essential to measure wind shear at different times of day in different seasons to accurately predict the performance of a wind power plant. The shear can be measured by monitoring wind speeds at two or three heights on a tower. Since wind turbines produce much more power in stronger winds, wind turbine designers try to put turbines on the tallest possible towers. At some point, however, the increased cost of towers outweighs the benefits. With current wind turbine technology, the optimum tower height for large wind machines appears to be approximately 40 to 50 meters.

For saving money in this survey also the wind has been recorded at 10 & 30 meters and for calculating the wind speed at 50 meters the following two methods has been used in this study.

3.1.1 *Log Law:*

The turbulent mixing in the atmosphere may be considered in a similar way to molecular mixing (this is called k theory). Assuming the mixing is dominated by mechanical mixing due to shear forces a relationship of wind speed with height is derived.

$$u = \frac{u_*}{k} \ln \left(\frac{z - D}{z_o} \right)$$

Where

 U_* is the friction notify

k is the von Karman constant

 $\mathbf{Z}_{\mathbf{0}}$ is the roughness length

D is the displacement height

The von Karman constant is generally taken as 0.4. The roughness length Z_0 is related to the vegetation cover of the area. The values of roughness length are given in Table-1. The displacement height D is the height above the roughness elements where the flow is free. For most vegetation it is small and is generally treated as zero. For large roughness elements like trees and building in towns it is not negligible and is the order of the average height of the elements. The <u>log law</u> may only be used for heights above D. Turbines are rarely sited in forests or towns, so D is usually taken as zero.

The wind speed at any height z can then be computed provided that the wind speed at a height Z_R is known. Thus:

$$\frac{u}{u_R} = \frac{\ln \left(\frac{z}{z_o} \right)}{\ln \left(\frac{z}{z_o} \right)}$$

Where

 U_R is the wind speed at reference height Z_R

The reference height is usually 10m or 30m as this is the height at which mean wind data is generally collected.

3.1.2 *Power Law:*

Engineers often prefer to use a <u>Power Law</u> to describe the increase in wind speed with height, as it is easier to evaluate.

$$\frac{u}{u_R} = \left(\frac{z - D}{z_R}\right)^{\alpha}$$

Where:

 α is the power law exponent

 U_R is the wind speed at reference height Z_R

The power law exponent typically varies between 0.1 and 0.32 depending upon the landscape type. A value of 1/7 is often quoted as a reasonable value for the power law exponent in countryside. The exponent can be calculated from the roughness length.

$$\alpha = \frac{\ln \left(\ln \left(\frac{z}{z_o} \right) \right)}{\ln \left(\frac{z}{z_R} \right)} \approx \frac{1}{\ln \sqrt{\frac{z \cdot z_R}{z_o}}}$$

Where: Z is the measurement height

Z_R is the reference height

 Z_0 is the roughness length

The power law exponent therefore varies with the interval between the two measurement heights. The power law should be carefully employed since it is not a physical representation of the surface layer and does not describe the flow nearest to the ground very well. Both the log law and the power law are simplified expressions of the <u>wind profile</u>. They are valid in flat homogeneous terrain. So they do not include the effects of topography, obstacles or changes in roughness or stability.

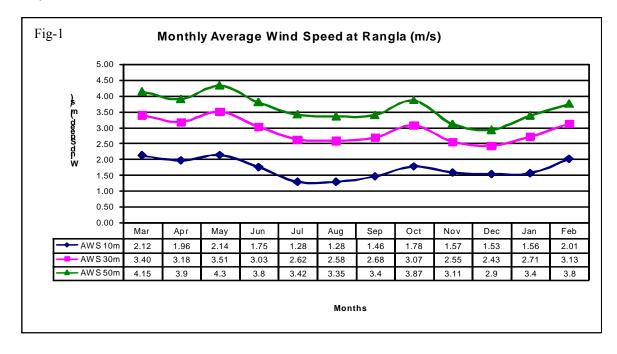
Table 1: Typical values of surface roughness length Z_0 and power law exponent α for various types of terrain

Type of terrain	Z_0	α
Mud Flats, Ice	10 ⁻⁵ to 3x 10 ⁻⁵	
Calm Sea	$2x10^{-4}$ to $3x10^{-4}$	
Sand	$2x10^{-4}$ to 10^{-3}	0.01
Mown Grass	0.001 to 0.01	
Low Grass	0.01 to 0.04	0.13
Fallow Field	0.02 to 0.03	
High Grass	0.04 to 0.1	0.19
Forest and Woodland	0.1 to 1	
Built up area, Suburb	1 to 2	0.32
City	1 to 4	

3.2 Average Wind Speed:

By using above mentioned methods the wind speed at 50 meters has been computed and monthly average of these wind speed at 50 meters height have been given in Fig 2 in graphical as well as tabular form.

Fig-1 shows monthly average wind speed at height of 10 meters, 30 meters and 50 meters from May 2007 to April 2008. At 30 meters height, we have the maximum average wind speed of 3.51 m/s during May, 2007. At 50 meters we have the annual average wind speed of 3.62 m/s from May-2007 to April 2008 and the highest average wind speed of 4.3 m/s is observed during May 2007.



3.3 **Diurnal Wind speed Variation:**

Fig-2 shows the annual diurnal wind speed variations at Rangla. The wind speed is generally equal during day and night time, it reaches maximum in evening which is around 3.72 m/s and 5.0 m/s at 30 meters and 50 meters height respectively.

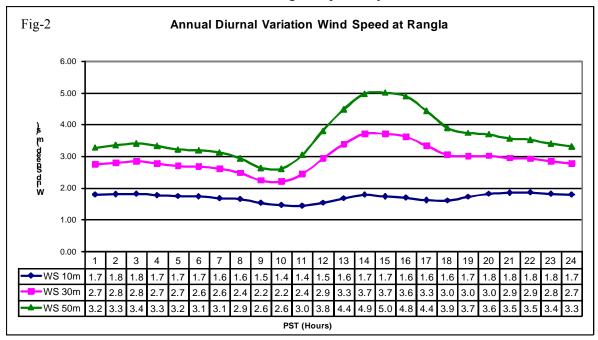
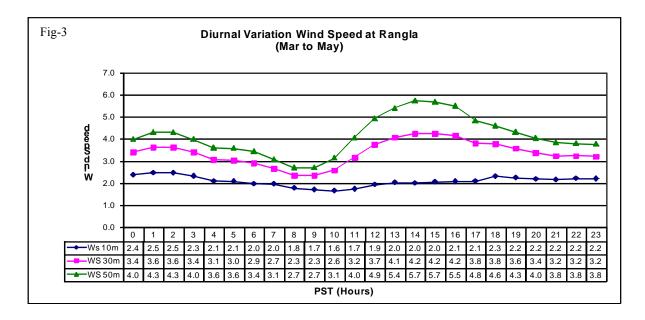
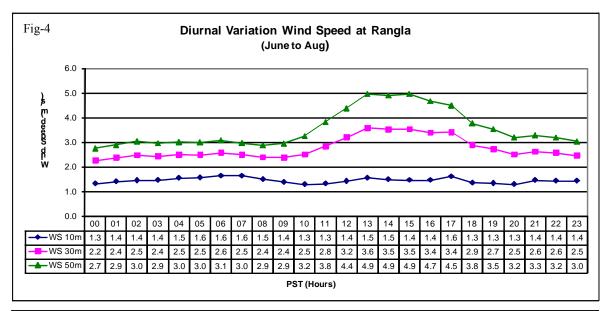
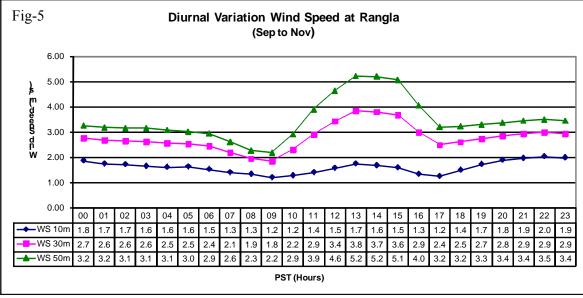
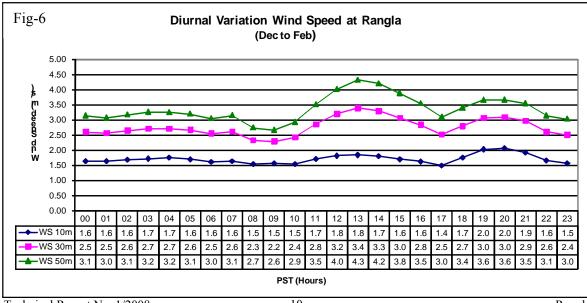


Fig-3, Fig-4, Fig-5 and Fig-6 shows the seasonal diurnal wind speed variations at Rangla for (Mar-May), (Jun-Aug), (Sep-Nov) and (Dec-Feb) respectively. Seasonal wind speed is generally higher during daytime and low during night in Rangla.









3.4 Wind speed Frequency Distribution:

Wind speed frequency distribution can simply be obtained by plotting the different wind speeds against their frequencies / relative frequencies. For obtaining frequency distribution the following two procedures are necessary.

3.4.1 **Binning of Data:**

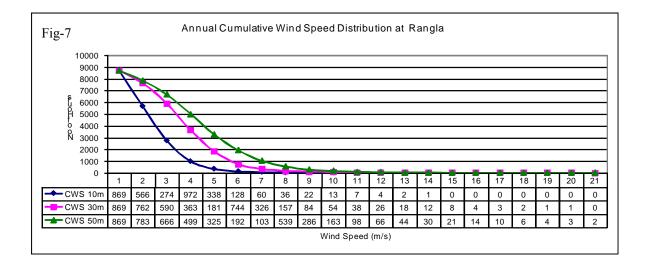
The sorting of the data into narrow wind speed bands is called binning of the data. In our case a bin width of 1m/sec has been used e.g. a measured wind speed of 3.5 m/sec would be placed in 3<X<=4 m/sec bin. The central value of each bin i.e. 0.5 m/sec, 1.5 m/sec etc has been used in calculations and frequency distribution group.

3.4.2 Relative Frequency:

It is proportional wind speed in each bin. It can be viewed as the estimate of probability of given wind speed in the bin. Relative frequency is defined as

R.F = probability P (Vi) = Frequency of given wind speed / Total period 3.4.3 *Annual Cumulative Wind Frequency:*

Fig-7 shows the Annual Cumulative Wind Frequency distribution at three heights 10, 30 and 50 meters. The analysis indicate that in a year at a height of 30 meters during 181 hours the wind speed is greater than equal to 5 m/s whereas at 50 meters, during one year 325 hours the wind speed is equal or greater than 5m/s.



3.4.4 Wind Frequency Distribution:

Fig-8 shows the Annual wind frequency distribution at Rangla. We can see that at 50 meters during 892 hours wind speed is 5 m/s, 494 hours speed is 6 m/s, 253 hours speed is 7 m/s, 123 hours speed is 8 m/s and during 65 hours the wind speed is 9m/s and so on. This indicates wind potential in this area.

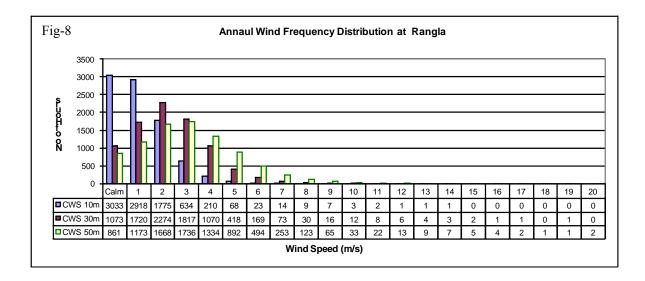
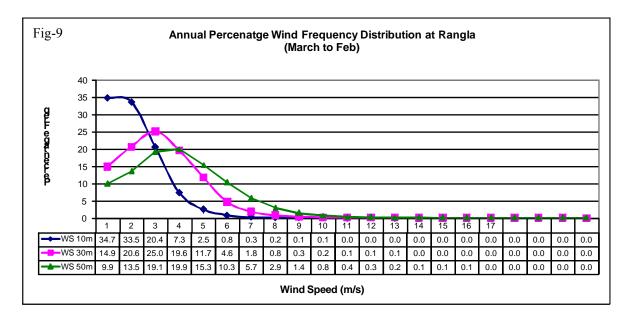


Fig-9 gives the frequency distribution in percentage. At 50 meters we find that during 15.3% of time wind is 5m/s, 10.3% of the time 6m/s and 5.7% of the time it is 7m/s. whereas at 30 meters height we get 11.7% of the time wind speed 5m/s, 4.6% of the times 6m/s and 1.8% of the time 7m/s.

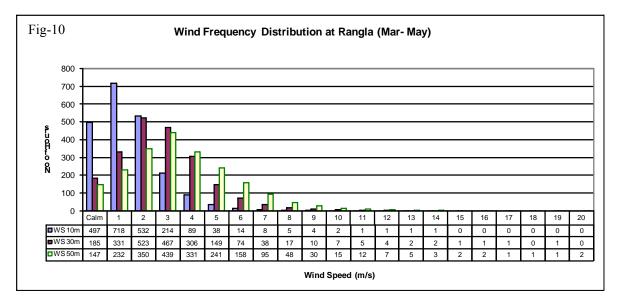


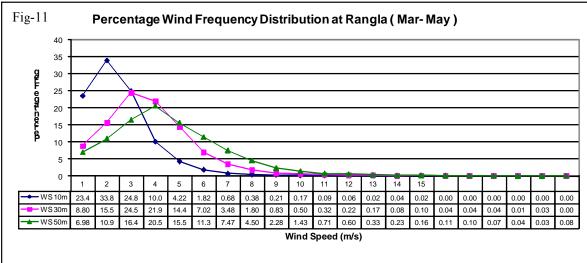
3.4.5 Seasonal Wind Frequency Distribution:

Figures 10–17 gives seasonal wind frequency distribution and percentage wind frequency distribution.

March-May

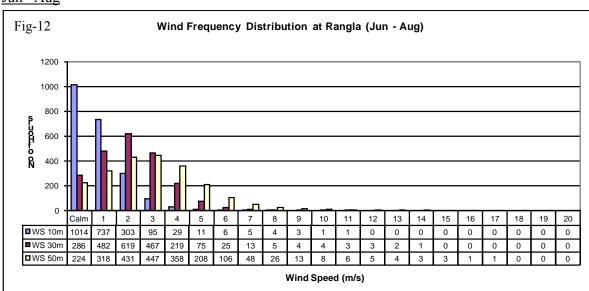
Fig-10 shows frequency distribution during the months of Mar to May. We can see that in this period at 30 meters height during 149 hours we get 5m/s, 74 hours 6m/s, 38 hours 7m/s. Similarly at 50 meters we get 241 hours 5m/s, 158 hours 6m/s, 95 hours 7m/s, 48 hours 8m/s, 30 hours 9m/s, 15 hours 10m/s.

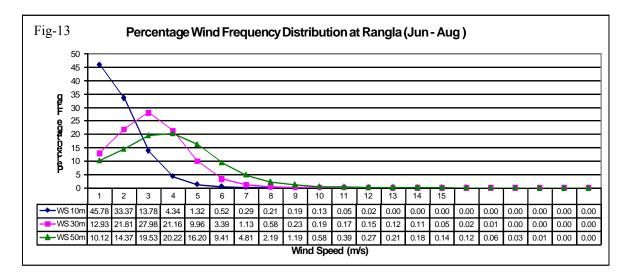




Similarly the above mentioned seasonal frequency distribution percentage terms have been presented in figure 11.

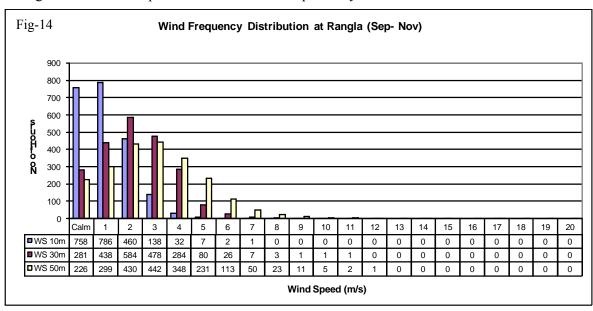
Jun-Aug

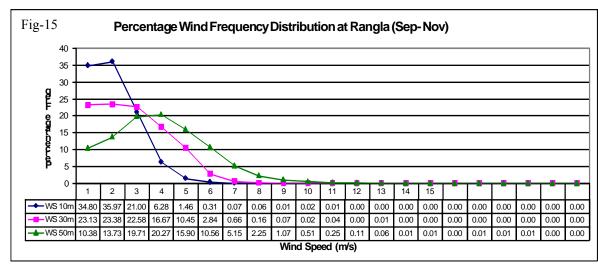




<u>September – November</u>

Fig-14 and 15 shows wind frequency distribution and percentage frequency distribution during the months of September to November respectively.



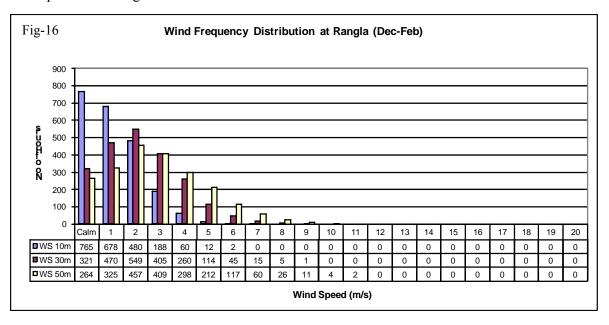


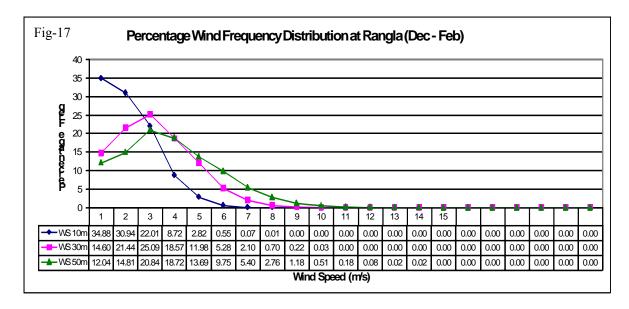
Dec – Feb

Fig-16 shows frequency distribution during the months of December to February. We can see that in this period at 30 meters height during 114 hours we get 5m/s, 45 hours 6m/s, 15 hours 7m/s.

Similarly at 50 meters we get 212 hours 5m/s, 117 hours 6m/s, 60 hours 7m/s, 26 hours 8m/s, 11 hours 9m/s.

Similarly the above mentioned seasonal frequency distribution percentage terms have been presented in figure 17.

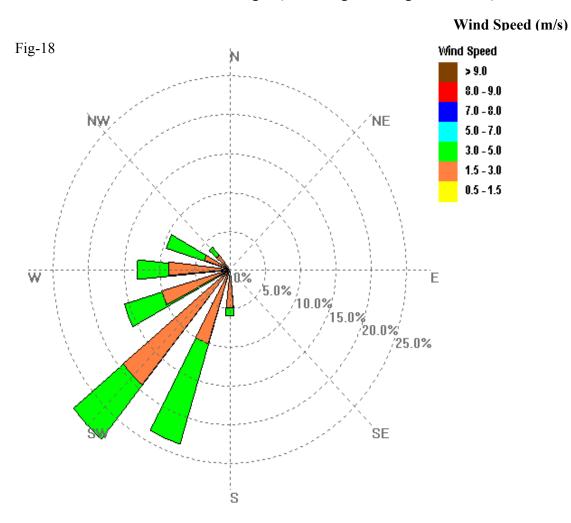




3.5 Wind Rose:

Fig-18 shows the Wind Rose Graph based on 12 months data from May 2007 – April 2008 collected at 30 meters height. Wind Rose indicates that most of the time the wind direction is West and South west. The average wind speed is 4.16 m/s and the percentage of wind speed greater than 5m/s is 19.2%.

Wind Rose at Rangla (30m height during 12 months)



Average Wind Speed	Wind greater than 5 m/s	Comments
4.16 m/s	19.2%	

3.6 Wind speed statistic:

3.6.1 The statistical Mean:

It is the average of a set of n numbers. Mathematically, we can write

$$M e a n = \frac{\left[\sum_{i=1}^{n} x_{i}\right]}{N}$$

The Mean Wind Speed V can be calculated by the formula.

$$V = \sum_{i=1}^{n} V_{i} P(V_{i})$$

Where Vi is the central wind speed of bin 1 and P(Vi) is the probability/relative frequency that the wind speed has in bin i.

3.6.2 Variance:

It is one of the several indices of variability that statistician, use to characterize the dispersion among the measures in a given set of data. Mathematically, variance is written as

Variance =
$$\sigma^2 = \sum (X_i - V)^2$$

Where V is mean of data set

In case of wind speed data, we can write it, as

$$\sigma^2 = \sum V_i^2 P(Vi) - (V)^2$$

3.6.3 Standard Deviation

It is the square root of the variance, denoted by σ

$$\sigma^2 = (\sigma)^{1/2} = \sum (V_i^2 P(V_i) - (V)^2)^{1/2}$$

3.7 Wind power density:

While investigating a wind power potential of an area, the average values of wind speed does not truly represent this potential because lot of information regarding frequency distribution of wind speed is suppressed in the process of averaging wind speed. As such the most important values for estimating the wind power potential of a given site is the value of the wind power density or the available theoretical instantaneous power from the wind. This available wind power in the wind is the flux of Kinetic Energy crossing the wind energy conversion system and its cross – sectional area.

Like water flowing in the river, wind contains energy that can be converted to electricity using wind turbines. The amount of electricity that wind turbines produce depends upon the amount of energy in the wind passing through the area swept by the wind turbines blades in a unit of time. This energy flow is referred to as the wind power density.

A key aspect of wind power density is its dependence on wind speed cubed. This means that the power contained in the wind increases very rapidly with wind speed; if the speed doubles, the power increases by a factor of eight. In practice, the relationship between the power output of a wind turbine and wind speed does not follow a cubic relationship. Below a certain minimum speed, the turbine does not have enough wind to operate, whereas above a certain speed its output levels off or begins to decline. In very high winds the turbine may even be shut down to prevent damage to it.

Wind power density also depends on air density. At higher attitudes, air density decreases and, as a result, so does the available power. This effect can reduce the power output of wind turbines on high mountains by as much as 40 percent compared to the power that could be produced at the same wind speeds at sea level. Air density depends inversely on temperature: colder temperatures are favorable for higher air densities and greater wind power production.

3.7.1 Wind power classes:

To simplify the characterization of the wind power potential, it is common to assign areas to one of seven wind classes, each representing arrange of wind power density at the special height above the ground. The standard International wind power classifications are shown in Table 2.

1 4	Dic-2. Internat	ionai wina i o	wei Ciassilicat	1011	
	России	30m I	Height	50m I	Height
Class	Resource Potential	Wind Speed	Wind Power	Wind Speed	Wind Power
	rotentiai	m/s	W/m ²	m/s	W/m ²
1		0 - 5.1	0 - 160	0 - 5.6	0 - 200
2	Marginal	5.1 – 5.9	160 - 240	5.6 - 6.4	200 - 300
3	Moderate	5.9 - 6.5	240 - 320	6.4 - 7.0	300 - 400
4	Good	6.5 - 7.0	320 - 400	7.0 - 7.5	400 - 500
5	Excellent	7.0 - 7.4	400 – 480	7.5 - 8.0	500 - 600
6		7.4 - 8.2	480 - 640	8.0 - 8.8	600 - 800
7		8 2 – 11 0	640 – 1600	88-119	800 - 2000

Table-2: International Wind Power Classification

By and large, the areas being developed today using large wind turbine are ranked as class 5 and above. Class 4 areas are also being considered for further development as wind turbines are adopted to run more efficiently a lower wind speeds. Class1 and class2 areas are not being deemed suitable for large machines, although a smaller wind turbine may be economical in areas where the value of the energy produced is higher

3.7.2 Power of wind Energy:

A parcel of Wind possesses kinetic energy

$$E = \frac{1}{2}mV^2$$

From this, power density is calculated as

$$P = \frac{e}{t} = \frac{1}{2} \frac{dm}{dt} V^2$$

Where $\frac{dm}{dt}$ is the mass of air following time.

From fluid dynamics, it can be proved that

$$dm/_{dt} = \varphi AV$$

Volume of cylindrical cross section can be written as

$$V = \pi r^2 L \qquad ---- \qquad (1)$$

Where r is radius of cylinder and L is length of it.

The wind moving with velocity V travels this distance L in time t so

$$S = L = Vt$$

So equation L takes the form

$$V = \pi r^2 V t$$

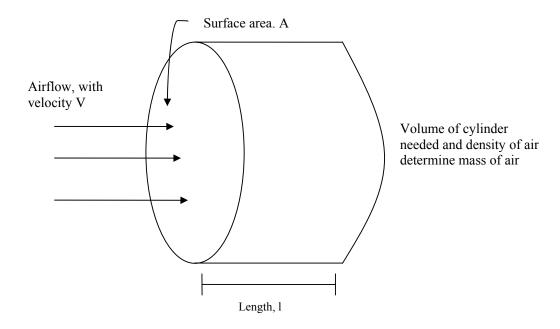
Now mass of wind can be written as

$$M = \varphi A v t$$

Differentiating

$$dm/_{dt} = \varphi AV d/_{dt(t)} = \varphi AV$$

Where φ is density of wind and others parameters have been defined in diagram.



So the power is then,

$$P = \frac{1}{2} \frac{dm}{dt} V^{2} = \frac{1}{2} \varphi AVT / t V^{2}$$
$$= \frac{1}{2} \varphi AV^{3}$$

And power density

$$P/A = 1/2 \varphi V^3$$

Density of wind at mean sea level is 1.225 kg/m³

At 15° C, The area depends upon the size of the rotor. Therefore, it is clear that power density chiefly depends on wind velocity and goes up as a cube of it.

3.7.3 Wind power calculation using Mean wind Speed:

Wind power calculated from Mean wind speed is not true representative of wind power. In real world, the wind varies constantly. Actual wind power density at most sites can rang from 1.0 to 3 times greater then that calculated. For example, we take wind speed of 5, 7 and 8 m/sec respectively the respective power densities are 76 wat/m², 210 watt/m² and 313 watt/m². The average of which is 200 watt/m². On the other hand, the average wind speed is 6.7 m/sec and power density of average wind is 181 watt/m². So the power of wind calculated by mean wind speed is less than the actual power present in wind i.e. Mean wind speed is not true representative for the wind power calculations.

To overcome this drawback we find some alternative arrangement, which reduces the deficit. The Weibull distribution is the best fit of wind data to calculate wind power based on mean wind speed and variance/standard deviation.

3.7.4 Weibull distribution:

The Weibull distribution (named after the Swedish physicist W. Weibull, who applied it when studying material strength in tension and fatigue in the 1930s) provides a close approximation to the probability laws of many natural phenomenons. It has been used to represent wind speed distribution for application in wind loads studies for sometime. In recent years most attention has been forced on this method for wind frequency applications not only due to its greater flexible and simplicity but also because it can give a good fit to experimental data.

The Weibull distribution function, which is a two-parameter function, has been found to fit much wind data with acceptable accuracy is expressed mathematically as

$$\phi(u) = \frac{k}{c} \left(\frac{u}{c}\right)^{k-1} \exp\left(-\left(\frac{u}{c}\right)^{k}\right)$$

Where:

u is the wind speed

c is the scale parameter with units of speed

k is the shape parameter and is dimensionless

When k = 2 the distribution reduces to Rayleigh distribution and if k=1 an exponential distribution is found. These are special cased of Weibull distribution.

Solving the equation, we find that the scale factor c is closely related to the mean wind speed for the site.

$$\overline{u} = c\tau \left(1 + \frac{1}{K}\right)$$

Where au is the complete gamma function

Similarly

$$\overline{u^n} = c^n \tau \left(1 + \frac{n}{k}\right)$$

And so

$$\overline{u^3} = c^3 \tau \left(1 + \frac{3}{k} \right)$$

The available power density is obtained:

$$E = \frac{1}{2}\varphi c^3 \tau \left(1 + \frac{3}{k}\right)$$

Where

E is the power density in watts / m^2

The shape factor k is related to the variance of the wind

$$\sigma^{2} = c2 \left[\left(1 + \frac{2}{k} \right) - \left(\tau \left(1 + \frac{1}{k} \right) \right)^{2} \right]$$

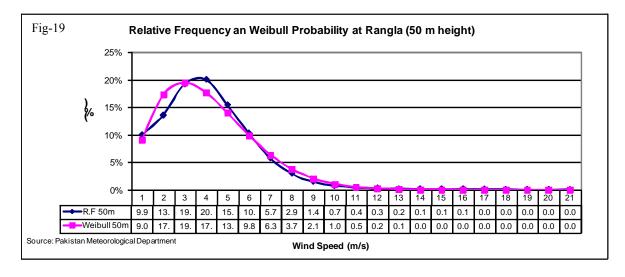
The two Weibull parameters k and c may be derived from site data.

A measure of the confidence of the fit of the Weibull curve to the real data is also returned. Often the Weibull curve is a good fit to the most of the data, but a poor fit to some. If the poor fit is in the low wind speed range, i.e. below cut in it may be possible to ignore the poor fit as this portion of wind does not contribute greatly to the overall power production.

The mathematical description of the wind frequency allows us to match with the turbine power curve. Thus a measure of the average total power capture in a year is achieved. Additionally the choice of turbine cut in and furling speed may be chosen to maximum the total energy capture.

3.7.5 Weibull Parameters:

Fig-19 shows the Weibull fit to the relative frequency of wind speed.



The Weibull parameters for three different heights 10 meters, 30 meters and 50 meters are given in Table-3 along with other key results of analysis. If we look at the shape parameters K and scale parameter C for 50 meters height we can find that the shape parameter K varies over a wind range from the lowest of 1.60 during July to the highest of 1.96 during the month of October with a annual value of K being 1.79.

The lowest values of the scale parameter C 3.29 is observed in December while the highest value of 4.83 is obtained in May and with an annual value of 4.05.

3.7.6 Average Wind Speed & Standard Deviation:

In Table-3 monthly average wind speed and standard deviation at three different heights are also given. The average wind speed values for 10 meters and 30 meters height have been obtained from the recorded data, whereas the values for the 50 meters height have been computed by using the power law as explained in the earlier section.

At 10 meters height the annual average wind speed is 1.65 m/s with Standard deviation of 1.16, at 30 meters this average speed is 2.9 m/s with Standard deviation of 1.7.

At 50 meters the monthly average wind speed varies from the lowest of 2.92 m/s in December to highest of 4.34 m/s during May. Whereas the average wind speed is 3.61 m/s with Standard deviation of 2.13.

3.7.7 Power Density:

The monthly power densities for three different heights 10 meters, 30 meters and 50 meters have also been given in Table-3. At 10 meters this power density varies between 5.58 W/m^2 January to 5.02 W/m^2 in December with Average of 8.61 W/m^2 .

At 30 meters height the power density varies from 25.87 W/m² in January to 17.06 W/m² in December and the average values is about 32.0 W/m².

At 50 meters height the power density of Rangla varies from 56.91 W/m² in January to 32.01 W/m² in December. The average power density of the area is 65.73 W/m².

Table-3: Monthly Average Wind, St. Deviation and Wind Power Density at Rangla

		10 m			
	Avg V (m/s)	St Dev	C (m/s)	K	P/A (w/m²)
January	1.52	1.02	1.69	1.55	5.58
February	1.97	1.28	2.19	1.59	11.66
March	2.07	1.36	2.31	1.58	13.68
April	1.91	1.25	2.13	1.58	10.77
May	2.09	1.66	2.26	1.29	19.67
June	1.69	1.31	1.84	1.32	9.86
July	1.24	1.16	1.27	1.07	5.86
August	1.23	0.92	1.34	1.36	3.59
September	1.41	1.10	1.53	1.31	5.82
October	1.72	1.03	1.93	1.75	6.93
November	1.53	0.91	1.71	1.74	4.84
December	1.48	0.97	1.65	1.58	5.02
Average	1.65	1.16	1.82	1.48	8.61
		30 m			
	Avg V (m/s)	St Dev	C (m/s)	K	P/A (w/m²)
January	2.67	1.60	2.99	1.74	25.87
February	3.08	1.70	3.47	1.91	35.88
March	3.34	1.82	3.76	1.93	44.97
April	3.12	1.78	3.51	1.83	38.78
May	3.47	2.32	3.86	1.55	66.66
June	2.99	1.81	3.35	1.72	36.83
July	2.57	1.69	2.87	1.58	26.27
August	2.54	1.38	2.86	1.94	19.68
September	2.63	1.55	2.95	1.77	24.23
October	3.01	1.50	3.40	2.14	29.99
November	2.50	1.32	2.82	2.00	18.28
December	2.39	1.34	2.69	1.87	17.06
Average	2.9	1.7	3.2	1.8	32.0
		50 m			
	AvgV (m/s)	St Dev	C (m/s)	K	P/A (w/m²)
January	3.39	2.14	3.78	1.64	56.91
February	3.74	2.05	4.22	1.92	63.92
March	4.13	2.27	4.66	1.91	86.37
April	3.90	2.28	4.38	1.79	78.14
May	4.34	2.86	4.83	1.57	127.17
June	3.79	2.37	4.24	1.66	78.64
July	3.41	2.21	3.80	1.60	60.12
August	3.35	1.89	3.77	1.86	47.40
September	3.39	2.01	3.81	1.76	52.50
October	3.86	2.08	4.36	1.96	68.88
November	3.11	1.71	3.50	1.92	36.64
December	2.92	1.67	3.29	1.84	32.01
Average	3.61	2.13	4.05	1.79	65.73

ESTIMATING WIND GENERATED ELECTRIC POWER OUTPUT

Appendix-I

Monthly Average Diurnal Variation of Wind Generated Electric Power Output.

Appendix-II

Hourly Wind Generated Electric Power Output

4.0 Estimating Wind Generated Electric Power Output

The average power output of wind energy conversion technologies (WECT) is a very important parameter since it determines the energy output over time thereby influencing the economic feasibility of a wind project. It is by far more useful than the rated power, which does not account for the variability of wind velocity thereby easily overestimating energy revenues. The average power of wind turbine, $\overline{P_{WT}}$, is the power produced at each wind speed multiplied by the fraction that wind speed is experienced, integrated over all possible wind speeds. In integral form this can be expressed as (Manwell et al., 2002; Borowy and Salameh, 1996):

$$\overline{P_{WT}} = \int_{0}^{\infty} P_{WT}(v) df(v)$$

This integral can be replaced with a summation over bins, N_{B_s} to calculate the average wind turbine power (Manwell et al., 2002).

$$\overline{P_{WT}} = \sum_{j=1}^{N_B} \left\{ \exp \left[-\left(\frac{v_{j-1}}{c}\right)^k \right] - \exp \left[-\left(\frac{v_j}{c}\right)^k \right] \right\} P_{WT} \left(\frac{v_{j-1} + v_j}{2}\right)$$

Please note that the relative frequency, f_j/N , corresponds to the term in brackets and the power output is calculated at the midpoint between v_{j-1} and v_j .

The available power at any given wind speed v that is convertible by a turbine is defined by (Manwell et al., 2002 Johnson, 1985)

$$P_{WT}(v) = \frac{1}{2} \rho A C_p \eta v^3$$

Where η is the drive terrain efficiency (i.e. generator power/rotor power), C_p , is the machine power coefficient. In an idealized wind turbine no losses are experienced and the power coefficient, C_p , is equal to Betz' limit (i.e. $C_{p,Betz}=16/27$) and $\eta=1$. Of course, in reality both the drive terrain efficiency and the power coefficient cannot be maximized. The extent to which the power output is limited by physical laws as well as engineering inefficiency is dependent on the specific characteristics of individual wind turbine types. This aspect will be discussed further in the analysis of the case study.

WECTs have a range of different power output performance curves, which need to be recognized when estimating the potential power output. The power output performance curves are not only defined by parameters such as the power coefficient and the drive terrain efficiency but also constrained by cut-in speed, furl-out speed and rated wind speed. Where the cut-in wind seed, v_c , is the minimum wind velocity to generate power from a turbine, the rated wind speed, v_R , is the wind speed at which the 'rated power' of a WETC is achieved and generally corresponds to the point at which the conversion efficiency is near its maximum and furl-out wind speed, v_F , is the wind speed at which the turbine shuts down to prevent structural damage.

To account for the above-mentioned constraints we can formulate a novel formula for the average electrical power output of a turbine, $\overline{P_{WTA}}$:

$$\overline{P_{WTA}} = \begin{cases}
\sum_{j=1}^{N_B} \left\{ \exp\left[-\left(\frac{v_{j-1}}{c}\right)^k\right] - \exp\left[-\left(\frac{v_j}{c}\right)^k\right] \right\} P_{WT}\left(\frac{v_{j-1} + v_j}{2}\right) & (v_c \le v \le v_R) \\
\sum_{j=1}^{N_B} \left\{ \exp\left[-\left(\frac{v_{j-1}}{c}\right)^k\right] - \exp\left[-\left(\frac{v_j}{c}\right)^k\right] \right\} P_{WT}(v_r) & (v_R \le v \le v_F) \\
0 & (v < v_c \text{ and } v > v_F)
\end{cases}$$

The energy production of the wind turbine WE(t) over time t can thus be calculated as

$$WE(t) = \overline{P_{WTA}}t$$

Another way of stating the energy output from a wind turbine is to look at the capacity factor for the turbine in its particular location. The capacity factor CF, is the actual energy output over a given period of time, WE(t), divided by the theoretical maximum energy output (i.e. this means that the machine is constantly running at its rated output) during the selected time-span, RO(t). This can be formulated as

$$CF = \frac{WE(t)}{RO(t)}$$

Theoretically capacity factor vary from 0 to 100%. In practice they usually range from 20 to 70% and mostly be around 20-30 percent. However, the economic feasibility of a wind turbine does not of course depend on the capacity factor of a wind turbine alone but also depends on the costs of alternative power systems. Therefore, a low capacity factor does not automatically render a wind turbine project unfeasible.

In order to maximize the energy output of a given wind regime the optimum wind speed, v_{opt} , needs to be determined. The optimum wind speed indicates at what wind velocity most energy is available in a given wind regime. It is at this particular wind speed that engineers should ensure that the power coefficient is most efficient to allow for the highest energy conversion of a turbine. The optimum wind speed can be calculated as follows (Lu et al., 2002):

$$v_{opt} = c \left(\frac{k+2}{k}\right)^{\frac{1}{2}}$$

In this regard, the power density of a turbine is a good comparative indicator to show the average power output per m^2 of wind swept area, A, at a given site. This can be defined as

Power Density =
$$\frac{\overline{P_{WTA}}}{A}$$

Another important aspect of that critically determines the energy output of a turbine is elevation. In many cases the available recorded wind speed data has been measured at a lower level than the planned hub height of the wind turbine. As wind velocity increases vertically the recorded wind speed data can be adjusted using the following standard formula (Borowy and Salameh, 1996.) where ν is the projected wind speed, ν_i the wind speed at reference height, H the hub height of a turbine, Hi the reference height and α the power-law exponent.

$$v = v_i \left(\frac{H}{H_i}\right)^{\alpha}$$

 α is often quoted to have a value of 1/7 and is seen as a reasonable power law exponent for even and unobstructed landscapes. However, where WECT development is planned either offshore or near woodlands or close to any other non flat terrains this value can differ subsequently and a more through analysis of α is necessary. Justus as well as Counnihan offer mathematical solution for 'fitting' α to these environments (Manwell et al., 2002).

4.1 Hypothetical Wind Generated Electric Power:

A **wind turbine** is a machine for converting the kinetic energy in wind into mechanical energy. If the mechanical energy is used directly by machinery, such as a pump or grinding stones, the machine is usually called a windmill. If the mechanical energy is then converted to electricity, the machine is called a wind generator.

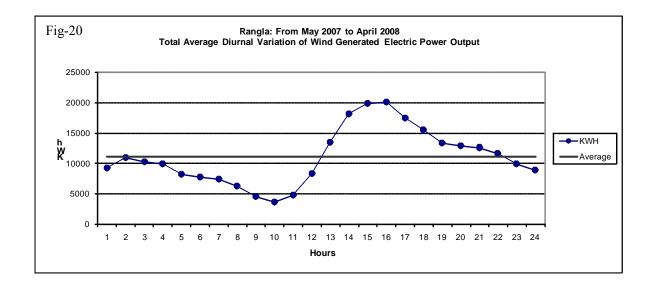
Hypothetical wind generated electric power output at Rangla has been estimated by using the 600KW wind turbine bonus 600/44 MK IV type. The cut in wind speed of this turbine is 3m/s and cutout wind speed is 25m/s. Rotor diameter of this turbine is 44 meters and hub height has been taken as 50 meters. The monthly and annual wind generated electric power outputs at Rangla are shown below in graphs and table-4.

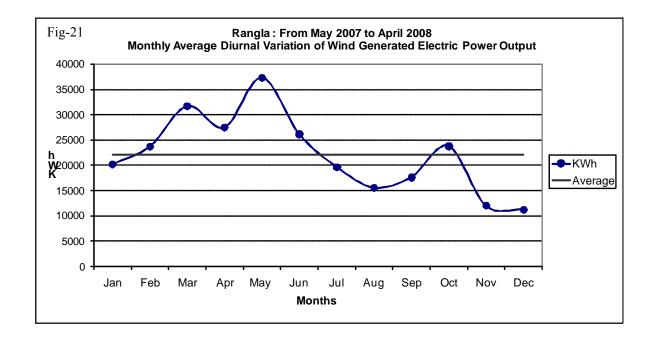
Table-4: Hypothetical wind generated electric energy output & capacity Factor for a Bonus 600/44MK IV Turbine at Rangla.

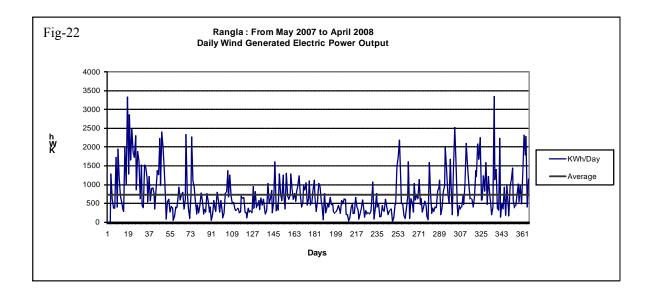
	PMD (Calculator (using	g 50M)	
Month	Input W/m ²	Output W/m ²	C.F.	KWh / Month
January	60	23	6%	25,622
February	67	26	7%	27,459
March	91	35	9%	39,838
April	82	32	8%	34,561
May	134	48	12%	53,853
June	83	31	8%	34,303
July	63	24	6%	26,993
August	50	19	5%	21,279
September	55	21	5%	22,939
October	73	28	7%	31,777
November	39	14	4%	15,411
December	34	12	3%	13,646
Annual	65	25	6%	332,976

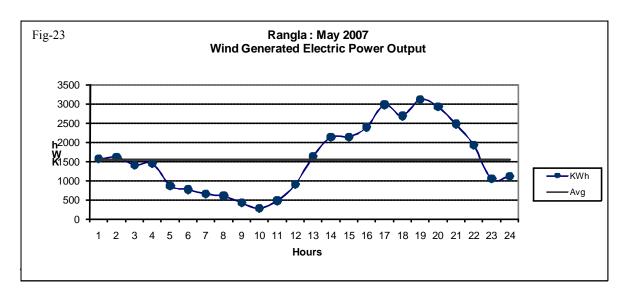
Wind Turbine spec	ification
Turbine	Bonus 600 / 44 MK IV
Power	600 KW
Cut in Wind	3 m/s
Cut out wind	25 m/s
Rotor Diameter	44 m
Hub height	50 m

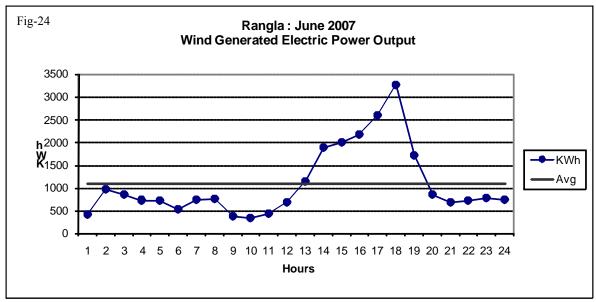
Figure 20 shows the average diurnal variation of wind generated electric energy output at Rangla (May-Apr). The graph shows that the maximum power is produced at about 3 PM; of course, this is the same time when we have the maximum wind speed in 24 hours. Figure 21 & 22 shows the monthly and daily wind generated electric power output. Figure 21 depicts that at Rangla the wind have more potential in the month of May as compared to other months. Figure 23 to 34 shows the monthly average diurnal variation of wind generated electric energy output.

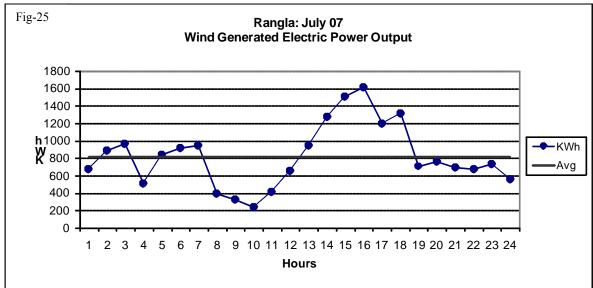


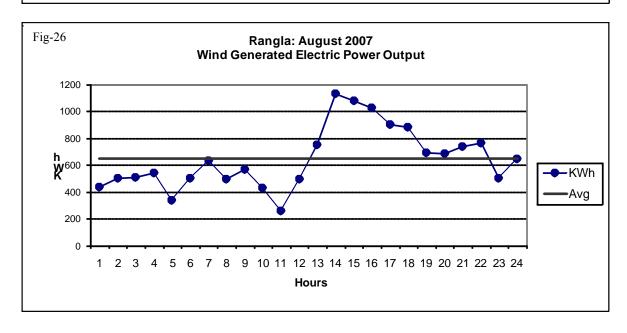


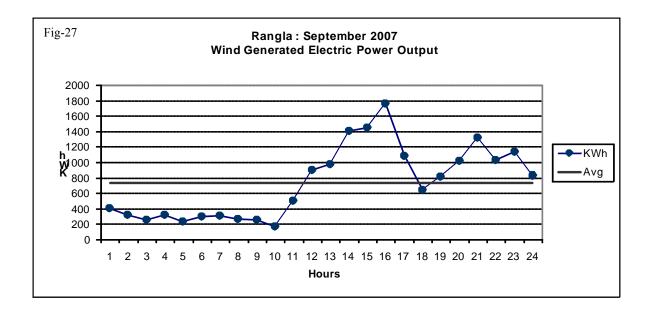


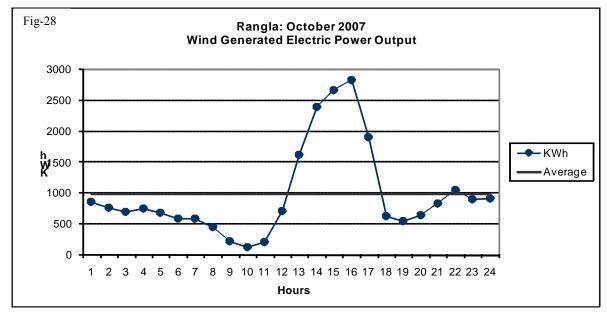


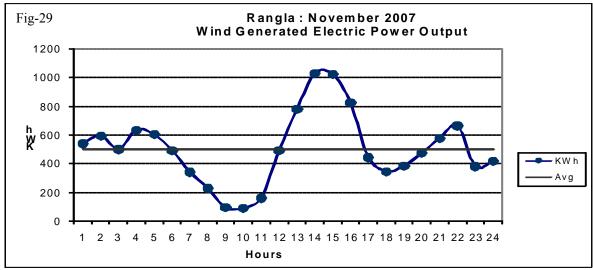


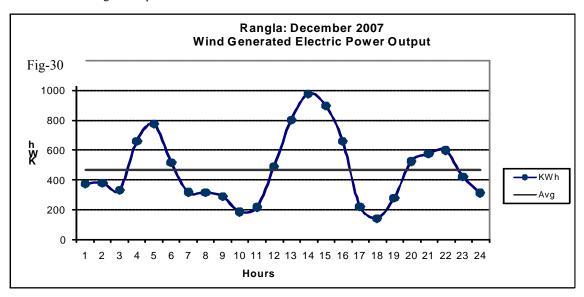


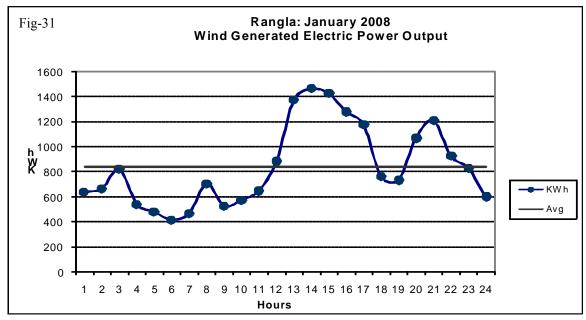


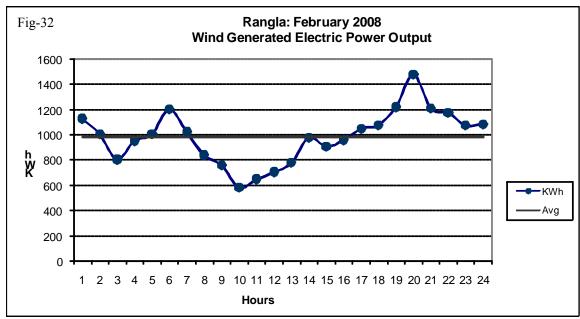


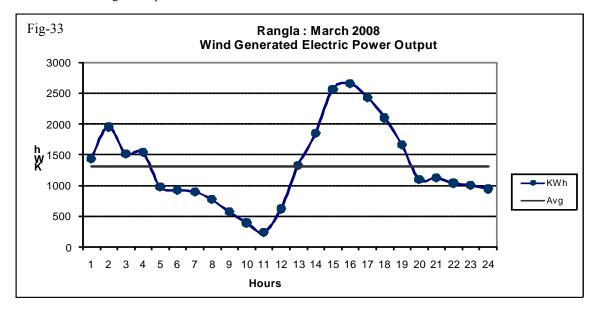


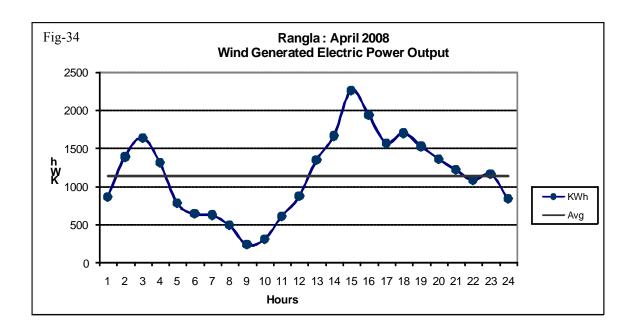










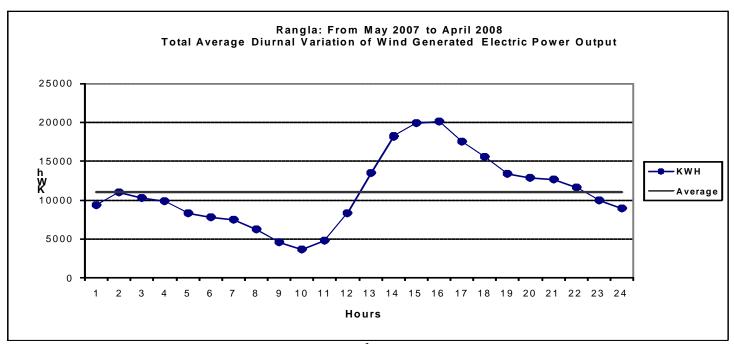


Appendix-I

Rangla	May 2007 to April 2008
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Wind Power Output of Bonus 600/44 Turbine (12 Month's Summary)

Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
May	1553	1596	1391	1433	853	755	633	585	408	267	461	890	1614	2123	2125	2378	2964	2676	3098	2913	2467	1912	1031	1098	37226
Jun	421	980	849	731	718	531	735	763	381	340	433	675	1144	1892	1993	2178	2600	3261	1713	846	676	713	779	749	26102
Jul	669	881	965	500	834	911	942	390	323	233	405	654	936	1270	1502	1609	1188	1307	703	757	687	673	729	552	19620
Aug	440	505	508	541	342	506	634	497	569	434	262	495	756	1134	1082	1027	904	888	693	688	739	764	502	650	15561
Sep	406	311	254	313	233	294	302	263	251	166	500	894	971	1402	1438	1754	1078	638	805	1012	1311	1028	1136	826	17585
Oct	864	776	708	761	694	594	592	462	235	134	221	710	1620	2398	2664	2827	1900	637	557	650	843	1051	909	917	23721
Nov	536	591	496	630	598	487	337	223	89	85	155	487	775	1025	1018	821	440	341	381	470	571	660	376	412	12005
Dec	372	379	330	658	774	516	315	315	285	182	214	488	803	977	899	659	216	138	276	523	572	598	419	310	11217
Jan	636	663	818	535	477	413	464	701	523	570	646	881	1371	1462	1424	1276	1174	759	730	1065	1206	924	826	598	20139
Feb	1127	1007	805	952	1004	1202	1022	840	759	583	648	707	777	977	907	958	1049	1076	1219	1475	1210	1174	1073	1084	23637
Mar	1432	1953	1515	1539	976	920	899	772	572	393	240	620	1329	1847	2561	2654	2427	2100	1658	1097	1125	1036	1003	945	31611
Apr	861	1388	1638	1313	779	640	625	489	240	309	606	869	1345	1664	2256	1933	1569	1696	1524	1360	1218	1084	1161	835	27398
KWH	9315	11028	10275	9906	8282	7768	7500	6299	4635	3697	4791	8370	13440	18170	19870	20075	17508	15518	13356	12857	12626	11617	9943	8975	265821
Average	11076	11076	11076	11076	11076	11076	11076	11076	11076	11076	11076	11076	11076	11076	11076	11076	11076	11076	11076	11076	11076	11076	11076	11076	



Appendix-II

Rang	jla	M	ay 20	07						Win	d Pov	ver (Outpu	ıt of I	Bonu	s 600	/44 T	urbir	e (Mo	onth's	s Sur	nmar	y)		
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0
4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	11.8	47.1	281.6	450.7	281.1	144.9	66.3	5.5	0.7	0.7	1290
5	0.7	3.9	14.8	2.0	0.0	0.0	0.0	8.4	5.5	0.0	14.8	39.9	44.6	66.3	44.6	50.3	45.6	7.1	5.5	2.0	0.0	12.4	126.8	113.2	608
6	17.2	12.6	11.9	12.6	12.6	3.3	0.7	2.0	0.0	0.0	2.0	18.3	35.3	32.4	50.3	79.8	55.9	11.9	18.1	8.4	2.0	0.0	0.0	4.2	391
7	18.3	0.7	0.0	0.0	0.0	20.0	2.0	2.0	11.3	3.9	23.0	18.3	23.0	60.6	61.6	66.3	45.6	5.5	7.7	1.3	5.5	1.3	2.0	1.3	381
8	8.9	173.1	208.4	396.2	104.1	57.0	60.6	1.3	0.0	3.3	12.6	12.6	2.0	4.8	71.9	150.1	84.6	16.6	0.7	79.0	91.7	74.2	85.5	30.6	1729
9	4.2	10.6	16.6	5.5	55.9	25.8	15.4	9.7	21.2	9.7	2.6	5.5	15.4	16.6	29.8	62.5	69.5	9.7	1.3	0.0	1.3	0.0	2.6	9.0	400
10	35.3	12.6	6.1	9.7	2.6	9.0	6.8	2.6	2.6	0.0	5.5	35.3	46.6	24.8	2.0	15.2	509.5	558.7	476.1	35.1	29.2	1.3	23.0	105.9	1955
11	183.5	102.9	67.2	40.9	53.0	109.2	91.1	34.5	17.2	13.7	24.8	66.3	71.9	67.2	77.6	79.8	55.0	15.4	0.7	6.1	8.4	6.1	0.0	0.0	1192
12	0.0	28.8	77.6	50.3	12.6	3.3	0.0	0.0	1.3	6.1	20.1	44.6	44.6	66.3	91.1	60.6	71.9	44.6	21.2	11.9	3.3	9.7	3.3	15.9	689
13	18.3	9.7	1.3	0.7	0.0	0.0	0.7	0.0	0.0	5.5	21.2	25.9	18.3	50.3	114.9	99.0	85.5	45.6	14.1	0.0	4.8	2.6	0.0	0.7	519
14	3.3	6.1	2.0	0.7	0.0	0.0	0.0	0.0	0.7	0.0	1.3	14.4	18.3	44.6	71.9	71.9	51.2	27.7	3.3	0.0	3.5	1.3	0.0	0.0	322
15	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.6	2.0	1.3	40.9	30.6	60.6	44.6	35.3	24.8	13.7	8.4	2.6	4.8	1.3	7.7	281
16	161.3	244.5	54.4	9.0	144.1	164.9	228.8	218.0	24.8	105.8	150.1	86.7	16.6	51.2	55.0	83.2	49.3	35.3	6.1	6.8	0.7	2.6	11.9	79.8	1991
17	158.4	228.3	91.1	11.9	8.4	18.3	3.3	27.7	6.8	1.3	0.7	9.7	45.6	55.9	91.1	87.7	76.4	23.0	9.0	3.3	2.0	4.8	11.9	39.9	1016
18	21.2	18.3	0.7	2.0	9.7	12.6	0.7	0.0	0.0	2.6	15.4	44.6	39.9	87.7	93.4	142.6	191.4	101.2	555.6	585.0	536.0	541.3	330.7	8.2	3341
19	243.0	37.7	163.7	82.1	40.9	77.6	36.2	27.7	9.7	1.3	4.8	39.9	60.6	60.6	60.6	50.3	44.6	15.4	5.5	2.6	49.3	35.3	71.9	66.3	1287
20	159.7	421.6	444.3	572.8	240.8	141.4	38.4	22.2	3.5	4.8	4.2	25.9	45.6	118.8	138.6	60.6	66.3	14.5	22.9	210.0	80.8	13.7	2.0	6.8	2860
21	18.3	12.6	6.8	3.9	3.3	2.0	14.1	16.6	22.4	0.0	0.0	15.9	20.6	69.5	141.0	209.7	217.9	78.1	281.6	154.5	107.5	203.3	56.0	2.0	1657
22	20.1	44.6	17.2	48.4	42.7	0.0	5.5	3.5	0.7	7.1	0.7	5.5	57.2	20.1	103.0	111.2	208.0	166.5	255.8	554.5	474.4	202.5	18.8	107.0	2475
23	60.6	77.6	66.3	9.7	18.4	35.3	84.4	9.5	0.7	2.0	6.1	40.9	315.6	460.0	26.0	55.6	95.7	79.8	126.8	75.1	30.6	107.0	54.0	11.3	1849
24	44.6	39.9	44.6	49.3	21.2	19.5	20.1	18.3	9.0	12.4	13.1	39.9	4.2	4.2	61.6	23.0	13.1	178.9	175.8	146.1	51.2	268.1	106.8	358.6	1724
25	267.3	58.4	29.2	55.9	60.6	8.4	4.2	171.1	268.4	80.4	69.5	20.1	19.5	33.3	77.4	295.0	134.7	228.3	130.7	130.7	94.0	27.7	4.8	25.9	2295
26	18.3	0.0	39.9	61.6	15.4	12.6	12.6	0.7	0.0	3.5	23.0	56.6	186.1	185.8	45.6	50.3	71.9	23.0	9.7	21.2	25.9	2.6	0.0	0.0	866
27	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	1.3	36.2	33.7	88.7	9.7	12.6	117.4	357.4	528.2	333.4	166.4	95.7	35.3	55.9	1872
28	77.6	39.9	20.1	5.5	2.6	20.1	4.2	0.0	0.0	0.0	5.5	55.9	138.6	154.5	95.0	266.9	77.0	60.6	60.6	217.6	229.8	50.3	27.7	25.9	1636
29	9.7	4.8	3.9	2.0	3.3	15.4	3.9	9.7	2.6	0.7	0.0	9.7	69.1	5.5	94.6	21.9	2.6	24.2	20.1	60.6	158.4	71.9	32.7	0.7	628
30	0.0	0.0	0.0	1.3	0.7	0.0	0.0	0.0	0.0	0.0	30.6	77.6	114.9	163.7	308.2	79.8	195.9	67.2	54.4	53.4	204.5	134.2	20.6	21.2	1528
31	3.3	6.8	2.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	6.8	42.7	85.5	99.0	36.6	0.7	10.6	4.8	11.9	61.6	37.1	32.4	1.3	0.0	443
KWh	1553	1596	1391	1433	853	755	633	585	408	267	461	890	1614	2123	2125	2378	2964	2676	3098	2913	2467	1912	1031	1098	37226

Rangl	la		June	2007						W	ind l	Powe	er Ou	tput o	f Bon	us 60	0/44	Turbir	ne (Mo	onth's	Sum	mary)		
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	0.0	0.7	2.6	2.6	3.9	3.9	21.2	3.9	3.3	3.9	18.3	0.7	62.5	85.5	20.1	26.9	30.6	15.4	45.6	36.2	7.7	0.0	0.0	1.3	397
2	36.0	7.1	113.5	9.7	72.7	130.7	59.5	40.9	30.6	35.3	30.6	21.2	107.5	144.9	101.3	53.1	25.3	46.9	158.4	36.0	13.1	82.1	63.8	107.0	1527
3	14.4	24.8	0.0	27.7	19.5	18.8	118.8	229.5	62.4	17.7	18.3	0.7	23.0	22.9	146.1	292.8	12.6	10.8	3.3	40.9	26.9	51.2	83.2	165.1	1431
4	61.6	99.6	64.8	66.3	101.3	38.4	61.6	192.3	4.2	0.0	0.7	12.6	15.4	6.8	21.2	21.2	25.9	66.3	35.3	25.9	44.6	77.6	79.8	30.6	1154
5	35.3	11.9	32.4	39.9	49.3	21.2	35.3	9.7	30.6	50.3	3.3	4.2	16.6	21.9	4.8	2.6	0.0	20.1	38.0	23.0	17.2	27.7	25.9	18.3	539
6	13.1	429.8	247.1	20.9	37.3	42.1	23.0	9.7	15.4	2.0	0.0	2.6	16.6	50.3	61.6	61.6	64.2	20.1	17.7	3.3	8.4	0.7	29.5	49.3	1226
7	25.9	23.0	32.4	12.6	37.1	25.9	41.7	3.3	11.3	21.2	6.1	9.7	1.3	0.7	4.8	42.7	22.4	27.7	4.2	0.0	0.7	0.7	85.5	130.7	571
8	67.2	44.6	50.3	66.3	35.3	25.9	8.4	3.9	9.7	11.9	9.0	2.0	42.7	85.5	69.5	83.1	56.3	44.6	23.0	80.1	0.0	13.7	21.2	35.3	889
9	18.3	9.7	9.7	6.8	12.6	12.6	44.6	66.3	30.6	21.2	39.9	25.9	9.0	80.2	82.1	91.1	83.2	66.3	7.7	12.6	9.7	39.9	66.3	66.3	912
10	35.3	44.6	25.9	74.2	49.3	55.0	44.6	6.8	0.7	0.0	0.0	6.1	50.3	55.9	83.2	66.3	55.9	29.8	1.3	15.3	15.9	25.9	1.3	2.0	745
11	0.7	1.3	4.8	2.0	0.7	0.0	0.0	0.0	0.0	0.0	9.0	46.6	33.3	27.7	71.9	99.0	22.7	5.5	2.0	9.7	0.7	6.1	2.0	4.8	350
12	1.3	1.3	2.0	1.3	1.3	0.0	0.0	0.0	0.0	4.8	25.9	35.3	35.3	66.3	33.3	122.8	155.7	146.6	166.4	40.8	4.8	14.4	5.5	0.7	865
13	9.0	99.6	16.6	0.0	0.0	0.0	0.0	0.7	3.3	2.6	15.4	24.8	51.2	51.2	118.8	122.8	269.2	209.7	35.1	22.7	219.4	43.0	36.6	18.3	1370
14	0.0	0.0	26.0	20.6	10.8	10.6	4.2	3.5	0.0	5.5	12.6	24.8	15.9	294.8	20.6	27.7	132.9	424.7	154.4	13.7	20.1	33.3	10.6	9.0	1276
15	23.4	7.7	18.1	190.1	114.7	4.2	24.2	4.2	12.6	35.3	37.1	77.6	229.5	242.9	269.5	256.4	216.4	448.4	23.0	3.5	0.0	1.3	0.0	0.0	2240
16	0.0	2.0	20.1	39.9	9.0	4.8	115.2	86.1	118.4	19.4	0.7	2.0	27.7	71.9	79.8	17.7	301.7	29.5	1.3	9.0	0.7	2.0	11.9	3.9	974
17	36.1	40.9	61.6	46.9	42.7	14.4	3.5	1.3	0.0	1.3	2.6	27.6	66.3	118.8	268.2	206.0	235.3	587.2	443.3	180.4	0.0	7.7	1.3	15.4	2409
18	3.3	0.0	0.7	3.3	1.3	4.8	18.3	12.6	0.7	0.0	0.7	20.1	44.6	77.6	158.4	228.3	379.4	534.7	251.7	4.2	55.9	63.8	77.4	20.1	1962
19	12.6	55.9	45.6	21.9	61.6	55.9	25.9	3.9	0.0	3.5	30.6	55.9	42.7	60.6	196.6	50.5	209.1	370.0	24.2	15.4	0.0	2.0	0.7	0.0	1345
20	0.0	1.3	20.1	18.3	15.4	18.8	23.0	8.4	0.0	0.7	14.1	77.4	77.6	93.4	11.3	50.3	83.2	50.3	4.2	1.3	11.9	2.0	1.3	9.0	593
21	0.7	17.2	4.2	1.3	3.9	2.0	0.7	1.3	3.3	9.0	15.4	0.7	2.0	0.7	0.7	9.7	4.8	0.0	0.0	0.0	1.3	4.8	1.3	3.3	88
22	2.0	6.8	6.1	5.5	11.9	2.6	4.2	2.6	0.7	0.7	3.5	7.1	1.3	2.0	0.0	0.0	0.7	23.1	91.7	77.6	26.9	113.2	121.0	35.1	546
23	18.3	15.4	9.7	6.1	4.2	0.0	0.0	24.8	12.6	8.4		60.6	40.9	60.6	85.5	101.3	60.6	19.4	3.9	25.9	2.0	1.3	0.0	0.7	618
24	0.0	0.0	1.3	6.1	15.4	1.3	2.6	0.0	0.0	1.3	12.6	6.1	15.4	8.4	9.0	45.6	39.9	21.2	20.1	23.0	25.9	9.7	1.3	1.3	268
25	2.0	4.8	3.9	4.2	0.0	0.7	0.0	0.0	0.0	5.5	10.2	36.4	4.8	24.8	17.2	9.0	30.6	4.8	66.3	55.0	79.8	40.9	12.4	8.4	422
26	0.7	0.0	0.0	0.0	4.2	12.4	13.1	0.0	0.0	4.8	40.9	32.4	74.2	87.7	43.7	22.7	30.0	0.7	2.0	0.7	0.0	19.5	6.1	0.0	396
27	0.0	0.0	1.3	1.3	0.7	0.0	0.0	0.0	0.0	0.0	0.7	0.7	0.0	2.0	0.7	3.9	4.2	0.7	1.3	1.3	1.3	9.5	10.2	4.8	44
28	0.0	4.2	4.2	1.3	0.7	0.0	0.0	0.7	7.7	15.4	9.0	9.0	0.7	9.0	2.6	9.0	0.0	0.0	3.5	26.3	44.2	0.0	1.3	6.8	155
29	4.2	25.3	22.7	30.5	2.0	1.3	1.3	6.8	4.2	16.6	8.9	25.9	27.7	20.6	2.6	47.7	45.9	35.3	30.6	12.6	7.7	1.3	19.5	1.3	402
30	0.0	0.0	1.3	3.9	0.0	23.0	39.9	39.9	19.5	42.1	1.3	19.4	7.7	17.1	8.4	6.8	1.3	2.0	54.0	50.3	29.5	17.7	2.0	0.0	387
KWh	421	980	849	731	718	531	735	763	381	340	433	675	1144	1892	1993	2178	2600	3261	1713	846	676	713	779	749	26102

Rang	la	Jι	ıly 200	07						W	ind I	owe	er Ou	tput (of Boı	nus 60	00/44	Turbi	ne (M	onth's	Sum	mary)		
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	4.8	0.0	3.3	3.3	0.0	0.0	0.0	0.7	0.0	2.0	6.8	39.9	35.3	60.6	79.8	91.1	61.6	55.9	42.7	55.9	45.6	39.9	46.6	50.3	726
2	17.2	78.1	359.7	84.5	31.3	7.7	13.1	21.3	15.9	0.7	19.0	48.4	17.7	40.9	61.6	68.5	27.7	7.7	0.0	0.7	0.0	0.0	0.0	1.3	923
3	0.0	0.7	0.0	30.5	27.7	3.3	35.3	0.0	0.0	0.7	23.5	46.6	44.6	66.3	77.6	114.9	71.4	16.6	8.4	5.5	0.0	3.3	16.6	2.0	595
4	0.0	0.7	1.3	18.3	21.2	77.6	99.0	71.9	66.3	9.5	30.6	49.3	85.5	66.3	54.0	20.1	21.2	7.7	0.0	14.8	12.6	0.0	6.8	0.0	734
5	0.7	0.0	2.6	9.0	0.7	0.0	0.0	2.0	12.6	14.8	0.7	14.8	15.4	50.6	42.7	28.8	20.6	40.9	51.2	59.2	47.7	36.1	325.9	10.8	788
6	1.3	1.3	9.0	0.7	9.0	25.9	27.7	4.8	1.3	9.7	35.3	30.6	39.9	25.9	50.3	44.6	11.9	0.0	0.0	0.0	2.0	2.0	12.6	2.0	347
7	0.0	0.0	24.8	8.9	23.0	6.1	7.7	0.0	4.2	11.3	3.9	12.6	48.8	107.0	140.9	125.1	12.4	9.7	1.3	0.7	1.3	9.7	20.1	7.7	587
8	2.6	9.5	30.5	3.5	502.7	598.3	549.6	103.6	113.2	16.6	0.0	0.0	9.7	39.9	55.0	30.6	39.9	30.6	23.0	35.3	3.5	3.5	19.5	119.4	2340
9	203.3	83.1	51.2	63.8	39.9	27.7	0.7	0.0	0.0	2.0	25.9	39.9	44.6	39.9	55.0	66.3	24.8	3.3	0.0	0.0	0.7	3.9	4.8	39.9	821
10	14.8	0.0	0.0	4.8	3.3	0.0	0.7	0.0	0.0	2.0	15.4	21.2	35.3	46.6	60.6	45.6	17.2	9.0	6.8	12.6	29.5	12.6	9.7	3.9	351
11	3.3	5.5	1.3	0.7	0.0	0.0	2.6	0.0	3.9	0.7	2.0	0.0	15.9	4.2	1.3	0.0	0.0	0.0	2.6	5.5	7.7	3.9	12.6	27.7	101
12	11.3	1.3	0.0	1.3	2.0	4.8	2.0	3.5	5.5	0.0	0.7	6.1	14.4	18.3	35.3	17.2	45.6	45.6	49.3	126.6	44.0	38.0	58.2	194.0	725
13	122.7	405.7	318.9	133.0	72.7	16.6	69.5	28.8	9.0	0.7	55.9	26.3	32.4	114.9	77.6	134.7	102.9	392.8	61.6	62.9	5.5	9.0	7.7	0.0	2262
14	2.6	0.7	0.7	3.9	0.0	0.0	2.6	0.0	4.2	3.3	11.9	24.8	24.8	21.9	67.2	13.7	72.3	32.4	55.9	226.0	251.2	159.8	114.7	4.2	1099
15	101.5	146.5	133.4	95.6	20.6	20.6	0.7	0.7	1.3	1.3	19.5	39.9	39.9	55.0	60.6	99.0	42.7	27.7	11.9	0.0	9.0	9.0	1.3	2.0	940
16	2.0	0.0	0.0	13.1	39.9	18.3	6.8	3.9	0.0	0.7	9.0	30.6	50.3	60.6	85.5	54.5	79.8	35.1	5.5	15.4	5.5	3.3	1.3	0.0	521
17	0.0	0.7	0.0	0.7	2.0	1.3	2.0	21.2	25.6	46.9	2.0	0.7	5.5	6.1	24.8	35.3	27.7	7.7	0.0	0.0	0.0	11.3	2.6	0.7	224
18	0.0	0.0	0.0	3.9	3.3	0.0	0.0	21.9	9.7	2.0	0.0	5.5	35.3	44.6	101.3	90.0	69.5	51.6	6.8	3.3	2.6	3.3	0.7	0.7	456
19	0.0	2.0	1.3	1.3	0.7	0.0	0.0	1.3	0.0	3.3	9.7	30.6	42.7	19.5	23.0	12.6	18.3	18.3	6.8	17.2	24.8	9.0	1.3	3.3	247
20	0.7	1.3	3.3	1.3	0.0	3.5	0.0	1.3	1.3	3.3	11.9	11.9	35.3	48.4	24.8	39.9	51.6	62.3	113.0	4.8	2.0	1.3	0.7	11.8	435
21	1.3	2.0	1.3	8.4	11.9	38.0	8.4	11.3	11.5	2.0	12.6	15.4	23.0	45.6	69.5	30.6	32.4	36.2	109.2	36.4	121.1	127.3	11.9	12.4	779
22	20.0	9.5	0.0	0.0	0.0	0.7	8.4	20.1	0.7	2.6	6.1	37.0	18.1	9.5	9.7	196.6	165.5	19.4	22.2	0.7	4.8	1.3	1.3	0.0	554
23	18.8	45.6	18.3	4.2	4.2	6.1	0.7	0.0	0.7	2.6	2.0	5.5	5.5	11.9	0.0	0.0	21.2	9.0	2.0	20.1	20.1	21.2	2.0	0.0	221
24	0.0	0.0	0.0	2.0	1.3	0.7	0.7	2.0	0.0	0.0	3.3	20.1	23.0	19.5	14.4	30.6	11.3	2.6	6.1	12.6	22.9	140.8	13.7	5.5	333
25	55.0	58.4	0.0	0.0	0.0	4.2	8.4	0.7	3.3	6.8	9.0	1.3	2.6	12.4	9.7	19.5	6.1	13.7	12.6	11.5	11.9	0.0	2.0	17.2	266
26	11.8	0.0	0.7	0.0	0.0	0.0	0.0	2.0	2.0	0.7	9.0	15.4	21.2	45.6	110.9	87.7	38.4	327.9	42.1	22.1	4.2	7.7	3.3	1.3	754
27	2.6	2.0	2.0	1.3	7.1	24.2	63.8	46.9	4.8	56.0	56.9	55.0	93.4	62.5	9.7	7.7	18.3	9.7	12.6	2.0	0.0	0.0	11.3	11.3	561
28	17.2	0.7	0.0	0.7	0.0	0.0	0.0	2.0	3.9	3.9	1.3	12.6	30.6	61.6	32.6	7.7	14.8	11.9	9.7	0.7	5.5	6.8	17.7	23.0	264
29	51.2	24.2	0.0	0.0	2.6	4.2	11.9	13.7	0.7	2.6	15.4	8.4	24.8	44.6	45.5	64.8	35.3	7.1	31.0	4.8	1.3	9.0	0.7	0.0	404
30	0.0	1.3	1.3	0.0	0.0	11.9	4.8	0.7	0.7	6.8	0.7	0.7	8.4	2.0	1.3	6.1	9.0	0.7	0.0	0.0	0.0	0.0	2.0	0.0	58
31	2.6	0.7	0.0	1.3	6.8	9.7	15.4	3.9	21.2	18.3	5.5	3.3	12.6	17.2	20.1	25.6	17.1	14.4	9.0	0.7	0.0	0.0	0.0	0.0	205
KWh	669	881	965	500	834	911	942	390	323	233	405	654	936	1270	1502	1609	1188	1307	703	757	687	673	729	552	19620

Rang	la	Aug	gust 2	007							Wind	d Pov	ver C	utput	of Bo	onus 6	00/44	Turbir	ne (M	onth	's Sun	nmary)		
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	0.0	0.0	0.0	0.7	9.0	0.7	3.5	5.5	0.0	1.3	12.6	2.0	13.7	79.8	18.1	16.6	23.0	20.1	14.4	79.4	254.3	10.8	4.2	13.1	582
2	4.8	21.2	9.7	2.0	0.0	1.3	0.7	4.2	32.3	41.3	46.9	4.8	0.0	0.0	1.3	20.1	35.3	40.9	17.2	12.6	9.0	0.0	4.8	20.1	330
3	9.0	4.2	0.0	0.7	0.7	21.9	29.5	3.3	2.6	12.6	12.6	32.4	12.6	2.0	0.0	0.0	0.0	9.0	25.9	50.3	11.9	9.7	20.1	22.2	293
4	39.9	17.1	0.7	1.3	0.0	0.7	5.5	12.6	93.4	39.9	18.3	2.6	9.0	50.3	25.6	15.8	63.5	24.0	42.7	30.6	21.3	229.5	22.2	26.0	792
5	2.6	8.4	0.7	5.5	4.8	49.3	39.9	24.8	28.8	0.0	0.0	11.3	23.0	50.6	23.0	0.0	14.8	23.0	5.5	8.4	4.2	66.3	163.7	26.9	585
6	0.7	6.1	4.8	15.4	0.0	9.0	35.3	18.3	0.7	2.0	9.7	18.3	9.7	15.4	0.7	19.5	3.3	2.0	12.6	27.7	27.7	21.9	6.1	6.8	273
7	18.3	3.9	9.0	0.0	8.4	39.9	9.0	17.4	11.9	61.6	4.2	2.0	33.5	77.6	55.0	25.9	45.6	60.6	30.6	25.9	30.6	5.5	0.0	0.7	577
8	15.4	3.3	12.4	15.4	2.6	1.3	0.0	0.0	0.0	2.6	21.2	25.9	25.9	39.9	55.9	44.6	14.8	3.5	0.7	2.0	1.3	1.3	2.6	3.3	296
9	2.6	3.9	5.5	1.3	1.3	0.0	1.3	0.0	0.7	0.0	0.7	0.7	15.4	3.9	21.2	9.7	9.7	12.6	5.5	0.0	2.6	1.3	9.0	3.5	112
10	0.0	0.0	0.7	4.8	0.7	0.0	1.3	1.3	3.9	6.8	2.6	1.3	6.1	30.6	29.5	18.3	10.8	17.2	9.7	35.3	30.6	15.4	6.8	5.5	239
11	0.0	0.0	4.8	24.8	66.3	83.2	83.2	85.5	66.3	32.4	0.7	21.3	44.6	21.9	25.9	20.1	12.6	37.1	25.9	35.3	14.8	15.4	9.7	28.8	760
12	8.4	0.0	0.0	0.0	0.0	21.9	24.8	20.1	15.9	29.8	4.8	11.9	26.6	45.5	75.1	204.5	114.3	47.7	21.3	16.6	27.7	43.1	36.1	1.3	797
13	8.4	28.8	34.8	0.0	4.2	0.0	23.0	55.0	55.0	32.4	1.3	12.6	55.9	64.8	49.3	71.9	55.0	61.6	77.4	85.5	107.0	170.9	40.1	281.0	1376
14	199.1	4.8	76.4	9.5	13.9	2.0	1.3	15.9	11.8	0.0	1.3	23.0	55.9	79.8	99.0	42.7	24.8	0.7	2.0	8.4	1.3	0.0	1.3	4.8	680
15	15.9	277.0	106.1	242.9	42.7	86.7	125.0	4.2	0.0	0.0	4.8	18.3	35.3	35.3	44.6	49.3	35.3	39.9	14.4	2.6	0.7	27.7	24.8	27.0	1260
16	0.0	2.6	0.0	0.0	0.0	0.0	19.5	35.3	35.3	18.3	4.8	7.7	40.9	44.6	55.0	114.9	134.7	50.3	41.7	32.4	40.9	12.6	2.0	0.7	694
17	0.0	0.7	4.2	5.5	8.4	72.9	87.7	25.9	15.4	30.6	15.4	2.6	15.9	35.3	21.3	21.2	27.0	4.8	6.1	9.7	15.4	7.7	4.2	50.3	488
18	30.6	20.6	2.0	4.2	20.1	44.6	60.6	45.6	35.3	34.2	11.9	10.2	24.2	35.3	49.3	40.8	9.0	6.8	13.7	25.9	0.7	0.0	0.7	0.0	526
19	0.7	6.1	1.3	9.0	11.3	1.3	0.0	7.7	21.2	9.7	12.6	0.7	0.7	8.4	23.0	16.6	24.8	45.6	48.4	38.0	15.4	11.9	9.7	24.8	349
20	29.5	18.3	45.6	12.6	8.4	0.0	0.0	0.7	12.6	4.8	11.9	37.7	12.6	6.8	30.6	35.3	27.7	2.0	12.6	5.5	4.8	2.0	0.7	0.0	322
21	0.0	0.0	0.0	0.0	39.5	17.1	0.0	0.7	4.8	6.8	0.7	5.5	4.8	18.3	45.6	44.6	60.6	39.9	20.6	0.7	0.7	0.0	1.3	2.0	314
22	2.0	8.4	0.0	0.0	0.0	0.0	0.0	2.0	3.3	2.0	12.6	39.9	25.9	67.2	99.0	29.5	20.1	2.6	6.1	37.1	6.1	9.0	0.0	0.0	373
23	0.7	3.5	0.7	20.1	3.9	18.3	21.2	25.9	23.0	13.7	4.8	15.4	6.8	15.9	8.4	13.7	24.8	3.3	10.8	9.7	11.9	1.3	0.0	2.0	260
24	8.9	30.6	20.0	0.0	0.0	0.7	4.2	0.7	0.7	1.3	2.0	6.8	10.2	25.9	44.6	18.3	18.3	11.5	9.0	22.4	23.5	4.8	0.0	11.9	276
25	21.9	24.8	117.5	103.0	26.3	6.1	25.9	5.5	15.4	15.4	4.8	20.1	44.6	61.9	26.9	3.5	0.7	42.4	56.1	54.0	0.0	10.6	6.8	5.5	700
26	2.6	1.3	1.3	0.0	2.6	0.0	0.7	0.7	11.3	7.7	11.9	44.6	44.6	50.3	40.9	49.8	31.0	235.0	97.4	6.8	0.7	2.6	0.0	1.3	645
27	0.7	0.0	0.0	27.7	32.4	23.0	9.0	24.8	7.7	9.0	4.8	70.5	24.2	35.3	23.0	25.9	20.1	0.7	0.7	15.4	71.9	79.8	91.1	66.3	664
28	15.9	1.3	27.7	20.1	18.3	1.3	0.0	3.3	0.0	2.0	6.8	21.2	55.0	35.3	33.3	12.6	4.2	1.3	2.0	1.3	0.0	1.3	0.0	0.0	264
29	0.0	0.0	0.0	5.5	8.9	1.3	1.3	9.7	15.4	3.9	4.8	9.7	37.1	50.3	30.6	30.6	32.4	6.8	2.0	0.0	0.0	0.0	1.3	1.3	253
30	0.0	0.0	9.0	3.3	3.3	0.7	0.0	1.3	21.2	6.1	5.5	2.0	6.1	0.0	6.8	2.6	3.9	12.6	21.2	0.7	2.0	1.3	2.0	0.7	112
31	1.3	8.4	13.7	5.5	4.2	1.3	20.6	39.9	23.0	6.1	4.8	12.6	35.3	46.6	20.1	8.2	2.6	23.0	39.5	9.0	0.7	0.7	30.6	12.4	370
KWh	440	505	508	541	342	506	634	497	569	434	262	495	756	1134	1082	1027	904	888	693	688	739	764	502	650	15561

Rang	Notation Notation																								
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	0.7	0.0	1.3	2.6	0.7	0.0	0.0	0.7	0.7	14.8	27.7	2.0	21.2	20.1	27.7	13.1	1.3	9.7	50.3	44.6	8.4	0.0	7.7	7.7	263
2	11.3	5.5	0.0	0.0	0.0	0.0	0.0	0.0	1.3	5.5	35.3	45.6	21.2	55.0	39.9	27.7	49.3	8.9	0.7	0.0	0.0	0.0	0.0	0.0	307
3	1.3	9.7	0.0	8.4	0.7	1.3	0.7	0.7	0.0	0.7	9.7	4.8	27.7	85.5	69.3	3.5	8.4	0.0	0.7	3.3	3.9	0.7	8.4	12.6	261
4	6.8	18.3	4.8	12.6	32.4	1.3	8.4	0.0	0.7	3.3	3.5	13.7	3.5	2.0	1.3	29.8	24.8	33.3	249.1	335.4	141.0	9.5	7.7	0.7	944
5	0.0	0.0	4.8	1.3	0.0	0.0	0.0	4.8	91.3	1.3	0.7	0.0	4.8	20.1	53.0	66.3	61.6	27.7	1.3	0.0	0.0	4.2	21.2	0.7	365
6	0.0	0.7	0.0	13.7	13.1	3.9	32.4	39.9	1.3	8.4	121.1	191.4	11.9	166.4	116.7	0.0	4.2	20.6	47.4	0.7	9.0	1.3	13.7	0.0	818
7	2.6	4.8	4.8	0.0	2.0	2.0	48.4	66.3	60.7	9.0	0.0	0.0	2.0	20.1	15.9	13.1	18.8	31.7	4.2	27.7	30.6	15.4	11.9	2.0	394
8	0.0	2.0	9.0	35.3	10.6	1.3	0.0	2.0	1.3	0.0	15.4	12.6	45.6	55.0	82.1	91.1	51.2	18.3	1.3	0.0	0.0	0.0	0.0	0.0	434
9	0.0	0.0	0.0	0.0	2.6	1.3	0.0	1.3	3.3	2.6	2.6	12.6	35.3	29.5	30.5	15.9	56.6	1.3	0.0	0.7	282.9	79.8	4.8	12.6	576
10	8.4	0.0	19.5	36.2	6.8	9.0	0.0	0.0	0.0	0.0	0.0	0.7	13.7	23.0	39.9	39.8	22.4	21.3	0.7	38.0	5.5	2.6	25.9	18.3	332
11	32.4	4.2	2.6	1.3	0.7	5.5	0.7	0.0	1.3	1.3	2.6	9.0	16.6	60.6	12.6	9.0	2.0	1.3	24.0	118.8	130.7	61.6	71.9	71.9	642
12	39.9	25.9	20.1	4.8	0.7	0.7	0.0	0.7	0.0	0.7	9.0	15.4	30.6	39.9	50.3	44.6	29.5	18.3	35.3	30.6	7.7	0.0	11.9	35.3	452
13	2.0	0.7	8.4	9.7	0.7	1.3	17.2	71.9	30.6	44.6	10.2	27.7	44.6	71.9	91.1	77.6	32.4	12.6	12.6	12.6	18.3	12.6	0.7	0.0	611
14	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.3	0.7	2.6	9.0	8.4	20.6	14.4	37.1	70.3	55.9	12.4	12.6	3.3	1.3	11.8	37.1	298
15	35.3	35.3	15.4	0.0	7.1	1.3	0.7	0.0	0.7	0.7	2.6	25.9	25.9	25.9	1.3	4.8	1.3	6.1	4.8	0.7	0.7	0.0	0.0	17.7	214
16	12.6	17.2	15.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	14.4	7.7	20.1	22.2	4.2	29.7	3.5	15.2	28.9	0.0	0.7	18.3	101.3	312
17	66.3	11.9	1.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	7.7	51.2	61.6	59.0	47.7	98.2	53.4	50.3	83.1	71.8	154.5	107.0	66.3	48.7	1040
18	0.7	1.3	9.7	9.7	35.3	39.9	15.4	1.3	1.3	2.6	6.8	21.2	25.9	30.6	44.6	35.3	5.5	0.7	0.7	18.3	61.6	71.9	53.0	11.3	504
19	0.0	3.3	21.2	17.2	0.0	0.7	1.3	0.0	0.7	5.5	30.6	49.3	35.3	83.2	38.4	6.8	0.0	1.3	2.6	27.7	61.6	83.2	77.6	77.6	625
20	91.1	83.2	13.1	5.5	20.1	39.9	24.2	11.9	6.8	13.7	31.3	99.3	164.8	45.3	12.4	4.2	14.4	23.0	39.9	30.6	40.9	18.3	3.3	9.7	847
21	3.3	0.7	3.3	0.7	0.0	2.0	0.0	0.0	0.0	0.0	87.4	55.9	5.5	11.3	12.4	1.3	0.7	6.1	6.1	0.0	0.0	21.9	35.3	3.9	258
22	0.7	0.0	3.9	5.5	44.8	126.8	88.3	21.3	2.6	9.5	16.6	23.0	32.4	33.8	48.4	12.6	1.3	2.0	9.0	24.8	3.3	12.6	6.8	2.6	532
23	3.9	6.8	6.8	6.8	2.6	6.8	2.6	2.0	1.3	0.0	4.8	77.6	83.2	107.0	27.0	494.2	306.3	151.8	97.6	23.0	44.6	45.6	49.3	49.3	1601
24	39.9	25.9	18.3	15.4	0.0	4.8	6.1	9.7	3.3	2.6	0.0	0.7	10.6	25.9	39.9	64.8	20.1	8.4	0.0	9.7	1.3	0.0	0.0	0.0	307
25	11.9	32.4	12.6	67.2	39.9	30.6	21.2	4.8	0.0	0.0	3.9	18.3	25.9	44.6	17.2	11.5	2.6	1.3	4.2	23.0	39.9	27.7	21.2	1.3	463
26	0.0	2.0	3.3	8.4	3.9	2.6	0.0	0.0	0.0	1.3	12.6	27.7	39.9	55.0	47.4	0.7	4.2	11.3	32.4	5.5	0.7	15.4	23.0	20.1	317
27	2.0	0.7	0.0	0.0	0.0	0.0	6.1	18.3	30.6	35.3	35.3	21.2	15.4	24.8	221.6	210.0	45.6	33.3	18.3	6.8	9.0	165.8	329.9	55.9	1286
28	3.9	2.0	27.7	41.7	2.6	3.9	9.0	2.6	9.7	2.0	6.1	23.0	50.3	50.3	79.8	122.8	71.9	8.4	0.0	25.9	49.3	49.3	55.0	52.2	749
29	8.4	1.3	11.3	0.0	0.0	0.7	12.6	0.0	0.0	0.0	12.6	23.0	55.0	60.6	79.8	142.6	79.8	20.1	6.8	8.4	0.7	18.3	21.2	21.2	584
30	21.2	15.4	15.4	9.0	6.1	6.8	6.8	3.3	0.7	0.0	1.3	18.3	44.6	55.0	53.5	71.9	8.4	49.3	44.6	82.1	202.0	202.0	178.2	154.5	1250
KWh	406	311	254	313	233	294	302	263	251	166	500	894	971	1402	1438	1754	1078	638	805	1012	1311	1028	1136	826	17585

Rang	la	Octo	ober 2	2007							Win	d Po	wer O	utput	of Boı	านร 60	0/44 T	urbin	e (Mo	onth's	s Sum	mary)	1		
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	130.7	85.5	49.3	23.0	3.9	0.7	2.0	0.0	0.0	0.7	5.5	35.3	49.3	55.0	77.6	83.2	39.9	4.8	30.6	35.3	0.7	12.6	15.4	3.3	744
2	6.8	3.9	9.7	3.9	3.3	6.1	25.9	39.9	3.9	0.7	0.0	0.7	20.1	55.0	39.9	17.2	0.7	2.0	2.0	21.3	55.0	30.6	6.8	1.3	356
3	2.0	2.0	0.0	1.3	0.0	0.0	0.0	1.3	0.7	0.7	15.4	39.9	60.6	66.3	50.3	369.4	403.1	256.1	26.6	4.8	0.7	3.3	3.3	3.5	1311
4	9.7	3.3	3.3	1.3	2.6	1.3	1.3	0.0	0.0	0.0	11.9	60.6	114.9	162.4	53.0	56.6	0.7	6.1	55.0	25.9	21.2	44.6	35.3	30.6	701
5	8.4	3.9	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.3	15.4	71.9	114.9	122.8	121.1	114.9	20.1	3.3	1.3	0.0	2.6	3.9	0.0	606
6	0.7	5.5	2.6	2.6	3.9	3.9	6.8	2.6	0.0	0.0	1.3	15.4	66.3	83.2	122.8	118.0	115.0	9.0	0.7	31.7	13.1	0.7	38.0	83.2	727
7	71.9	71.9	93.4	68.5	71.9	99.0	130.7	93.4	77.6	49.3	39.9	27.7	0.7	11.9	18.3	15.4	30.6	25.9	44.6	68.5	71.9	35.3	39.9	25.9	1284
8	35.3	15.4	35.3	21.2	39.9	35.3	6.1	0.7	2.6	0.0	0.0	24.2	60.6	77.6	85.5	74.2	30.6	1.3	20.6	71.9	71.9	66.3	49.3	49.3	875
9	35.3	21.2	21.2	18.3	0.7	6.8	9.7	2.6	0.7	0.0	2.0	25.9	66.3	77.6	93.4	91.1	48.4	0.7	2.6	0.0	12.6	21.2	25.9	18.3	602
10	2.0	2.0	0.7	1.3	2.6	3.3	1.3	0.0	0.0	0.0	18.3	39.9	71.9	118.8	202.0	142.6	126.8	13.1	4.8	8.4	0.7	0.0	1.3	2.6	764
11	1.3	0.0	2.6	0.0	1.3	3.9	6.1	1.3	0.0	0.0	10.6	25.9	49.3	71.9	83.2	114.9	71.9	22.2	0.0	0.7	24.8	49.3	9.7	9.7	561
12	2.6	0.0	0.0	0.0	0.0	1.3	2.6	0.0	0.0	0.0	1.3	21.2	56.9	87.7	107.0	134.7	79.8	21.3	9.0	27.7	71.9	77.6	51.2	44.6	798
13	83.2	91.1	71.9	77.6	60.6	25.9	12.6	9.7	2.6	0.7	0.0	42.7	83.2	91.1	138.6	99.0	46.6	4.8	0.7	0.0	0.0	2.0	3.3	18.3	966
14	9.7	3.9	6.8	9.7	21.2	32.4	25.9	2.6	0.0	2.0	3.3	20.1	74.2	150.5	178.2	228.3	109.1	4.8	1.3	67.2	166.4	61.6	25.9	30.6	1235
15	39.9	21.2	1.3	0.0	3.3	2.0	3.9	6.8	9.7	0.0	0.0	9.7	40.9	138.6	98.2	81.3	46.6	9.7	60.6	0.7	14.4	49.3	44.6	30.6	713
16	39.9	30.6	6.8	3.9	2.0	2.0	2.0	0.0	0.0	0.0	11.9	25.9	55.0	50.3	77.6	16.6	15.4	8.4	11.9	0.0	0.0	24.8	21.2	6.8	413
17	0.7	0.0	0.0	0.0	0.0	2.0	0.0	0.0	0.0	0.0	3.3	35.3	61.6	114.9	101.7	118.8	85.5	20.9	0.7	2.6	1.3	0.0	0.0	0.0	549
18	9.7	25.9	39.9	55.0	60.6	39.9	66.3	83.2	71.9	55.0	39.9	4.8	22.4	35.3	50.3	79.8	32.4	16.6	21.2	0.7	2.6	27.7	55.0	77.6	973
19	39.9	56.9	60.6	77.6	71.9	13.1	0.0	0.0	0.0	9.0	30.6	77.6	77.6	66.3	77.6	60.6	35.3	21.2	25.9	25.9	2.0	2.0	9.0	25.9	866
20	15.4	30.6	60.6	61.6	66.3	49.3	60.6	27.7	1.3	1.3	14.8	25.9	77.6	66.3	71.9	71.9	114.9	85.5	66.3	44.0	18.3	13.1	0.0	2.0	1047
21	0.0	0.0	0.0	0.0	6.1	39.9	12.6	18.3	3.9	0.0	0.0	17.2	55.0	85.5	77.6	29.5	18.3	3.9	39.9	6.8	2.0	0.0	0.7	39.9	457
22	25.9	6.1	3.9	9.7	12.6	3.9	3.3	1.3	1.3	0.7	0.0	11.3	45.6	91.1	93.4	150.5	40.8	0.0	3.3	0.0	0.0	28.8	49.3	39.9	622
23	77.6	83.2	91.1	91.1	61.6	25.9	35.3	25.9	6.1	3.9	0.7	8.4	35.3	93.4	146.6	126.8	71.9	55.0	50.3	6.8	7.7	0.0	0.0	1.3	1105
24	12.6	18.3	6.8	40.9	55.0	35.3	11.9	0.7	0.0	0.0	0.0	11.3	40.9	55.0	49.3	35.3	11.3	0.0	5.5	2.0	0.0	23.0	21.2	18.3	454
25	9.7	30.6	21.2	18.3	9.7	18.3	12.6	13.7	0.7	0.0	1.3	15.4	45.6	75.1	91.1	83.2	27.7	6.8	10.2	9.0	1.3	2.6	0.0	0.0	504
26	0.0	1.3	3.9	1.3	3.3	12.6	39.9	9.7	0.0	0.0	1.3	55.0	99.0	134.7	154.5	122.8	102.9	0.7	6.1	0.7	14.8	25.9	44.6	30.6	865
27	6.8	15.4	12.6	23.0	23.0	21.2	39.9	39.9	20.1	0.7	1.3	2.0	0.7	9.7	9.0	11.9	13.7	0.0	8.4	79.8	107.0	268.0	202.0	202.0	1118
28	154.5	107.0	51.2	15.4	21.2	21.2	6.8	3.9	9.7	2.6	0.7	4.2	25.9	49.3	66.3	49.3	27.7	5.5	6.8	6.1	0.0	0.0	15.4	3.9	654
29	3.9	0.7	0.0	0.0	3.3	7.7	0.7	2.6	0.0	0.0	0.7	1.3	35.3	51.2	60.6	66.3	29.5	4.8	9.7	2.0	0.0	2.0	3.9	3.9	290
30	6.8	3.3	9.7	15.4	15.4	49.3	35.3	23.0	3.9	0.7	0.0	7.7	55.9	49.3	44.6	44.6	8.4	0.0	2.6	21.2	30.6	45.6	25.9	35.3	534
31	21.2	35.3	40.9	118.8	67.2	30.6	30.6	51.2	18.3	6.8	3.9	2.6	0.0	8.4	21.2	11.9	0.7	6.1	25.9	77.6	130.7	130.7	107.0	77.6	1025
KWh	864	776	708	761	694	594	592	462	235	134	221	710	1620	2398	2664	2827	1900	637	557	650	843	1051	909	917	23721

Rangl	а	Nove	mber	2007							Win	d Pov	ver C	utput	of Bo	nus 6	00/44	Turb	ine (M	lonth's	Sumr	nary)			
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	60.6	61.6	55.0	55.0	60.6	85.5	6.8	2.0	0.7	6.8	18.3	20.1	25.9	18.3	23.0	15.4	0.0	27.7	37.1	27.7	85.5	109.2	83.2	66.3	952
2	45.6	9.0	11.3	21.3	39.9	5.5	0.0	0.7	0.7	0.0	2.6	11.9	45.6	35.3	35.3	24.8	0.7	0.0	0.0	11.3	49.3	77.6	71.9	49.3	549
3	71.9	107.0	0.0	49.3	20.1	2.6	2.6	0.0	1.3	16.6	9.7	30.6	40.9	55.0	35.3	5.5	3.5	1.3	0.7	0.0	0.0	0.0	0.0	0.0	454
4	0.0	4.8	0.0	2.6	6.1	5.5	0.7	1.3	0.0	0.0	0.0	0.0	1.3	1.3	0.0	1.3	0.7	0.0	0.0	2.6	2.6	3.9	3.9	21.2	60
5	14.8	18.3	9.0	29.5	3.9	21.2	15.4	1.3	12.6	15.4	6.8	2.0	6.8	21.2	15.4	12.6	21.2	44.6	119.4	192.6	114.9	39.9	27.0	0.7	766
6	2.6	2.0	1.3	0.0	2.0	1.3	0.7	0.0	9.0	2.0	4.8	21.2	44.6	49.3	39.9	45.6	23.0	12.6	0.7	0.0	0.0	0.0	0.0	0.0	262
7	0.0	0.0	0.0	0.0	1.3	0.0	3.3	0.0	0.7	1.3	21.9	66.3	71.9	77.6	79.8	38.0	15.4	0.7	0.0	0.0	0.0	0.0	0.7	12.6	391
8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	11.9	60.6	77.6	77.6	77.6	83.2	71.9	15.4	18.3	2.0	0.0	0.0	0.0	0.0	496
9	6.1	6.8	12.6	2.6	0.7	0.0	2.0	0.0	0.0	2.0	15.4	71.9	55.0	74.2	49.3	49.3	13.7	11.9	11.9	7.7	0.0	0.0	0.0	6.1	399
10	15.4	12.6	3.3	12.6	21.2	15.4	18.3	12.6	0.0	0.0	5.5	39.9	49.3	71.9	93.4	114.9	68.5	36.2	21.2	6.1	0.0	0.0	14.8	21.2	654
11	21.2	12.6	15.4	25.9	44.6	18.3	9.7	6.1	1.3	0.7	0.0	7.7	35.3	49.3	77.6	71.9	10.2	0.7	6.1	0.0	0.7	15.4	15.4	21.2	467
12	21.2	18.3	23.0	21.2	21.2	9.7	3.9	3.9	2.0	0.0	0.0	12.6	30.6	49.3	66.3	83.2	55.0	15.4	11.3	0.0	0.0	0.0	2.0	21.2	471
13	21.2	12.6	21.2	21.2	9.7	9.0	11.9	3.3	2.0	0.0	0.0	9.0	18.3	50.3	25.9	35.3	15.4	5.5	0.0	0.0	0.0	1.3	6.8	2.0	282
14	3.3	3.9	3.9	6.8	21.2	21.2	15.4	0.0	0.0	0.0	1.3	6.8	15.4	35.3	21.2	15.4	17.2	32.4	0.0	2.0	2.6	2.6	2.6	3.9	234
15	2.6	2.6	2.6	12.6	3.9	1.3	0.0	0.0	0.0	0.0	0.0	4.8	25.9	60.6	55.0	55.0	12.6	2.6	0.0	0.0	9.0	6.8	6.8	12.6	277
16	6.8	18.3	18.3	12.6	25.9	18.3	18.3	12.6	3.3	2.6	3.9	3.9	2.6	7.7	25.9	12.6	4.8	0.0	4.2	12.6	44.6	39.9	21.2	12.6	333
17	18.3	21.2	2.0	12.6	18.3	6.8	15.4	18.3	6.8	2.0	0.0	2.0	30.6	49.3	35.3	35.3	6.1	14.8	0.0	4.2	30.6	60.6	30.6	23.0	444
18	27.7	13.1	3.3	9.0	2.6	0.0	0.0	3.9	2.6	0.0	2.6	21.2	49.3	61.6	44.6	11.9	24.8	27.7	6.8	5.5	2.0	0.7	0.0	0.0	321
19	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	5.5	21.2	30.6	35.3	35.3	0.7	0.0	1.3	3.9	9.7	21.2	30.6	21.2	14.8	231
20	3.3	18.3	30.6	25.9	39.9	44.6	49.3	32.4	3.3	2.0	0.0	0.0	6.1	6.1	18.3	4.2	0.0	1.3	50.3	66.3	50.3	44.6	23.0	49.3	569
21	39.9	83.2	55.0	55.0	55.0	55.0	30.6	21.2	12.6	5.5	0.7	0.7	15.4	12.6	18.3	8.4	0.0	0.0	0.0	7.7	2.0	2.0	0.0	2.6	483
22	32.4	49.3	71.9	35.3	55.9	66.3	71.9	25.9	9.7	0.7	0.0	0.0	0.7	2.0	1.3	0.0	0.0	9.0	35.3	49.3	44.6	30.6	6.1	23.0	621
23	30.6	71.9	126.8	170.3	99.0	44.6	18.3	15.4	3.3	9.7	1.3	0.7	0.0	2.0	3.9	0.0	0.0	0.0	0.0	3.3	11.3	0.0	2.0	1.3	615
24	3.9	12.6	21.2	39.9	30.6	23.0	20.1	17.2	3.3	0.0	0.0	0.0	2.0	9.7	6.8	0.7	0.0	2.6	3.9	6.8	7.7	0.0	0.0	0.0	212
25	0.0	0.0	2.0	2.6	2.6	21.2	12.6	25.9	6.8	3.9	3.9	0.7	0.0	0.0	0.0	1.3	30.6	39.9	25.9	18.3	0.0	0.0	0.0	0.0	198
26	0.0	0.7	0.0	0.7	3.9	0.7	0.0	2.0	0.0	0.7	1.3	3.3	9.7	3.9	2.6	0.0	0.0	0.0	2.6	3.9	2.0	0.0	0.0	0.0	38
27	0.0	1.3	0.7	1.3	0.0	0.0	0.7	2.0	0.0	0.0	0.0	0.0	3.3	21.2	35.3	25.9	3.9	19.5	2.0	0.7	3.9	1.3	0.0	0.0	123
28	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	0.0	11.9	35.3	49.3	71.9	60.6	71.9	42.7	2.0	3.9	12.6	12.6	0.0	2.0	1.3	5.5	384
29	9.0	23.0	5.5	2.0	0.7	0.0	0.0	1.3	6.8	2.0	2.6	18.3	6.8	18.3	3.3	21.9	6.8	8.4	5.5	6.1	77.2	188.7	32.4	40.9	487
30	77.6	6.1	0.7	2.6	7.7	9.7	9.7	13.7	1.3	0.0	0.0	0.7	2.0	8.4	20.9	4.8	31.7	5.5	1.3	11.3	9.7	2.6	3.3	0.7	232
KWh	536	591	496	630	598	487	337	223	89	85	155	487	775	1025	1018	821	440	341	381	470	571	660	376	412	12005

Rang	la	Dece	mber	2007							Win	d Pov	ver Ou	itput o	f Bor	nus 60	0/44	Γurbi	ne (M	onth's	Sum	ımary)			
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	3.9	3.9	3.3	0.0	2.6	3.9	6.8	18.3	35.3	12.6	9.7	21.2	18.3	39.9	4.8	9.0	1.3	0.7	0.0	0.0	0.0	3.9	27.7	6.1	233
2	5.5	5.5	0.0	0.0	0.0	1.3	0.0	0.0	0.7	3.3	30.6	55.0	83.2	99.0	83.2	71.9	28.8	2.0	1.3	18.3	44.6	60.6	39.9	30.6	665
3	1.3	0.0	0.0	0.0	0.7	0.7	0.0	0.7	0.0	0.0	0.0	2.0	15.4	21.2	5.5	0.0	2.0	9.7	41.1	117.1	71.9	51.2	39.9	25.9	406
4	20.1	44.6	25.9	18.3	12.6	14.8	0.7	2.0	0.0	0.0	1.3	3.3	4.2	18.3	21.2	15.4	0.7	0.7	27.7	60.6	13.1	1.3	0.0	0.0	306
5	2.6	0.7	3.3	3.3	0.7	0.0	0.0	0.0	0.7	0.0	0.7	0.0	3.3	0.7	0.7	15.4	18.3	4.8	11.3	3.9	6.8	3.9	1.3	2.0	84
6	0.0	9.0	0.7	0.0	10.6	7.7	0.0	0.7	0.0	0.0	0.0	0.0	2.6	15.4	18.3	19.0	2.6	0.7	28.8	77.6	23.0	6.8	0.7	0.0	224
7	0.0	0.0	0.7	7.7	0.0	1.3	0.0	0.7	0.0	0.0	8.4	45.6	71.9	91.1	79.8	37.1	12.6	5.5	6.1	0.7	0.7	2.0	0.0	6.1	378
8	35.3	44.6	30.6	49.3	55.9	40.9	49.3	66.3	52.7	1.3	0.0	2.6	21.2	30.6	23.0	6.1	1.3	9.0	15.4	9.7	27.7	20.6	0.0	0.0	593
9	15.4	1.3	4.8	3.3	0.0	0.7	9.0	8.4	8.4	35.9	15.2	13.7	22.2	0.7	30.8	4.2	0.0	0.0	9.0	21.3	39.9	24.8	20.1	27.7	317
10	12.6	0.7	0.0	1.3	0.0	2.0	8.9	20.1	8.4	0.7	6.8	18.8	8.4	2.6	10.6	7.7	13.1	1.3	3.3	0.0	0.7	0.0	0.0	1.3	129
11	3.9	3.9	11.9	25.9	55.0	12.6	3.9	15.4	1.3	0.0	0.0	5.5	18.3	30.6	27.7	24.8	0.0	4.8	2.0	2.0	1.3	30.6	15.4	3.9	301
12	2.6	6.1	3.3	2.6	21.3	39.9	49.3	11.9	0.7	2.0	3.3	0.7	5.5	6.8	25.9	8.4	0.0	0.7	3.3	6.8	9.0	3.3	0.0	2.0	215
13	0.7	0.0	0.0	69.5	16.4	18.3	4.8	32.4	45.5	17.1	17.1	8.4	5.5	12.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.3	249
14	0.0	0.0	1.3	3.9	2.0	0.7	0.0	0.0	2.6	2.6	0.0	0.0	0.0	0.0	0.0	2.6	3.3	15.4	21.2	25.9	39.9	39.9	35.3	25.9	222
15	25.9	30.6	21.2	25.9	18.3	21.2	21.2	15.4	6.8	6.8	18.3	3.9	3.3	2.0	6.8	9.7	12.6	6.1	0.0	1.3	18.3	6.8	3.9	3.3	289
16	2.6	6.1	2.6	0.7	3.3	6.1	0.7	3.3	0.0	0.0	0.0	2.6	17.2	44.6	49.3	23.0	1.3	2.0	5.5	44.6	66.3	39.9	101.3	91.1	514
17	138.6	105.3	68.5	118.8	204.5	66.3	18.3	30.6	60.6	74.2	35.3	18.3	25.9	18.3	18.3	8.4	1.3	23.0	9.0	0.7	0.0	6.1	5.5	18.3	1074
18	12.6	3.9	6.8	15.4	6.8	9.7	6.8	4.8	1.3	0.7	4.2	0.0	0.7	2.6	2.6	2.6	2.0	0.0	1.3	3.3	0.7	0.7	0.0	0.0	89
19	0.0	6.1	7.7	0.0	0.0	0.0	0.0	0.0	0.0	1.3	18.3	49.3	44.6	20.1	3.5	0.0	0.7	0.7	2.0	4.2	39.9	161.3	12.4	0.7	373
20	0.0	5.5	42.4	204.5	183.5	107.0	55.0	23.0	31.7	5.5	2.0	9.7	0.7	2.0	1.3	6.1	5.5	0.0	0.7	9.7	0.7	29.5	32.3	12.4	770
21	13.1	27.6	40.1	9.7	61.6	18.4	21.9	11.9	6.1	0.0	1.3	15.4	14.8	9.7	4.2	11.9	9.7	12.6	9.7	21.2	21.2	21.2	18.3	32.4	414
22	60.6	50.3	35.3	50.3	77.4	113.8	30.6	21.2	3.9	11.3	1.3	0.7	2.0	3.9	6.8	0.7	0.0	0.0	0.0	0.0	0.0	0.0	4.2	9.0	483
23	0.7	12.6	2.6	12.6	12.6	1.3	4.2	1.3	0.0	1.3	0.0	0.0	0.7	2.6	4.8	0.0	0.7	0.7	14.4	14.4	16.6	7.7	37.3	5.5	154
24	5.5	2.0	0.0	0.0	0.7	0.0	2.6	1.3	7.1	1.3	4.8	20.1	6.8	19.0	44.6	30.6	0.7	3.9	0.0	0.0	0.0	0.0	0.0	0.0	151
25	0.7	3.9	2.0	3.9	3.3	0.7	0.0	0.0	0.7	0.0	6.1	35.3	55.0	77.6	60.6	50.3	8.4	0.0	12.6	30.6	49.3	35.3	1.3	0.0	437
26	0.0	0.0	2.6	2.6	0.0	0.0	0.0	0.0	0.0	0.0	1.3	21.2	40.9	71.9	77.6	49.3	8.4	9.7	35.3	21.3	0.0	0.0	0.0	0.0	342
27	2.6	0.0	0.0	6.1	6.8	21.2	18.3	21.9	9.7	2.0	0.0	9.0	44.6	55.0	49.3	21.2	12.6	1.3	0.0	0.7	3.9	0.0	0.0	0.0	286
28	2.6	0.7	2.6	18.3	15.4	1.3	0.0	0.0	0.0	2.0	6.8	40.9	107.0	107.0	74.2	117.1	50.3	20.1	8.4	12.6	21.2	1.3	3.5	0.0	613
29	1.3	3.9	8.4	3.9	2.6	0.0	2.0	1.3	0.0	0.7	12.6	51.2	99.0	66.3	83.2	55.0	12.6	2.0	0.0	0.0	0.0	0.7	2.0	0.0	408
30	0.0	0.0	1.3	0.0	0.0	4.2	1.3	2.0	1.3	0.0	0.0	3.3	9.7	50.3	44.6	25.9	1.3	0.0	0.7	2.6	15.4	25.9	12.6	3.9	206
31	1.3	0.0	0.0	0.7	0.0	0.0	0.0	0.0	0.0	0.0	9.0	30.6	50.3	55.0	36.2	25.9	4.8	1.3	6.1	12.6	39.9	12.6	3.9	1.3	291
KWh	372	379	330	658	774	516	315	315	285	182	214	488	803	977	899	659	216	138	276	523	572	598	419	310	11217

Rang	la	Janı	uary 2	800						,	Wind	Powe	r Out	put of	Bonu	ıs 600)/44 Tı	urbine	(Mor	nth's S	Summ	ary)			
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	0.7	0.7	7.7	23.5	0.7	9.7	1.3	3.3	1.3	0.0	18.3	30.6	49.3	39.9	55.0	27.7	2.0	0.0	2.6	0.0	9.7	21.2	3.9	1.3	310
2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	7.7	25.9	49.3	49.3	49.3	30.6	7.7	1.3	21.2	21.2	49.3	17.2	25.9	0.0	356
3	1.3	0.7	0.0	0.0	0.0	0.7	0.0	0.7	0.0	0.0	0.7	0.0	1.3	1.3	0.0	0.0	0.0	0.0	0.0	10.6	3.3	1.3	0.0	0.7	22
4	0.0	0.0	0.0	0.7	2.0	0.0	0.0	0.0	11.9	6.8	1.3	2.6	9.0	2.0	2.0	1.3	5.5	0.0	15.9	22.9	27.7	6.1	0.7	0.0	118
5	34.5	16.6	61.6	5.5	13.7	14.5	4.8	1.3	0.0	0.0	0.0	50.3	61.6	25.8	40.9	18.3	36.1	2.0	13.7	15.2	4.8	36.1	8.9	5.5	471
6	3.9	6.1	45.5	19.4	2.6	20.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	42.1	95.7	62.5	9.0	23.0	45.5	27.7	15.4	39.8	9.7	1.3	470
7	12.6	27.7	32.4	26.0	24.8	29.2	11.9	116.0	191.4	59.5	48.4	56.9	75.1	74.2	45.5	8.4	48.8	59.2	46.9	85.3	99.2	26.9	120.0	142.6	1468
8	175.5	257.6	185.0	27.7	51.2	55.9	61.6	68.5	74.2	178.6	129.9	11.3	29.5	37.4	27.6	20.1	2.6	49.8	101.3	71.9	81.1	30.3	4.2	0.0	1733
9	13.1	26.0	47.4	66.9	5.5	26.3	50.8	21.3	13.1	75.1	74.2	178.9	207.4	184.7	59.2	115.8	243.4	69.5	31.5	109.5	95.7	110.9	216.7	141.7	2184
10	117.1	57.7	74.8	0.0	60.7	45.9	48.4	36.1	0.7	2.0	0.7	7.7	51.7	23.4	61.0	234.7	118.8	80.4	25.8	26.3	17.1	1.3	2.0	0.0	1094
11	0.0	0.0	0.7	1.3	0.0	0.0	0.0	0.0	0.0	0.0	6.1	0.7	0.0	2.0	1.3	1.3	21.2	71.9	60.6	60.6	85.5	66.3	71.9	60.6	512
12	83.2	77.6	55.0	71.9	50.3	35.3	44.6	39.9	8.4	0.7	0.7	2.0	0.0	0.0	0.0	3.3	3.9	1.3	2.6	2.0	2.6	0.0	0.0	0.0	485
13	0.0	0.7	2.0	1.3	2.6	0.7	2.0	2.6	0.0	0.0	0.0	1.3	12.6	3.9	18.3	0.7	2.6	18.3	6.8	21.2	30.6	25.9	9.7	2.0	165
14	0.7	0.7	2.0	1.3	11.3	18.3	1.3	1.3	9.0	0.0	0.0	2.6	14.8	12.6	1.3	0.7	6.1	1.3	3.9	12.6	3.9	0.0	0.7	1.3	107
15	14.1	32.4	30.6	23.0	8.4	28.8	16.6	69.5	5.5	2.6	2.6	2.0	3.9	9.7	44.6	9.7	9.7	2.0	4.8	0.0	9.0	26.6	30.6	2.6	389
16	14.8	2.0	15.4	8.4	8.4	1.3	18.3	33.7	32.4	61.6	72.7	82.1	18.4	2.0	11.5	39.2	17.7	8.2	2.0	66.6	40.9	60.1	46.6	15.9	680
17	24.2	4.2	61.3	71.9	31.0	0.0	0.0	26.9	0.0	4.2	17.1	2.6	7.1	28.8	37.1	58.7	134.7	203.3	167.2	241.4	368.4	100.2	12.4	0.0	1602
18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	17.1	17.2	13.7	0.0	0.7	0.7	0.7	0.0	0.0	9.5	39.9	6.1	106
19	3.3	16.6	56.9	35.3	4.8	12.6	30.5	49.3	28.8	1.3	8.4	50.3	49.3	77.6	49.3	55.0	66.3	2.0	2.6	16.6	2.6	0.0	0.0	0.0	619
20	0.0	0.7	1.3	2.0	12.6	3.9	3.9	6.8	2.0	0.0	0.7	35.3	66.3	61.6	55.0	50.0	13.7	11.3	35.3	55.0	35.3	44.6	18.3	3.9	519
21	6.8	1.3	0.0	1.3	9.7	18.3	6.8	3.9	2.6	0.0	0.0	2.6	30.6	55.0	45.6	49.3	4.2	1.3	1.3	2.6	0.7	0.0	1.3	23.0	268
22	12.6	25.9	61.6	83.2	114.9	32.6	36.4	48.4	15.9	14.4	50.3	77.6	85.5	42.7	61.6	11.8	31.7	49.3	66.3	50.3	30.6	25.9	6.8	1.3	1037
23	0.0	0.0	0.0	0.0	0.7	0.7	0.0	0.0	3.3	0.0	0.0	11.9	82.1	122.8	122.8	122.8	101.3	20.6	4.8	1.3	1.3	0.0	0.0	0.7	597
24	0.7	0.0	2.6	1.3	0.7	0.0	0.0	0.0	0.0	9.0	21.2	55.0	138.6	154.5	166.4	107.0	64.8	4.2	0.0	0.0	2.0	3.3	0.0	1.3	732
25	0.0	0.0	3.3	0.0	0.0	2.0	0.0	2.6	0.0	0.0	4.2	61.6	91.1	122.8	154.5	107.0	49.3	4.2	11.3	12.6	2.0	0.0	1.3	2.0	631
26	3.9	1.3	3.3	3.3	2.0	0.7	2.0	2.0	2.0	0.0	4.8	35.3	126.8	150.5	44.5	40.9	113.2	50.3	23.0	107.0	83.2	130.7	142.6	63.8	1137
27	44.6	35.3	27.7	39.9	30.6	25.9	77.4	90.3	21.2	3.3	3.3	3.9	2.6	11.9	24.8	13.7	16.6	0.7	0.0	0.0	0.0	0.0	0.0	2.6	476
28	15.4	9.0	0.0	2.0	6.8	6.8	12.6	30.6	83.2	134.7	154.5	85.5	55.9	20.1	3.3	0.0	0.0	0.0	0.0	0.0	0.0	1.3	1.3	0.0	623
29	2.6	1.3	0.0	0.0	0.0	1.3	9.7	30.6	15.4	3.3	0.0	0.0	18.4	47.4	64.0	24.0	13.1	11.9	27.0	1.3	0.0	1.3	0.0	0.0	273
30	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7	0.0	0.0	15.4	35.3	60.6	44.6	25.9	11.3	5.5	0.7	27.0	30.6	25.9	114.9	398
31	50.3	61.6	39.9	18.3	21.2	21.2	23.0	15.4	1.3	12.6	18.3	4.8	0.7	3.9	7.7	17.2	3.3	0.0	0.0	23.0	77.6	107.0	24.8	3.3	556
KWh	636	663	818	535	477	413	464	701	523	570	646	881	1371	1462	1424	1276	1174	759	730	1065	1206	924	826	598	20139

Rang	la	Febr	uary	2008							Wind	Powe	er Out	put of	f Bor	nus 60	0/44	Γurbin	e (Mo	nth's	Sumn	nary)			
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	2.0	15.4	3.9	6.8	21.2	6.8	12.6	3.9	0.7	0.0	0.0	1.3	20.1	35.3	66.3	49.3	30.6	12.6	61.6	2.0	32.4	39.9	1.3	1.3	427
2	0.0	0.7	0.7	0.7	0.7	0.7	1.3	2.0	0.0	0.0	0.0	1.3	3.3	1.3	2.0	20.6	77.5	4.8	9.0	14.8	2.6	11.3	4.8	0.0	160
3	0.7	1.3	0.0	1.3	0.0	0.0	0.0	0.0	2.0	0.0	0.0	1.3	12.6	35.3	3.9	2.0	4.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	65
4	0.0	0.0	0.0	0.0	77.2	67.2	24.2	45.6	88.7	63.8	85.5	113.8	125.1	107.0	56.0	28.8	91.1	164.9	120.0	159.3	105.3	38.0	11.9	21.9	1595
5	17.2	93.4	52.4	40.8	45.6	52.4	61.0	60.1	91.1	55.9	60.6	28.8	35.3	21.3	8.4	1.3	3.3	2.0	1.3	1.3	0.0	0.0	0.0	0.0	733
6	1.3	0.0	0.7	0.0	0.0	2.6	54.4	51.2	4.8	0.0	2.0	9.0	4.8	61.6	15.2	4.2	0.0	2.6	0.0	9.7	6.8	9.7	0.0	0.7	241
7	0.0	4.2	7.1	0.7	1.3	2.0	3.3	1.3	1.3	15.4	5.5	0.7	22.4	21.9	17.2	53.0	55.9	20.1	32.4	62.8	7.1	7.1	1.3	36.2	380
8	48.1	15.4	7.1	0.7	1.3	0.0	0.0	0.0	0.0	0.0	2.6	0.7	12.4	17.2	11.9	2.6	2.0	30.6	66.3	24.8	21.2	9.0	2.0	3.9	280
9	3.9	12.6	18.3	35.3	71.9	50.3	12.6	6.1	2.0	15.4	6.8	15.4	9.7	2.0	2.0	6.1	35.3	30.6	35.3	9.7	6.8	3.9	6.8	3.9	402
10	3.9	3.9	5.5	18.3	6.8	6.8	9.7	6.8	0.7	0.7	0.0	0.7	23.0	55.9	91.1	54.0	37.1	7.7	0.0	12.6	12.6	15.4	11.9	0.0	385
11	0.0	0.0	1.3	0.7	0.0	1.3	0.0	0.0	0.0	0.0	11.9	60.6	91.1	134.7	91.1	59.2	32.4	28.2	14.8	66.3	66.3	71.9	55.0	39.9	826
12	21.2	12.6	15.4	21.2	25.9	44.6	66.3	71.9	30.6	44.6	39.9	39.9	15.4	2.0	5.5	4.8	55.9	35.3	24.8	101.3	82.1	55.9	55.0	39.9	912
13	30.6	101.3	146.6	203.3	167.6	107.0	91.1	77.6	49.3	25.9	25.9	6.8	11.9	2.0	3.9	0.0	0.7	0.0	17.1	9.0	4.2	15.4	4.8	16.6	1118
14	3.5	0.0	2.6	4.8	0.0	0.0	0.0	0.0	0.7	0.7	0.0	0.0	8.4	37.1	29.8	6.1	7.7	4.2	33.3	27.7	17.2	9.0	4.8	8.4	206
15	18.8	8.4	1.3	3.9	1.3	3.3	3.9	3.3	1.3	2.0	0.0	9.7	35.3	69.5	71.9	60.6	28.7	4.8	12.6	2.6	6.8	12.6	6.1	1.3	370
16	2.6	5.5	5.5	16.6	45.9	114.9	69.5	60.6	91.1	91.1	55.9	55.0	50.3	49.3	49.3	25.9	6.8	3.9	2.6	1.3	1.3	0.0	0.0	2.6	807
17	4.8	3.5	4.8	4.8	0.0	0.0	0.0	0.0	0.0	0.7	15.4	39.9	50.3	77.6	79.8	71.9	66.3	4.2	61.9	130.7	99.0	93.4	66.3	83.2	959
18	43.7	21.2	27.7	15.4	23.0	25.9	44.6	50.3	79.8	69.5	66.3	85.5	22.9	11.9	30.6	60.6	50.3	71.9	130.7	130.7	154.5	229.5	334.5	217.9	1999
19	282.6	157.0	101.3	105.3	66.3	91.1	58.2	134.5	91.0	37.1	35.3	18.3	6.8	12.6	12.6	3.9	4.8	11.9	4.2	1.3	35.3	55.0	21.2	75.1	1422
20	130.7	77.6	36.2	44.6	77.6	93.4	107.5	30.6	49.3	12.6	9.7	3.3	0.0	13.1	39.9	30.6	17.2	6.1	0.7	0.7	2.6	0.7	0.0	1.3	786
21	4.8	43.7	0.7	0.0	0.0	7.1	0.7	9.7	8.2	0.7	4.2	8.9	38.0	66.6	22.4	17.2	49.3	71.9	50.3	54.5	22.4	11.9	18.7	0.0	512
22	29.5	11.9	10.2	83.6	12.6	23.0	52.2	35.3	27.7	8.4	9.7	3.3	4.8	11.9	38.0	155.7	112.8	163.7	154.5	189.0	151.8	127.9	153.3	101.3	1672
23	75.1	59.2	107.1	51.1	82.3	89.0	12.4	16.6	8.4	0.7	11.8	13.1	35.1	7.7	20.0	69.5	55.9	45.5	117.4	134.1	6.1	2.0	0.0	16.6	1036
24	25.9	1.3	0.0	6.1	0.0	12.4	4.8	1.3	2.0	7.7	3.3	2.0	7.7	25.9	55.9	24.2	5.5	0.0	0.0	0.0	1.3	18.3	5.5	0.0	211
25	0.0	0.0	2.0	6.8	15.4	67.2	61.6	25.9	18.3	3.9	9.7	21.2	12.6	35.3	18.3	9.7	18.3	51.2	101.3	228.3	254.5	183.5	150.1	178.2	1473
26	241.4	256.4	134.7	159.1	126.8	179.5	158.4	35.3	71.9	71.9	77.6	66.3	77.6	37.4	16.6	45.6	50.3	93.4	61.6	60.6	79.8	66.3	130.7	228.3	2527
27	126.8	55.9	60.6	30.6	35.3	111.5	91.1	72.9	30.6	39.9	107.0	99.0	39.9	15.4	30.6	71.9	146.6	203.3	103.0	35.3	27.7	16.6	1.3	1.3	1554
28	6.1	44.6	49.3	83.2	83.2	39.9	21.2	37.1	6.8	12.6	1.3	0.0	0.0	2.6	11.3	0.7	0.0	1.3	2.6	0.7	0.7	3.3	0.7	2.6	411
29	2.0	0.0	2.6	6.8	15.4	2.6	0.0	0.0	1.3	2.6	0.7	1.3	0.7	6.1	6.1	18.3	2.0	0.0	0.0	4.8	2.0	66.4	25.3	1.3	168
KWh	1127	1007	805	952	1004	1202	1022	840	759	583	648	707	777	977	907	958	1049	1076	1219	1475	1210	1174	1073	1084	23637

Rang	la	Ma	rch 20	800						,	Wind	Pow	er Ou	tput o	f Bon	us 60	0/44 T	urbin	e (Mo	nth's	Sumn	nary)			
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	18.4	2.0	21.6	32.4	37.9	12.4	13.1	33.8	4.2	0.0	6.1	25.9	49.3	60.6	35.3	45.6	12.4	1.3	2.6	10.6	0.0	1.3	4.2	9.7	440
2	0.7	9.7	12.6	0.0	1.3	0.0	0.0	0.0	0.0	1.3	21.2	23.0	25.9	41.7	77.6	49.3	55.9	16.6	0.7	2.0	0.0	0.0	1.3	12.6	353
3	6.8	44.6	0.0	6.1	2.6	0.0	1.3	0.0	50.5	101.3	74.2	15.4	1.3	9.7	12.4	19.5	18.4	1.3	0.0	1.3	8.4	2.0	11.3	21.2	409
4	8.4	35.5	168.9	11.8	3.3	9.7	15.9	42.1	108.0	99.3	8.4	0.7	0.0	4.2	28.8	12.6	26.9	13.1	21.3	8.4	1.3	18.3	21.2	35.3	703
5	21.2	21.2	25.9	25.9	25.9	51.2	95.7	66.3	32.4	18.3	9.7	21.2	18.3	9.7	2.6	20.1	4.8	1.3	0.7	5.5	1.3	0.0	2.0	1.3	482
6	24.8	17.2	30.6	27.7	23.0	18.3	21.2	9.7	2.0	53.4	25.6	1.3	24.8	30.6	121.1	38.0	70.6	114.9	134.7	114.9	55.9	11.9	9.7	21.3	1003
7	55.0	55.0	49.3	49.3	55.9	66.3	31.7	9.7	11.5	7.7	9.7	43.1	191.4	92.1	61.0	44.2	61.9	68.5	105.3	109.2	304.5	342.9	202.0	77.6	2104
8	75.1	97.6	339.6	393.8	101.3	66.3	67.2	40.9	85.3	21.2	3.9	3.3	6.1	12.6	50.3	71.9	60.6	20.6	2.0	2.0	0.0	0.7	1.3	0.0	1523
9	0.0	3.9	6.8	0.7	2.0	0.7	0.0	0.0	0.0	0.0	9.0	9.7	51.2	93.4	105.3	73.8	334.5	155.7	61.6	49.3	49.3	20.1	5.5	3.3	1036
10	3.9	6.8	6.8	9.7	3.9	6.8	6.8	1.3	0.0	0.0	0.7	20.1	49.3	85.5	20.1	4.8	50.3	9.7	4.8	8.9	51.2	107.0	91.1	83.2	633
11	44.6	12.6	1.3	0.0	1.3	12.6	15.4	15.4	9.7	8.4	1.3	19.5	44.6	93.4	19.5	27.7	27.7	47.4	50.3	39.9	10.6	7.7	60.6	66.3	638
12	60.6	50.3	32.4	3.9	9.0	2.6	2.0	2.0	0.0	1.3	0.7	2.6	55.9	61.6	107.0	99.0	68.5	15.9	9.0	3.9	11.3	3.3	3.3	0.0	606
13	0.0	2.0	37.1	18.3	12.6	6.8	12.6	51.2	15.4	6.8	3.9	3.3	11.3	18.3	23.0	44.6	45.6	39.9	21.2	14.8	2.0	6.1	10.8	2.6	410
14	0.7	9.0	1.3	0.0	0.7	12.6	21.2	35.3	3.9	3.9	3.9	4.8	36.2	55.0	91.1	134.7	138.6	77.4	6.1	4.8	2.6	0.7	8.4	23.0	676
15	49.3	83.2	154.5	190.1	190.1	154.5	130.7	87.7	45.6	18.3	6.8	6.1	4.2	11.9	36.4	55.9	68.5	11.9	4.8	25.9	4.8	1.3	2.0	23.0	1368
16	60.7	217.9	37.3	79.8	40.1	8.4	2.6	12.6	3.3	0.0	1.3	32.4	77.6	83.2	130.7	122.8	134.7	87.7	35.3	27.7	0.0	4.8	0.0	11.3	1212
17	1.3	2.6	1.3	17.2	28.8	5.5	0.7	4.2	1.3	0.0	5.5	56.9	114.9	166.4	307.6	372.0	176.6	27.0	51.1	154.4	370.8	130.2	56.9	30.6	2084
18	50.3	18.3	30.6	2.0	0.7	0.7	32.4	37.1	46.6	6.8	3.9	3.3	18.3	41.3	87.0	347.2	315.5	199.4	87.4	79.0	45.9	29.2	85.5	110.9	1679
19	202.0	216.4	71.9	60.6	23.0	27.7	133.0	82.3	9.7	2.0	1.3	28.8	143.9	150.4	321.3	118.3	2.6	175.5	196.9	19.4	87.7	39.0	79.8	55.9	2249
20	93.4	71.9	25.9	18.3	32.4	11.9	12.6	9.7	2.6	1.3	2.0	2.0	2.0	12.6	35.3	13.1	49.3	35.1	30.5	60.6	6.8	9.7	25.9	32.4	597
21	46.6	55.0	114.9	55.0	55.0	55.0	21.2	15.4	18.3	8.4	12.6	0.0	1.3	13.7	55.0	18.3	5.5	0.0	0.0	7.7	0.0	0.7	15.4	21.2	596
22	3.9	9.0	3.9	14.4	50.3	48.4	39.9	80.4	53.0	2.6	0.7	18.1	11.9	102.6	122.8	79.8	11.5	17.2	1.3	55.9	15.9	201.1	192.6	94.9	1232
23	50.3	44.6	21.2	35.3	60.6	30.6	9.7	15.4	44.6	9.7	6.8	12.4	40.9	68.0	88.7	91.1	60.6	14.8	22.2	24.2	7.7	0.0	15.9	55.0	830
24	107.0	190.1	134.7	107.0	83.2	77.6	46.6	12.6	5.5	0.7	15.4	66.3	99.0	130.7	166.4	107.0	99.0	51.2	5.5	4.8	0.0	0.0	27.7	55.0	1593
25	49.3	60.6	49.3	55.0	71.9	37.1	9.7	6.8	3.9	0.0	0.0	18.3	5.5	11.9	5.5	15.4	11.9	4.8	9.0	14.8	0.0	4.2	18.3	6.8	470
26	3.9	1.3	0.7	1.3	8.9	154.5	122.8	83.1	6.1	3.3	0.0	108.1	33.7	13.1	19.5	203.3	170.3	83.2	71.9	49.3	25.9	24.8	13.1	21.2	1223
27	21.2	12.6	18.3	20.1	12.6	12.6	9.7	6.8	3.3	2.0	0.7	24.8	66.3	72.9	25.3	16.6	45.6	385.3	122.8	8.9	9.0	12.6	6.8	21.2	937
28	18.3	4.2	12.6	21.2	6.8	9.7	9.7	3.9	3.9	3.9	2.6	12.6	25.9	77.6	151.8	36.6	13.7	77.5	18.3	29.8	20.1	4.2	7.7	2.6	575
29	15.4	3.9	2.6	1.3	0.0	0.0	0.7	0.0	0.0	0.7	1.3	9.7	15.4	49.3	50.3	37.1	8.4	2.0	2.0	1.3	1.3	0.7	0.7	0.7	204
30	0.0	0.0	0.0	2.6	2.0	0.0	1.3	0.0	0.0	0.0	0.0	14.8	27.7	66.3	71.9	77.6	35.3	50.3	3.3	7.7	1.3	11.3	2.6	19.5	395
31	339.2	593.9	101.3	278.7	29.8	20.1	11.9	6.1	1.3	11.3	1.3	11.9	75.1	107.0	130.7	256.1	241.4	293.4	576.3	149.9	29.0	40.9	20.0	25.9	3352
KWh	1432	1953	1515	1539	976	920	899	772	572	393	240	620	1329	1847	2561	2654	2427	2100	1658	1097	1125	1036	1003	945	31611

Rang	ļΙa	Αŗ	oril 20	80							Wind	Pow	er Out	tput o	f Bon	us 60	0/44 T	urbin	e (Mo	nth's \$	Summ	nary)			
Dt./Hrs	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24 Hrs
1	8.4	40.9	114.9	260.7	78.2	27.6	11.9	0.0	0.0	0.0	2.0	15.4	46.6	55.9	58.2	99.0	126.8	114.9	51.2	7.7	1.3	2.0	14.1	3.3	1141
2	0.0	9.0	9.7	1.3	8.4	0.7	23.4	61.9	5.5	19.5	122.7	54.5	20.6	29.8	0.0	29.8	27.7	57.7	394.9	284.5	202.0	31.5	8.4	9.0	1412
3	0.0	0.7	0.0	0.0	0.0	24.8	50.3	9.0	3.9	3.3	0.0	0.0	18.3	5.5	38.0	48.7	24.7	2.6	2.0	10.6	83.1	37.3	3.3	0.0	366
4	0.0	0.0	4.2	3.9	3.9	6.8	1.3	7.1	1.3	3.3	13.7	55.0	68.5	27.7	4.8	21.2	12.4	2.0	0.0	6.1	48.8	5.5	9.7	23.0	330
5	50.3	74.2	106.7	72.7	72.9	35.3	33.3	90.3	54.5	120.0	51.2	19.4	80.2	165.2	146.1	190.2	133.0	243.5	34.5	242.7	145.4	79.7	0.7	0.7	2242
6	0.0	0.7	1.3	0.7	1.3	0.0	13.7	8.9	0.0	2.0	2.0	0.0	7.1	8.4	16.6	2.6	1.3	0.0	0.0	9.0	20.1	35.3	5.5	0.0	136
7	0.7	48.4	26.6	12.6	4.8	2.0	6.8	12.6	36.2	51.6	11.3	35.3	20.1	29.5	55.0	49.3	39.9	12.6	2.6	2.0	0.7	2.6	12.4	16.6	492
8	27.7	116.4	33.8	45.6	48.7	7.7	9.0	0.0	0.0	2.0	9.7	8.4	0.7	1.3	0.0	0.0	0.0	0.0	9.5	30.6	1.3	0.7	1.3	0.0	354
9	2.0	1.3	246.3	291.3	53.5	35.3	60.6	25.9	41.7	6.8	0.7	0.0	19.5	14.5	31.3	4.8	12.4	0.0	0.0	22.4	25.9	4.2	27.0	3.3	930
10	15.4	12.6	30.6	15.4	3.5	14.8	3.5	1.3	7.7	0.7	0.7	4.2	0.0	0.0	0.0	0.0	0.0	0.0	4.8	0.0	0.0	1.3	23.4	51.2	191
11	31.7	17.2	164.8	56.9	0.7	4.2	14.8	2.0	0.0	0.0	15.4	40.9	55.9	114.9	126.8	166.4	85.5	50.3	17.1	2.0	0.0	0.7	5.5	0.0	973
12	1.3	6.8	24.8	17.2	5.5	7.7	0.0	0.0	0.0	24.8	55.9	63.8	85.5	16.6	11.3	21.9	95.7	142.6	48.7	26.0	3.9	18.3	6.8	9.7	695
13	4.2	0.0	11.3	25.9	15.4	15.4	2.6	0.7	0.0	0.0	0.7	0.0	9.7	18.3	21.2	12.6	9.7	0.0	1.3	6.1	9.7	0.7	2.6	2.6	170
14	13.1	23.0	0.7	5.5	12.6	30.5	48.7	24.2	0.0	3.3	11.9	12.6	72.9	93.4	114.7	34.5	56.3	2.0	26.9	126.8	105.3	98.2	26.6	13.1	956
15	21.6	4.2	1.3	8.4	29.8	10.2	16.6	0.7	10.6	8.9	30.6	33.7	97.4	124.8	53.1	107.2	60.1	132.7	228.7	26.0	92.0	9.0	20.1	1.3	1129
16	0.0	0.0	0.0	0.0	4.8	21.3	24.2	4.8	2.0	12.6	146.1	280.8	126.8	99.0	184.1	54.5	56.3	8.9	2.0	44.6	110.9	159.7	79.0	21.2	1443
17	32.4	20.1	15.4	21.2	15.4	25.9	9.7	9.7	15.4	9.7	6.1	24.2	39.9	85.5	83.2	77.6	52.4	2.6	0.0	0.7	4.8	2.6	3.9	12.6	571
18	18.3	12.6	6.8	15.4	12.6	3.3	12.6	3.9	1.3	2.6	1.3	15.4	51.2	71.9	71.9	66.3	4.8	1.3	0.0	0.0	6.1	2.0	2.6	6.8	391
19	3.3	3.9	9.7	2.6	0.7	0.0	0.0	0.0	0.0	0.7	2.6	14.4	44.6	45.6	118.8	39.0	42.7	1.3	0.7	0.7	2.6	56.9	43.7	12.6	447
20	21.2	15.4	35.3	30.6	35.3	23.0	21.2	39.9	2.0	2.6	15.4	5.5	39.9	41.7	55.9	55.0	30.6	11.3	0.0	2.0	20.1	99.0	93.4	55.0	751
21	26.6	35.3	39.9	61.6	60.6	17.2	6.8	3.9	1.3	0.7	2.0	25.9	60.6	87.7	142.6	202.0	72.7	22.4	0.0	20.0	1.3	11.3	60.6	45.6	1008
22	35.3	25.9	27.7	6.8	6.1	36.2	20.1	16.6	3.9	2.6	0.0	19.5	25.9	71.9	83.2	38.3	14.8	30.6	44.6	4.8	9.7	3.9	2.6	12.6	543
23	3.9	51.2	56.9	30.6	44.6	30.6	60.6	35.3	39.9	4.8	0.7	24.8	77.6	134.7	142.6	107.0	92.1	0.0	3.5	4.8	6.8	15.4	3.9	3.9	976
24	9.7	6.8	9.7	9.7	15.4	6.8	9.7	3.9	3.9	2.6	1.3	12.6	66.3	83.2	51.2	2.0	0.7	0.0	0.0	0.0	1.3	43.7	113.2	42.7	496
25	6.8	23.0	39.9	37.1	21.2	25.9	15.4	3.9	0.7	0.0	7.7	35.3	66.0	18.8	138.6	67.2	46.7	157.9	140.9	159.7	127.3	69.5	35.3	55.9	1301
26	190.4	528.2	284.6	50.3	66.3	71.9	101.3	80.2	2.0	13.1	85.5	13.1	18.4	16.6	191.0	15.9	8.9	27.3	18.4	40.9	11.9	33.3	211.1	235.2	2315
27	255.3	221.6	281.1	195.3	130.7	127.3	9.7	39.9	6.1	9.7	0.7	3.3	14.4	61.6	101.3	60.6	71.9	24.8	1.3	1.3	0.0	37.1	83.2	55.0	1793
28	44.6	35.3	15.4	21.2	11.3	2.0	1.3	0.7	0.0	1.3	6.1	27.7	44.6	37.1	61.6	183.5	199.9	556.1	412.5	180.0	121.1	142.6	158.4	20.1	2284
29	11.9	9.0	6.1	0.0	2.0	2.6	3.9	0.0	0.0	0.0	2.0	12.6	35.3	66.3	85.5	93.4	42.7	21.9	2.6	8.4	2.0	0.0	0.7	3.3	412
30	24.8	44.6	32.4	12.6	12.6	23.0	31.7	2.0	0.0	0.0	0.0	11.3	30.6	37.1	67.2	83.2	146.6	69.1	75.1	90.3	53.1	80.4	102.4	119.4	1149
KWh	861	1388	1638	1313	779	640	625	489	240	309	606	869	1345	1664	2256	1933	1569	1696	1524	1360	1218	1084	1161	835	27398